

Webinar, 2023-02-09, 10:00 CET

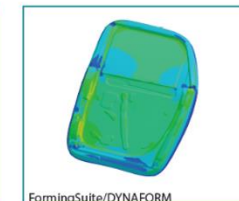
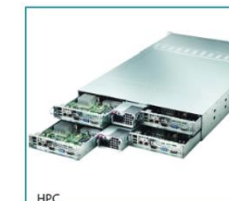
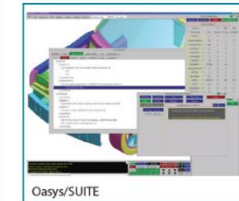
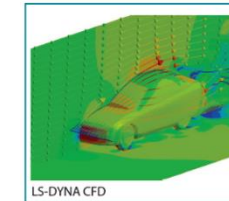
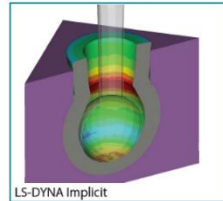
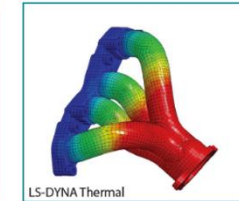
Simulation of FOPS and ROPS: an LS-DYNA Application Demonstration

Axel Hallén, DYNAmore Nordic, an Ansys company

Contact – DYNAmore Nordic, an Ansys company



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 - E-mail: support@dynamore.se
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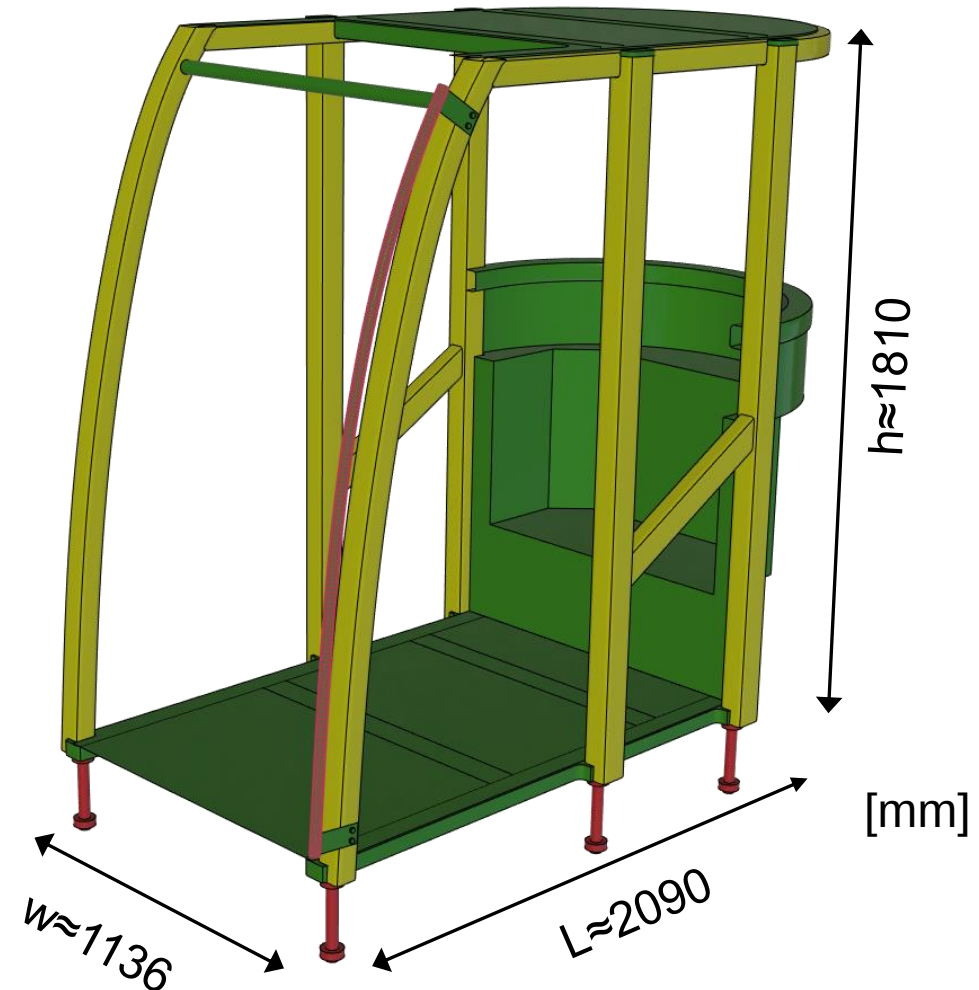


- Introduction to falling object and roll-over protective structures (FOPS and ROPS) for earth-moving machinery and testing thereof.
- Setting up an FE-simulation of FOPS testing.
- Setting up an FE-simulation of ROPS testing.
- Displaying our supporting resources in the form of webinars and guidelines in the process of discussing the above mentioned FE-modeling.

- Testing of FOPS and ROPS is crucial to ensuring operator safety in a wide range of vehicles and machinery.
- These tests are expensive and complicated to perform physically. It is therefore desirable to reduce the amount of physical testing by using numerical simulation instead.
- This example is inspired by the standards for earth-moving machinery,
 - SS-EN ISO 3449:2008 (FOPS laboratory tests and performance requirements).
 - SS-EN ISO 3471:2008 (ROPS laboratory tests and performance requirements).
- For Integral FOPS/ROPS, where the same structure is used for the evaluation against both standards, the FOPS test precedes the ROPS test such that the latter is performed on an already deformed structure.
- The simulation of this example will thus be performed in three stages.
 - 1) Bolt pre-tensioning in a dynamic relaxation phase.
 - 2) FOPS test using explicit time integration.
 - 3) ROPS test on pre-deformed structure using implicit time integration.

Protective Cab Geometry

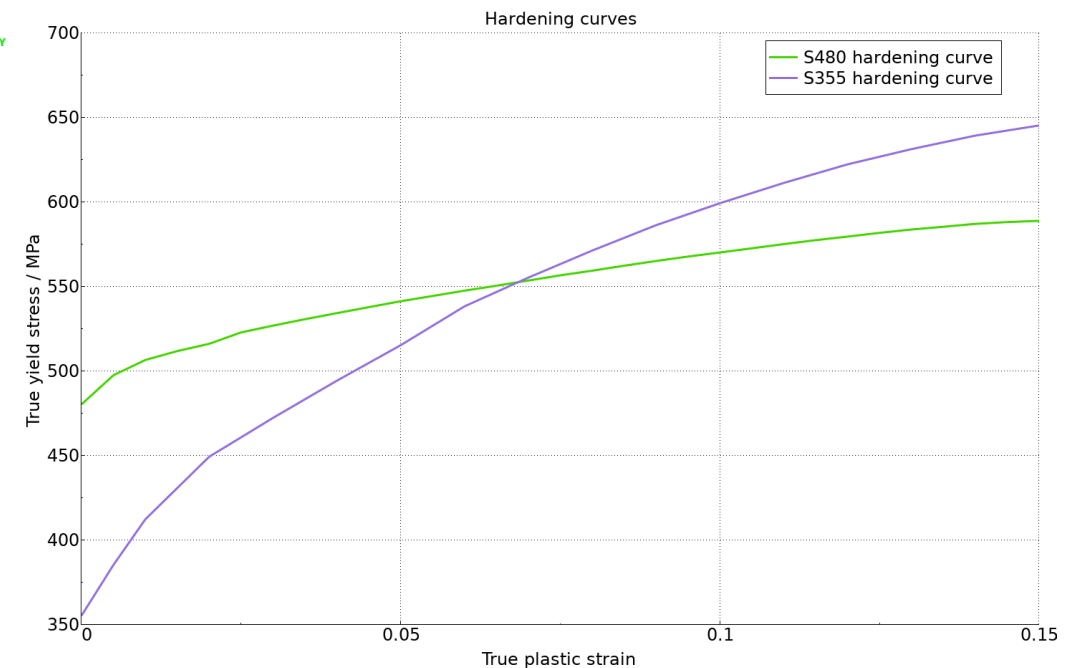
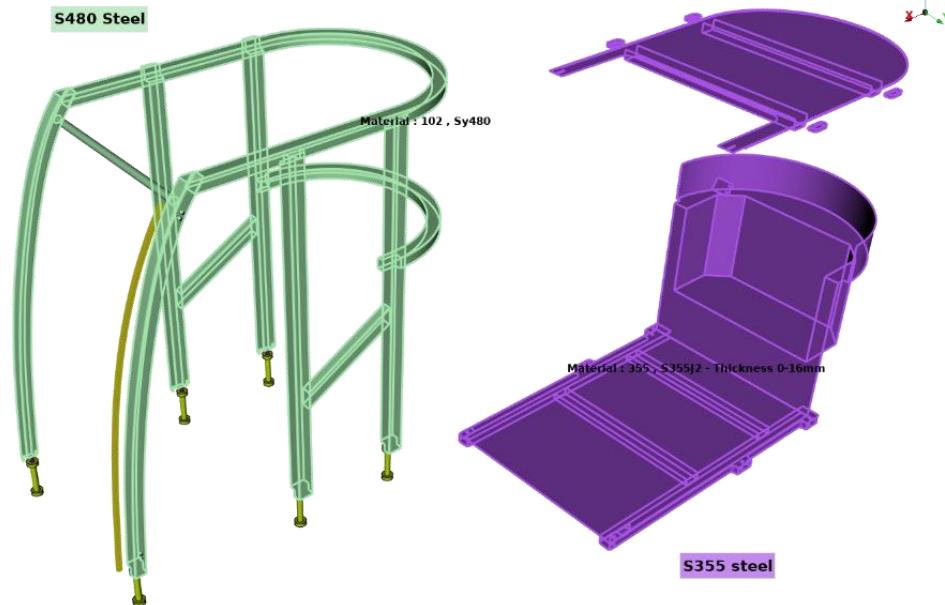
- The cab structure is inspired by images of present and past designs of earth moving machinery.
- It is assumed that the mass of the machine is 15 tonnes.
- The purpose of a FOPS is to provide the operator with reasonable protection from falling objects such as trees, rocks, small concrete blocks, hand tools, et cetera.
- A FOPS is classified as having either level 1 or level 2 impact protection.
 - Level 1: small falling objects
 - Level 2: heavy falling objects
- The purpose of a ROPS is to reduce the possibility of an (seat-belted) operator being crushed in the event of machine roll-over.



Protective Cab Geometry – Materials

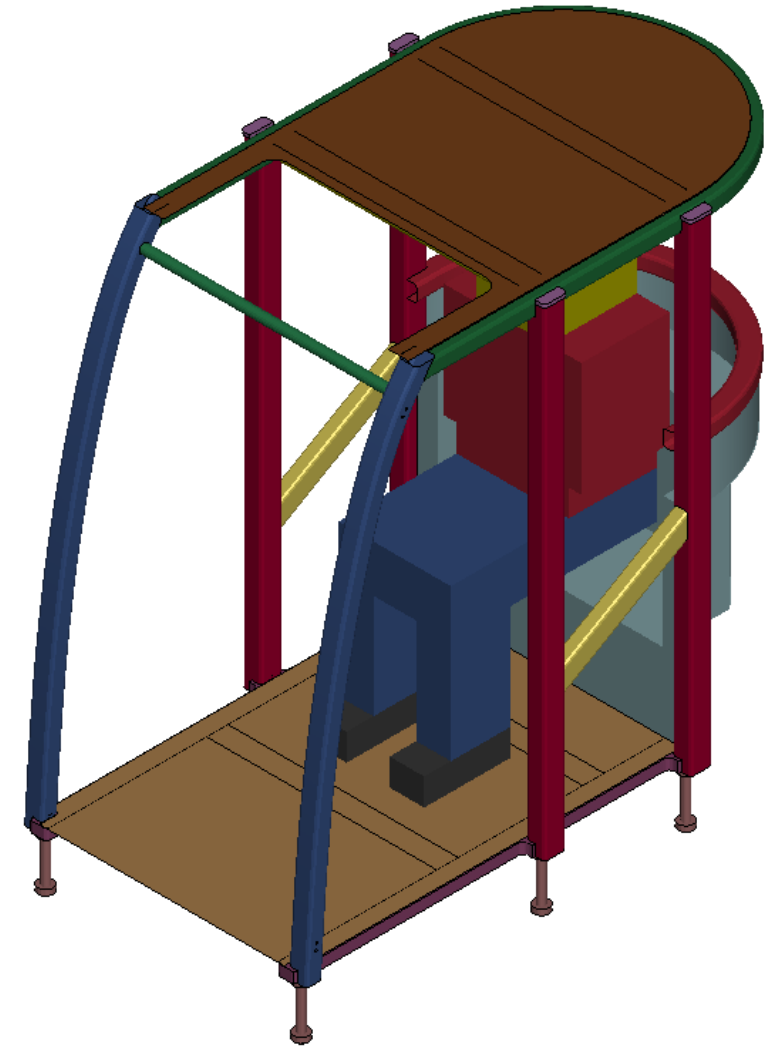
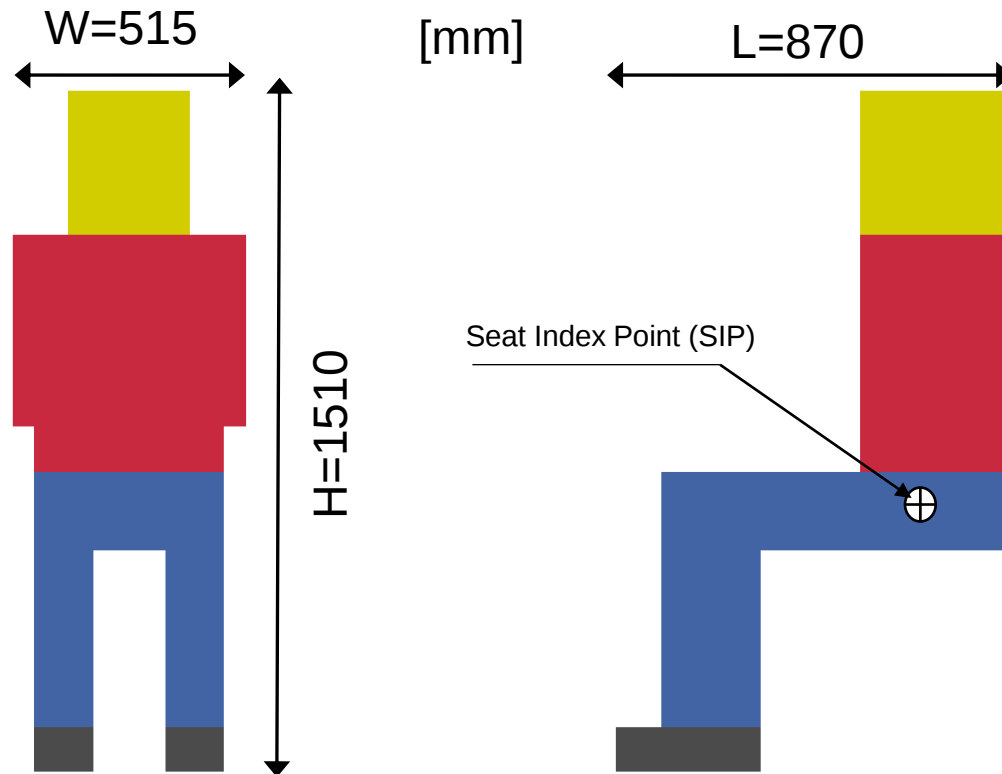
- S480 steel was used for the tubular structural members in green.
- S355 steel was used for the sheet metal and solid parts in purple.
- Steel with 10.9 strength was used for solid bolts.

0:run.key : 190130,ROPS Cab Test 10 - All loading, simple LDD,grabhandle+fundament pretens : ORIGINAL STATE



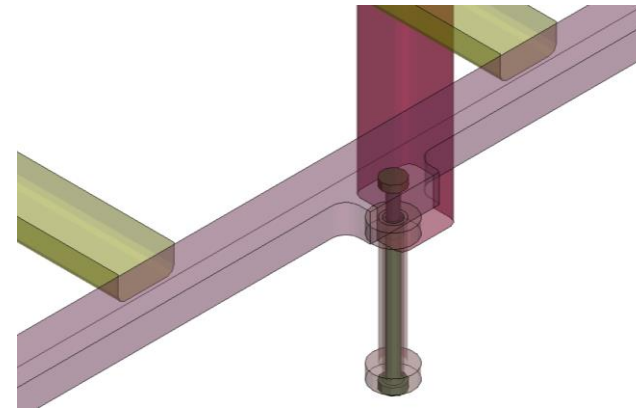
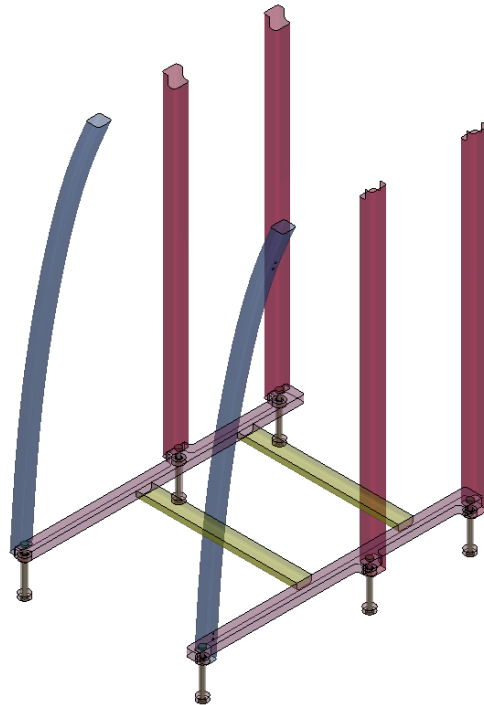
Deflection Limiting Volume (DLV)

- The DLV is based on ISO 3164:1995(E) and represents 'A large, seated, male operator wearing normal clothing and a protective helmet.



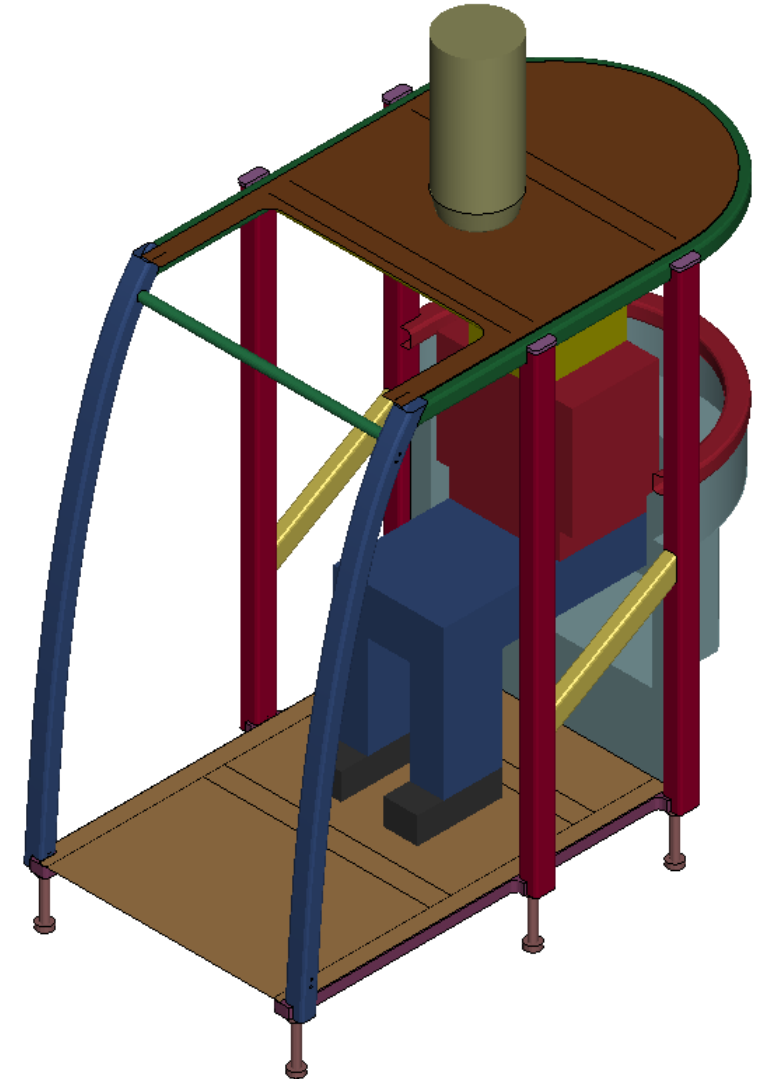
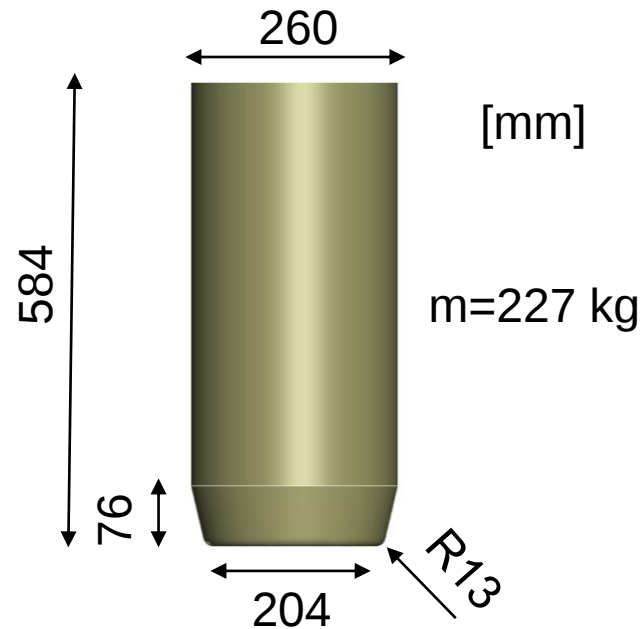
Mounting to a Testbed

- The mounting of the test specimen to a test bed should be the same as when mounted on the machine, and the test bed shall represent the stiffness of the machine.
- The pillars are mounted to the floor of the structure through six long bolts which also connect the structure to the testbed, represented by six rigid fundaments because of the high machine mass.



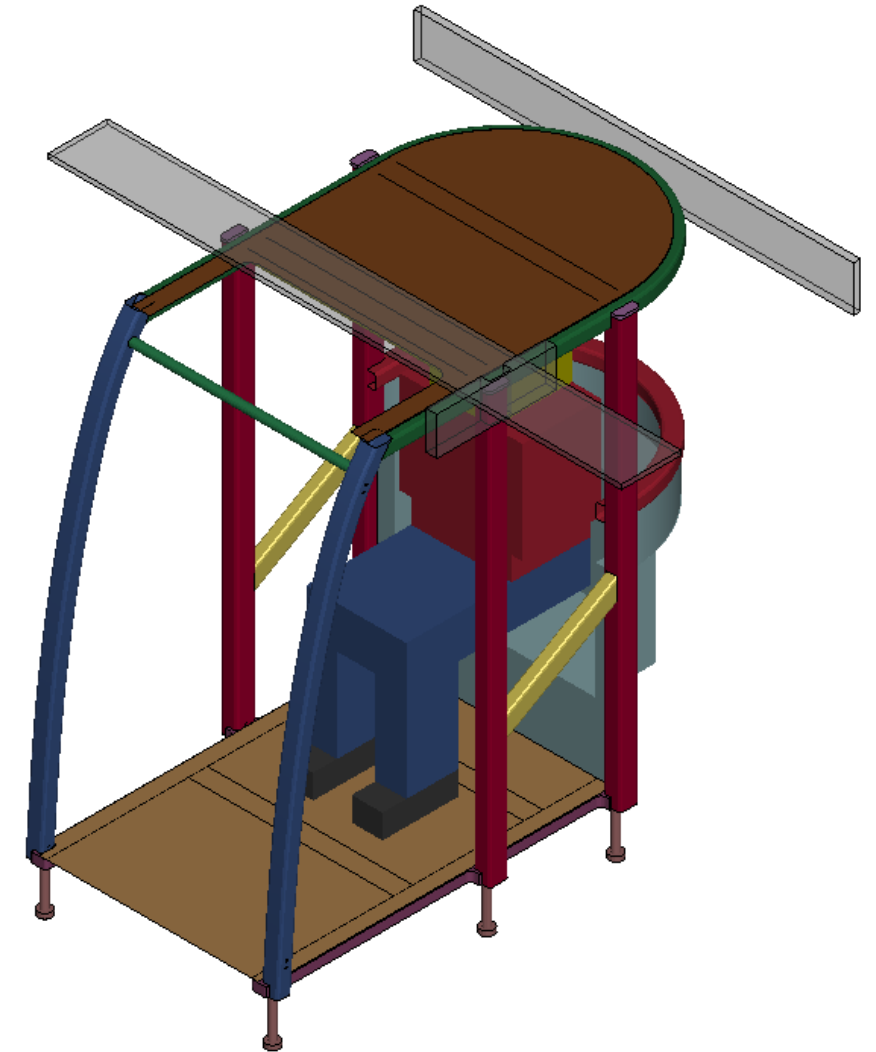
FOPS Test

- Level 2 test object is a solid steel or ductile iron cylinder.
- The mass of the test object determines drop height such that an impact energy of 11 600 J is achieved.
- The typical mass is 227 kg, which results in a drop height of 5.22 m ($g=9.807 \text{ m/s}^2$).
- DLV must not be penetrated.



ROPS Test

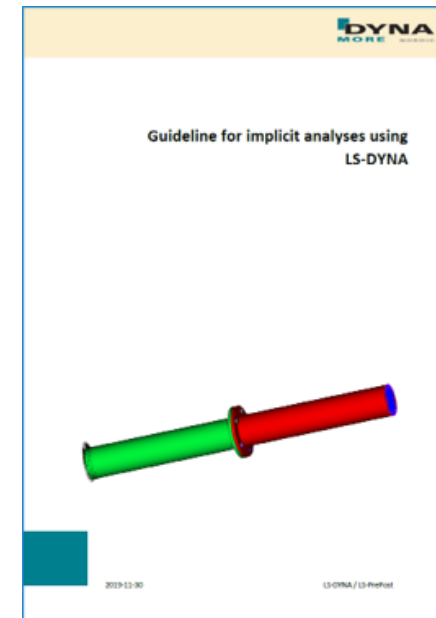
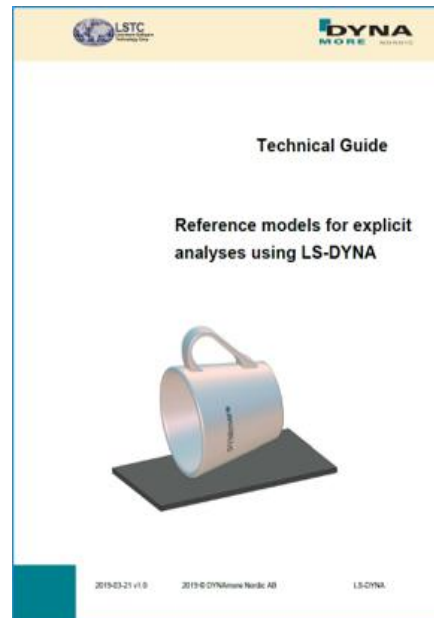
- Loads are applied to the ROPS laterally, vertically, and longitudinally, in sequence, and in a quasi-static manner. Loads are applied through load distribution devices (LDD).
 - 1. Lateral loading and unloading.
 - 2. Vertical loading and unloading.
 - 3. Longitudinal loading and unloading.
- There are force resistance requirements in all three directions as well as an energy absorption requirement in the lateral direction.
- The mass of the machine that the ROPS is mounted on determines the magnitude of force and energy requirements.
- No part of the ROPS is allowed to penetrate the DLV.



- The simulation consists of three stages.
 - 1) Bolt pre-tensioning using dynamic relaxation
 - 2) FOPS test using explicit time integration.
 - Interface springback to save the deformed structure to use in the ROPS test.
 - 3) ROPS test using implicit time integration, set up using cases.

Simulation Strategy – Guidelines

- We at DYNAmore Nordic provide an explicit and an implicit guideline with recommendations, examples, and lots of good information to help you when using the different solvers.
- Together with the guidelines, we provide recommended Control and Database keywords.
- All of this and more is found on our Client Area.

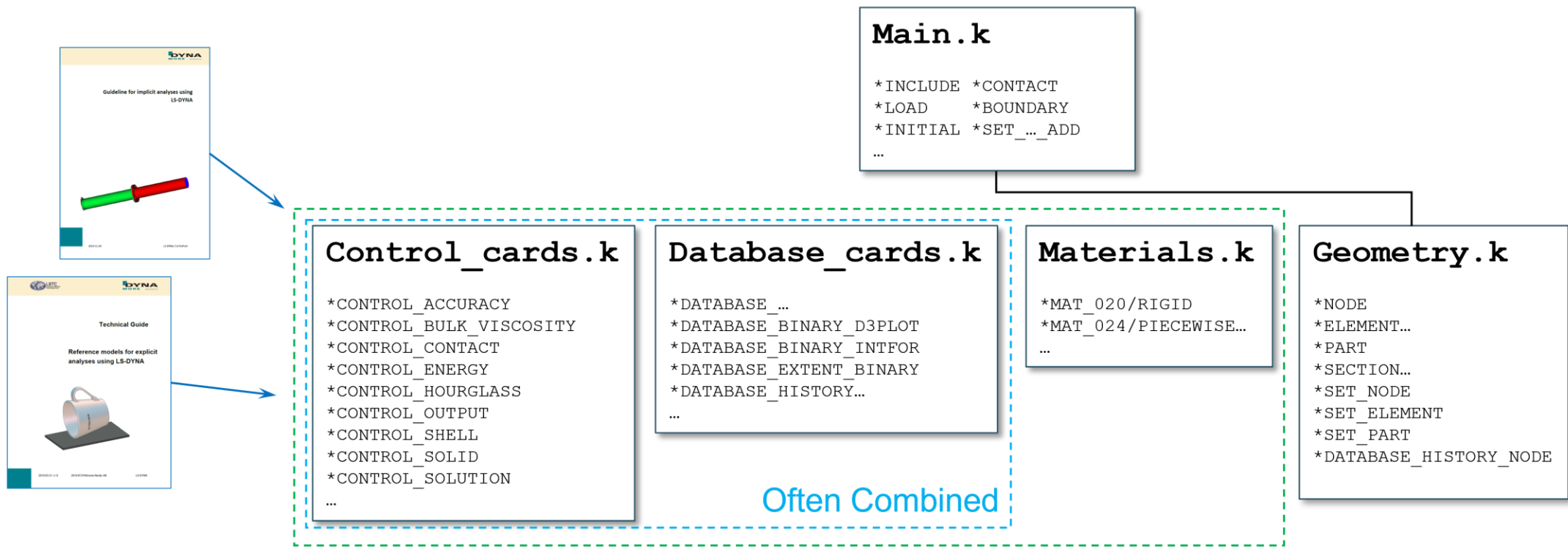


Suggested Modeling Structure



- If you are new to LS-DYNA, consider watching the webinar “*Explicit Model Breakdown*” for a good introduction.
- When modeling a large and complex problem, it is important to have a structured approach.
 - Make use of the keyword *INCLUDE to lift out parts of the model into separate keyword files for improved workability and easier overview.
 - Employ a logical numbering of ID:s by letting imported parts start with distinct numbers, e.g., the element and node ID:s of the test object in the FOPS model start at 1 000 001, and other keywords pertaining to the test object also have the ID 1 000 001.
 - Take the time to document changes that you do, and the effect they have, e.g., changing settings in a contact keyword or changing element formulation.

Suggested Modeling Structure

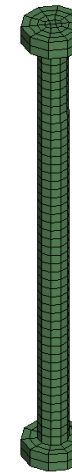
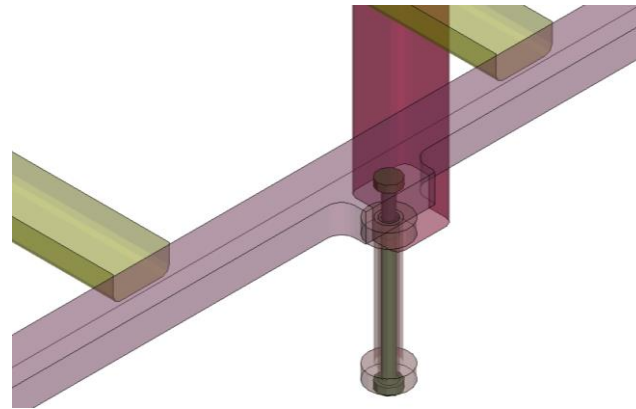
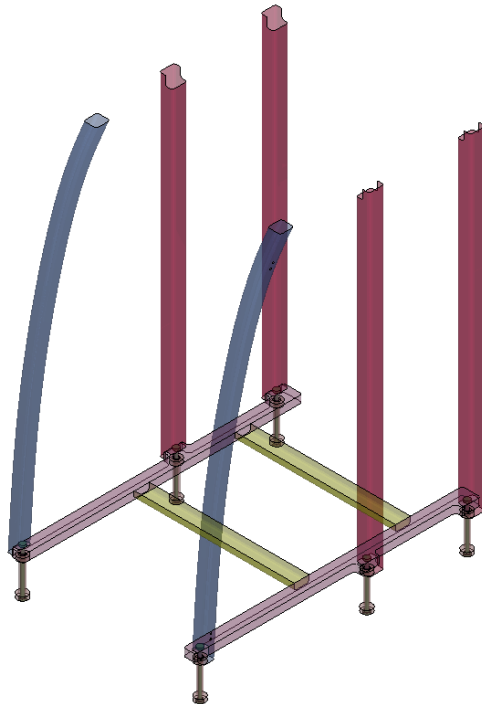


Rarely changed ⇒

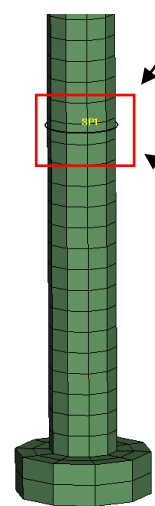
- Few errors are introduced.
- All normal results are always available.
- Prepare settings for different types of analyses.

Bolt Pre-Tensioning – Dynamic Relaxation

- The model contains six long bolts for mounting the structure to the testbed.
- Pre-tensioning takes place in a dynamic relaxation phase preceding the FOPS test.
- See our related webinar “*Pre-Tensioning and Dynamic Relaxation*” on our Client Area.



Bolt Pre-Tensioning – Dynamic Relaxation



***DATABASE_CROSS_SECTION_PLANE**

Keyword Input Form

NewID Draw Pick Add Accept Delete Default Done (Subsys: 1 Main.k) Setting

☐ Use *Parameter ☐ Comment

***INITIAL_STRESS_SECTION (6)**

1	ISSID	CSID	LCID	PSID	VID	IZSHEAR	ISTIFF
	10	10	1	21	0	2	0

COMMENT:

Resistance against shearing and bending

***SET_PART_LIST with all the bolts**

Keyword Input Form

RefBy Add Accept Delete Default Done (Subsys: 1 Main.k) Setting

☐ Use *Parameter ☐ Comment

***DEFINE_CURVE_(TITLE) (5)**

TITLE

Pretension DR

1	LCID	SIDR	SFA	SFO	OFFA	OFFO	DATTYP	LCINT
	1	1	1.0000000	600.00000	0.0	0.0	0	0

Repeated Data by Button and List

2	A1	O1
	0.0	0.0

1	0.0	0.0
2	0.001	1.0
3	0.1	1.0

Data Pt. 1 Load XYData

Replace Insert Plot Raise

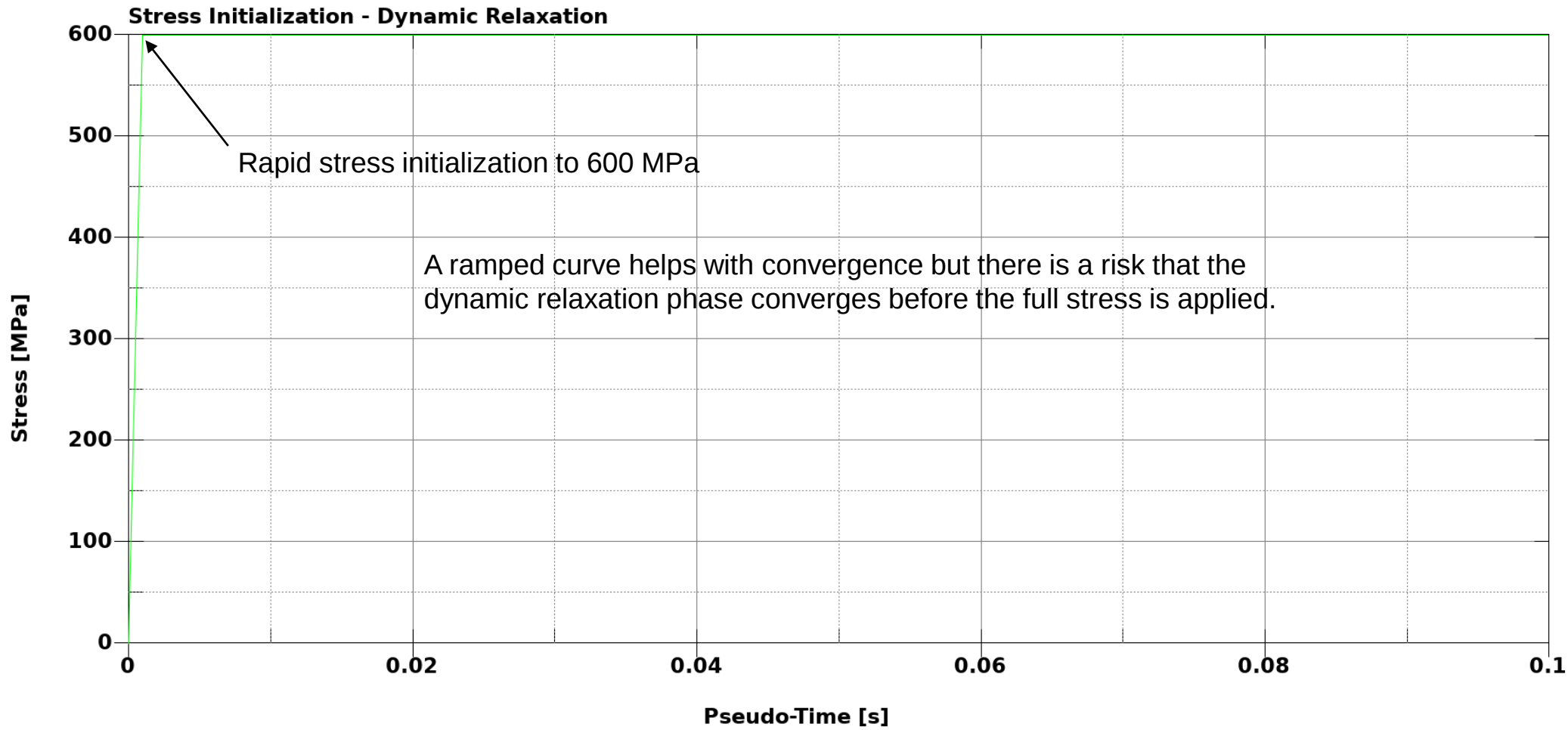
Delete Help New Padd

ChangeXY Copy Paste

Total Card: 5 Smallest ID: 1 Largest ID: 480 Total deleted card: 0

1, only used in dynamic relaxation phase

Bolt Pre-Tensioning – Dynamic Relaxation



Bolt Pre-Tensioning – Dynamic Relaxation

- *DATABASE_BINARY_D3DRLF to receive output during a dynamic relaxation phase in the same way as a normal D3PLOT-file. The user specifies the number of calculation cycles between output states.

Keyword Input Form

☐ Use *Parameter ☐ Comment

(Subsys: 6 Control_cards.k)

*CONTROL_DYNAMIC_RELAXATION (1)

	NRCYCK	DRTOL	DRFCTR	DRTERM	TSSFDR	IRELAL	EDTTL	IDRFLG
1	250	0.0010000	0.9774000	0.0	0.0	0	0.0400000	1

Repeated Data by Button and List

Changed from default value 0.995 to achieve critical damping to speed up convergence.

Data Pt.

Simulation of FOPS Test – Overview



- High-speed, dynamic event → Explicit analysis is suitable.
- First order, under-integrated elements.
- R13.1.1 version of LS-DYNA. Run with single precision.
- The test object is placed close to the point of impact and given an initial velocity rather than simulating free fall.
- The initial velocity of the 227 kg test object dropped from a height of 5.22 m is 10.12 m/s.
- Contact between test object and roof as well as other contacts to hold the structure together.
- Selective mass-scaling to decrease computational cost
- Damping is applied to make the structure still after impact quicker
- Upon termination, the deformed structure is saved by using springback.

Simulation of FOPS Test – Test Object

- The test object is modeled as a rigid body for simplicity and to reduce computational cost.
- For information about how rigid bodies work in LS-DYNA, there is the webinar “*Rigid Bodies in LS-DYNA*”.

Keyword Input Form

1000001 Test object

(Subsys: 3 Test_object.k)

***MAT_RIGID**

*PART_INERTIA_(TITLE) (1)

1 TITLE						
Test object						
2 PID	SECID	MID	EOSID	HGID	GRAV	ADPOPT
1000001	1000001	1000001	0	0	0	0
3 XC	YC	ZC	TM	IRCS	NODEID	
302.75571	0.5630589	2096.5110	0.2270000	0	0	
4 IXX	IYY	IZZ	IYX	IYZ	IZZ	
2.797e+10	-2977.7371	-417.71689	2.797e+10	4935.1992	9.004e+09	
5 VTX	VTY	VTZ	VRX	VRZ		
0.0	0.0	0.0	0.0	0.0	0.0	

Translational mass of 227 kg

Keyword Input Form

1

(Subsys: 1 Main.k)

***INITIAL_VELOCITY_RIGID_BODY** (1)

1 PID	VX	VY	VZ	VXR	VYR	VZR	ICID
1000001	0.0	0.0	-1.012e+04	0.0	0.0	0.0	0

10 m/s

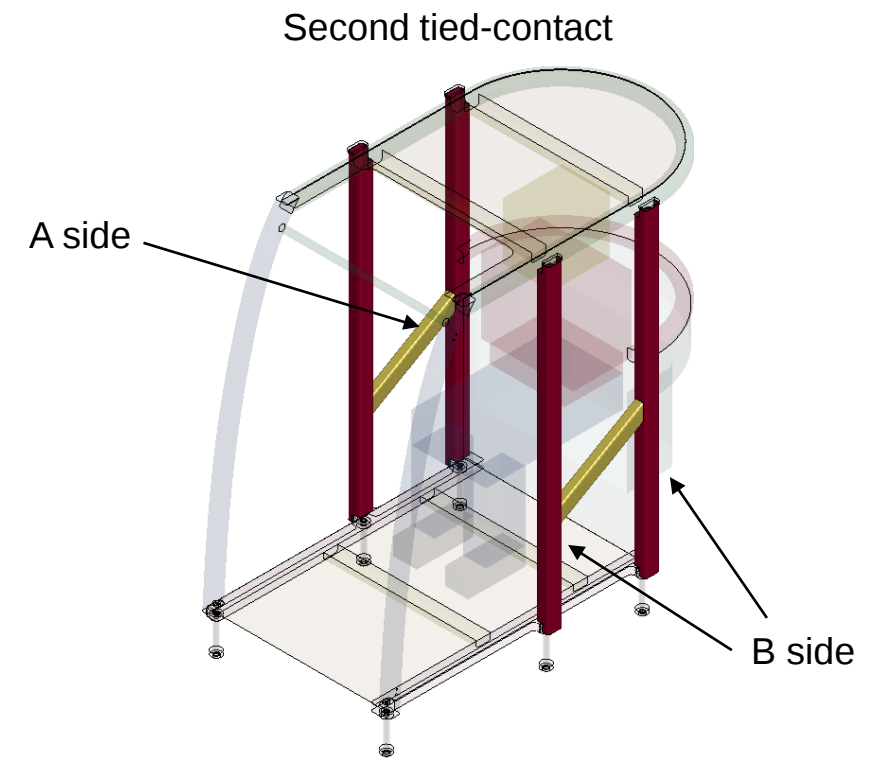
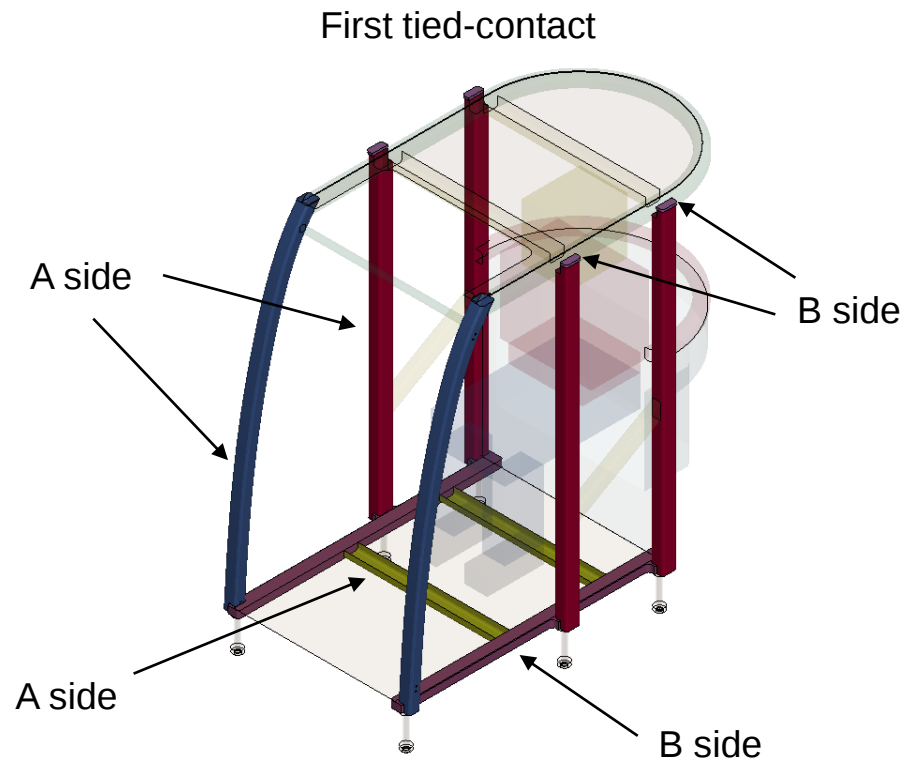
Simulation of FOPS Test – Contacts



- Without any contact algorithms, the test object would just pass through the cab, and it would be difficult to get achieve connectivity for the whole structure.
- We have a webinar on “*Tied and Tiebreak Contacts in Explicit Simulation*”.
- Additionally, the upcoming webinar in two weeks by Jimmy Forsberg will be about contacts in explicit analyses.

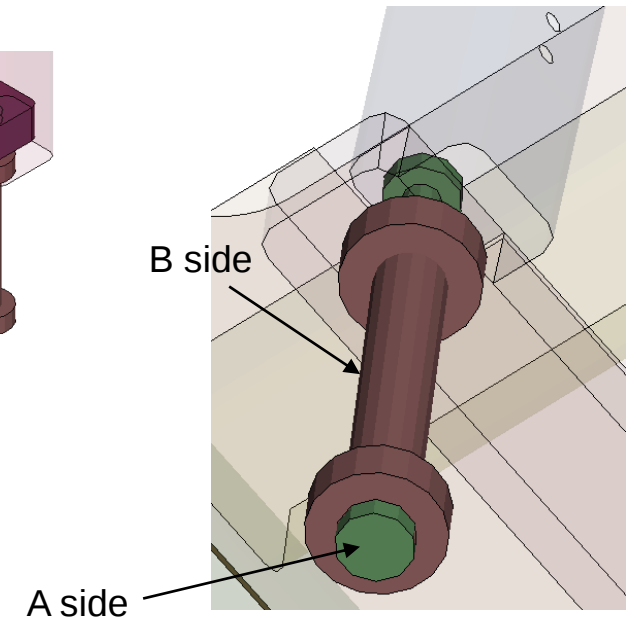
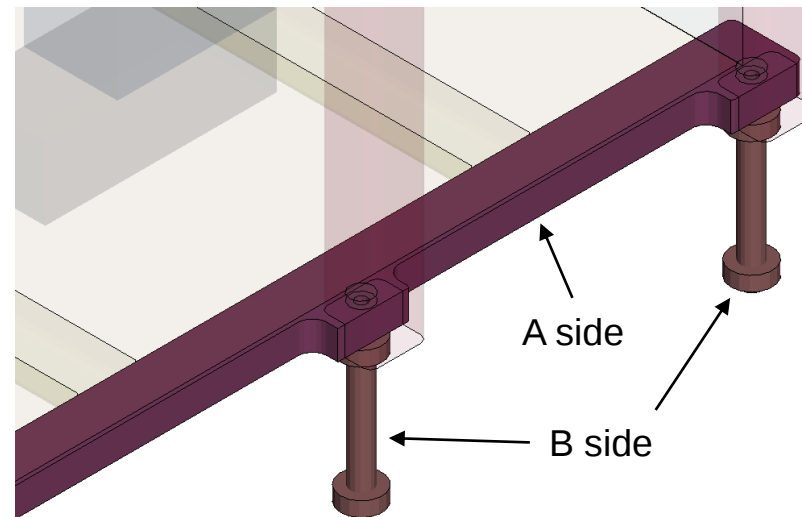
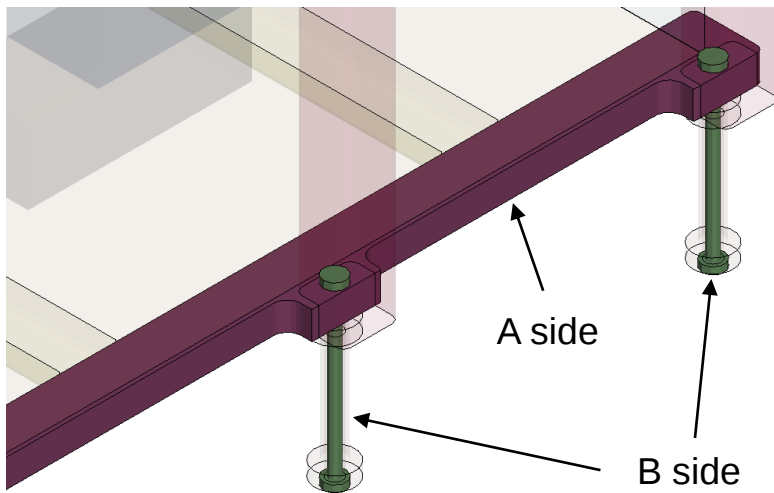
Simulation of FOPS Test – Contacts

- *CONTACT_TIED_SHELL_EDGE_TO_SURFACE_OFFSET is used for the tied contacts. The addition of OFFSET changes from a constraint formulation to a penalty formulation.



Simulation of FOPS Test – Contacts

- *CONTACT_AUTOMATIC_SURFACE_TO_SURFACE is used for standard contacts. Settings are taken from the Explicit Guideline.
- One contact between test object and the rest of the model. Another contact between DLV and the cab to check for penetration of the DLV.
- In addition, there are three contacts involving the floor, bolts, and fundamentals.



Simulation of FOPS Test – Mass Scaling



- There are parts in the model with solid elements which results in a low critical time-step. To reduce computational cost, one can use mass-scaling.
- There is information about mass-scaling in the webinar “*Mass-Scaling and Subcycling in LS-DYNA*”.

Simulation of FOPS Test – Mass Scaling



Keyword Input Form

☐ Use *Parameter ☐ Comment

Desired time-step, set to negative

(Subsys: 6 Control_cards.k) Setting

1	DTINIT	TSSFAC	ISDO	TSLIMIT	DT2MS	LCTM	ERODE	MS1ST
	0.0	0.9	0	0.0	-1.000e-06	0	0	0

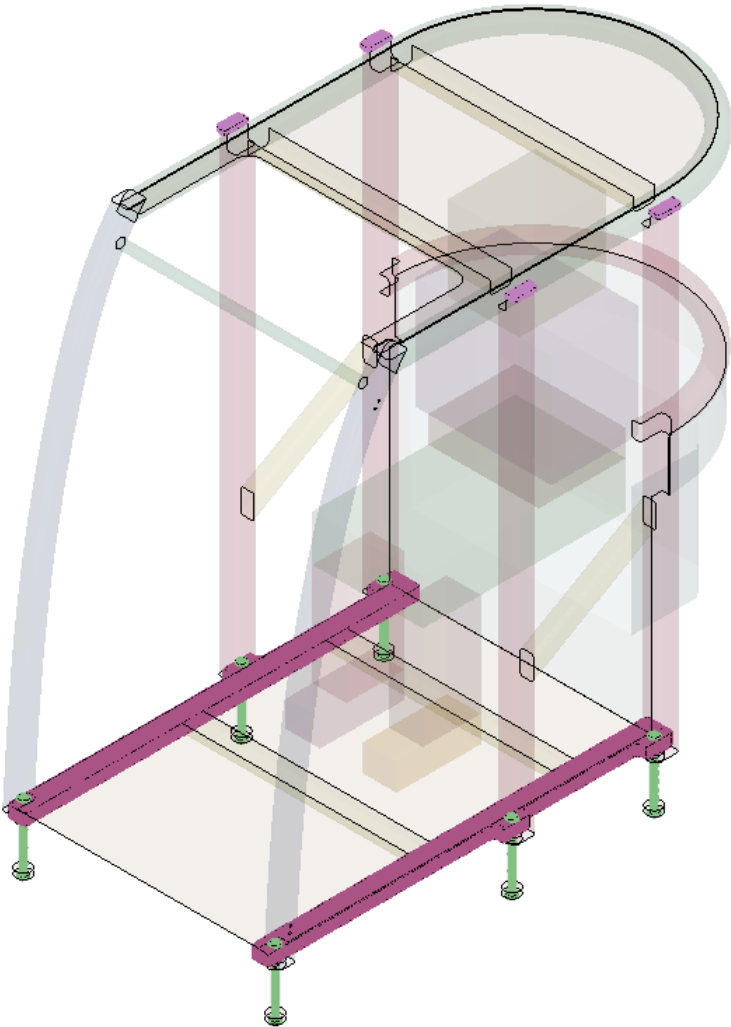
Active optional cards
☐ None ☒ Opt1 ☐ Opt12

2	DT2MSF	DT2MSLC	IMSCL	UNUSED	UNUSED	RMSCL	EMSCL	IHDO
	0.0	0	-31			0.0	0.0	0

3	IGADO	DTUSR
	0	

Activates selective mass-scaling.
Negative value indicates part set.

*SET_PART_LIST of solid parts that receive selective mass-scaling. Other parts receive conventional mass-scaling.



Simulation of FOPS Test – Damping



- The impact from the test object induces vibrations in the structure, and there are no natural damping effects such as surrounding air or internal losses in the material. To obtain a structure at equilibrium within a reasonable simulation time, damping is introduced.
- There is information about damping in the webinar “*Damping in Explicit LS-DYNA*”.
- *DAMPING_GLOBAL is used which is mass weighted damping.
 - A load curve is used to turn the damping on at an appropriate time and to decide damping coefficient.
 - To achieve critical damping, the coefficient is set to $2\pi\omega_{min}$, where ω_{min} is the lowest angular frequency mode of interest.

Simulation of FOPS Test – Damping

Keyword Input Form

Accept Delete Default Done
(Subsys: 1 Main.k) Setting

☐ Use *Parameter ☐ Comment

*DAMPING_GLOBAL (1)

1	LCID	VALDMP	STX	STY	STZ	SRX	SRY	SRZ
	10	0.0	0.0	0.0	0.0	0.0	0.0	0.0

COMMENT:

Keyword Input Form

NewID Draw RefBy Add Accept Delete Default Done
(Subsys: 1 Main.k) Setting

☐ Use *Parameter ☐ Comment

*DEFINE_CURVE_(TITLE) (5)

TITLE
Damping

1	LCID	SIDR	SFA	SFO	OFFA	OFFO	DATTYP	LCINT
	10	0	1.0000000	1047.2000	0.0	0.0	0	0

Repeated Data by Button and List

2	A1	O1
	0.0	0.0

1	0.0	0.0
2	0.05	0.0
3	0.055	1.0
4	0.15	1.0

Data Pt. 1 Load XYData

Replace Insert Plot Raise

Delete Help New Padd

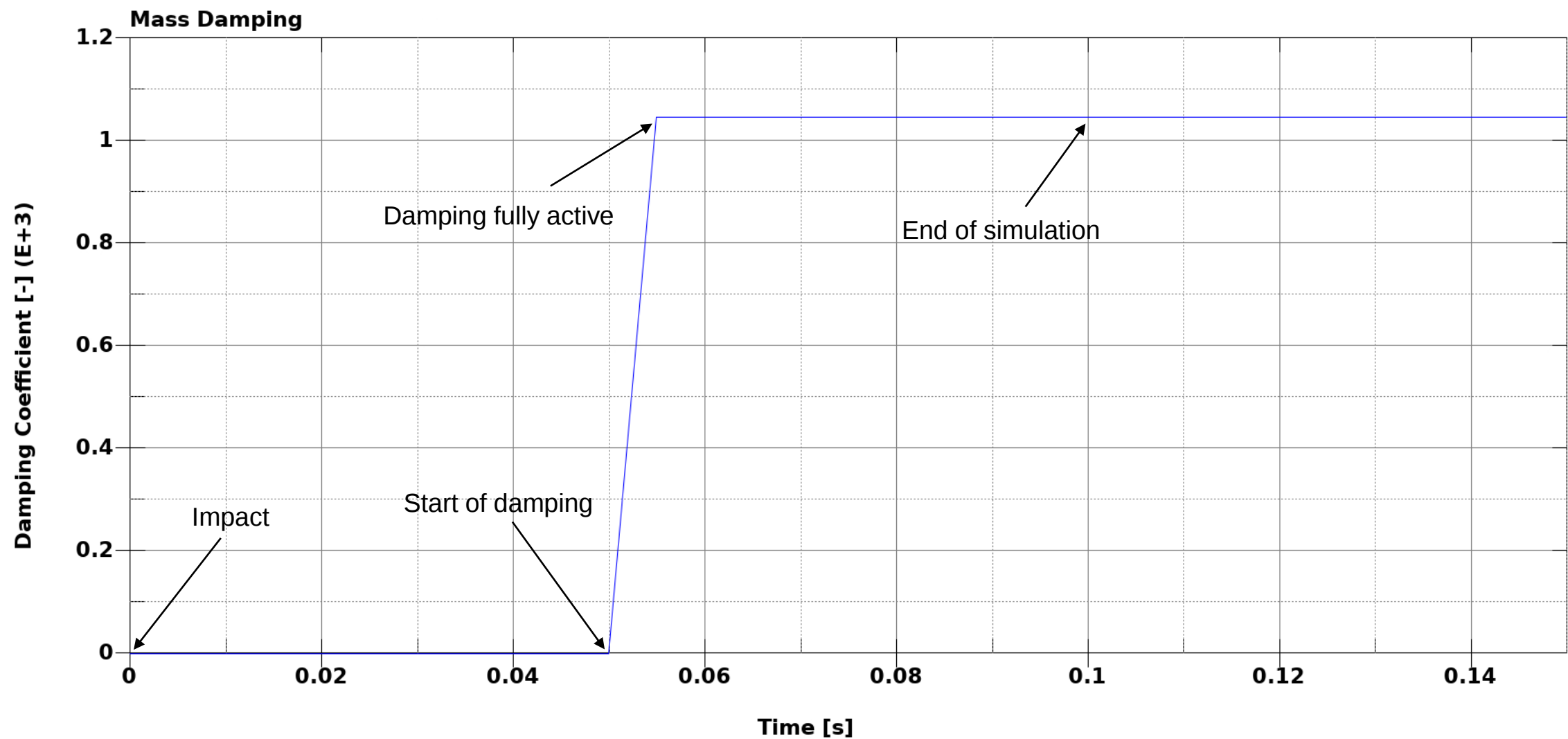
ChangeXY Copy Paste

Total Card: 5 Smallest ID: 1 Largest ID: 480 Total deleted card: 0

0, only used in transient analysis

1 Pretension DR
10 Damping
20 Hardening curve 1
355 Hardening curve
480 Hardening curve

Simulation of FOPS Test – Damping



Simulation of FOPS Test – Springback

- The purpose of adding “Springback” to the simulation is that this causes LS-DYNA to, upon termination, write the final state of the system to an output file so that the results can be used as input for another subsequent analysis.
- The name springback is due to historical reasons since this was implemented in the context of metal forming but is in no way limited to such types of analyses.

*SET_PART_LIST
containing all parts
that are to be
outputted. In this
case, the test
object is excluded.

Keyword Input Form

NewID Pick Add Accept Delete Default Done 1

☐ Use *Parameter ☐ Comment (Subsys: 1 Main.k) Setting

*INTERFACE_SPRINGBACK_LSDYNA (1)

1	PSID	NSHV	ETYPE	:	FTENSR	NTHHSV	RFLAG	INTSTRN
	51	0	3		0	0	0	0

☐ OPTC

2	OPTC	SLDQ	NCYC	FSPLIT	NDFLAG	CFLAG	HFLAG
		0		0	0	0	

Repeated Data by Button and List

3	NID	TC	RC
		0	0

Set to 3 for LSDA format. A file called dynain.lsda is created.

Data Pt.
Replace Insert
Delete Help

Simulation of ROPS Test – Overview



- Slow, quasi-static event → Implicit analysis is suitable.
- First order, fully-integrated elements.
- R13.1 version of LS-DYNA. Run with double precision.
- Load distribution devices in three directions are prescribed displacements in sequence.
- Three simulations are run in sequence using the *CASE logic.
- Contact between LDDs and cab as well as other contacts to hold the structure together.

Simulation of ROPS Test – Implicit Guideline



- The implicit guideline has already been mentioned, but there is also a webinar “*Guideline for Implicit Analysis*”, where my colleague Anders Jonsson goes through some details.

Simulation of ROPS Test – Explicit to Implicit



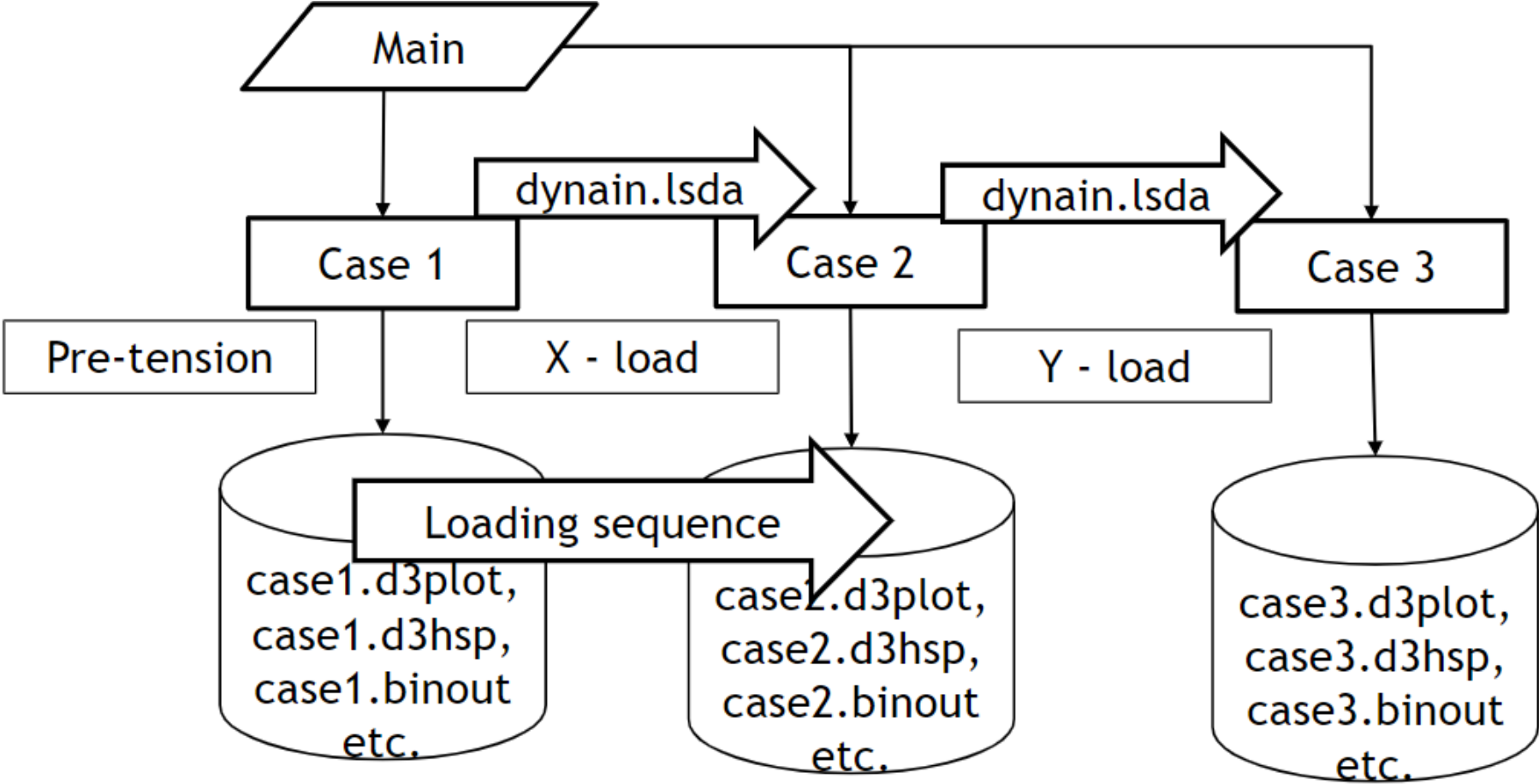
- There is a webinar on our Client Area titled “*From Explicit to Implicit Simulation Models*” which deals with the considerations one must take when moving between the two solvers.
- In addition, there is an upcoming webinar in four weeks which my colleague Anders Jonsson will give on the topic of Explicit/Implicit Switching.
- For this case, there was not a lot of problems associated with going from an explicit model to an implicit model, but in general there are a few things that one needs to keep in mind.
 - When doing explicit analyses, you can generally get away with modeling practices of questionable nature to a higher extent than when doing implicit analyses, i.e. explicit analysis is more forgiving.
 - Connectivity is crucial for implicit analysis. While an explicit analysis may work fine even with parts of the model hanging freely, this might hinder convergence in an implicit context.
 - For a more detailed explanation, please see the referenced webinars.

Simulation of ROPS Test – *CASE



- You can use the *CASE logic when setting up a simulation with several steps in sequence to split up the analysis into smaller parts for easier workability.
 - The *CASE concept offers an intuitive way of setting up a load history.
 - It gives a clear definition of which features that are active in each step.
 - It reduces the need for birth/death times for contacts, boundary conditions et cetera.
- Our webinar on the topic is called *“Load History Management”*.

Simulation of ROPS Test – *CASE



Simulation of ROPS Test – *CASE

Cases.k

```
1 $LSPrePost Multiphysics Solution CASE FILE
2 *KEYWORD
3 *CASE
4     1lateral
5
6 1
7 *CASE
8     2vertical
9
10 2
11 *CASE
12     3longitudinal
13
14 3
15 *CASE_BEGIN_1
16 *INCLUDE
17 lateral.k
18 *CASE_END_1
19 *CASE_BEGIN_2
20 *INCLUDE
21 vertical.k
22 *CASE_END_2
23 *CASE_BEGIN_3
24 *INCLUDE
25 longitudinal.k
26 *CASE_END_3
27 *END
28
```

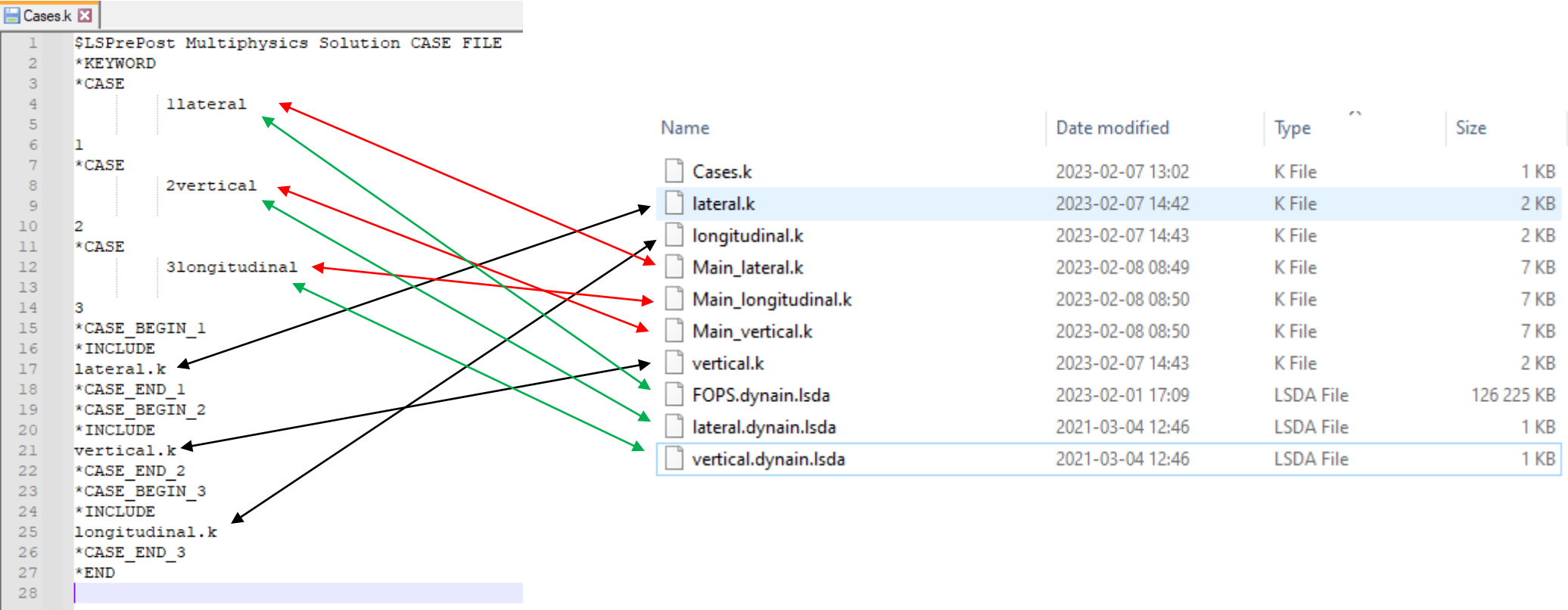
lateral.k

```
1 $$ LS-DYNA Keyword file created by LS-PrePost(R) V4.10 (Beta)-30Jan2023
2 $$ Created on Feb-7-2023 (12:56:09)
3 *KEYWORD
4 *CONTROL_TERMINATION
5 $$ endtim endcyc dtmin endeng endmas nosol
6     20.0      0      0.0      0.01.000000E8      0
7 *INTERFACE_SPRINGBACK_LSDYNA
8 $$ psid nshv ftype - ftensr nthhsv rflag intstrn
9     20     9999      3      0      0      1      0
10 $$ optc sldo ncyc fsplit ndflag cflag hflag
11 OPTCARD      0      0      0      0      1      1
12 *INCLUDE
13 $$
14 Main_lateral.k
15 *INCLUDE
16 $$
17 FOPS.dynain.lsd
18 *SET_PART_LIST_TITLE
19 Springback
20 $$ sid da1 da2 da3 da4 solver
21     20  0.0  0.0  0.0  0.0MECH
22 $$ pid1 pid2 pid3 pid4 pid5 pid6 pid7 pid8
23     3     4     5     6     7     8     9    10
24    11    12    14    15    16    19    20    22
25 2000008 2000001 2000002 2000003 2000004 2000005 2000006 2000007
26 *END
27
```

File containing everything, geometry, materials, loads..

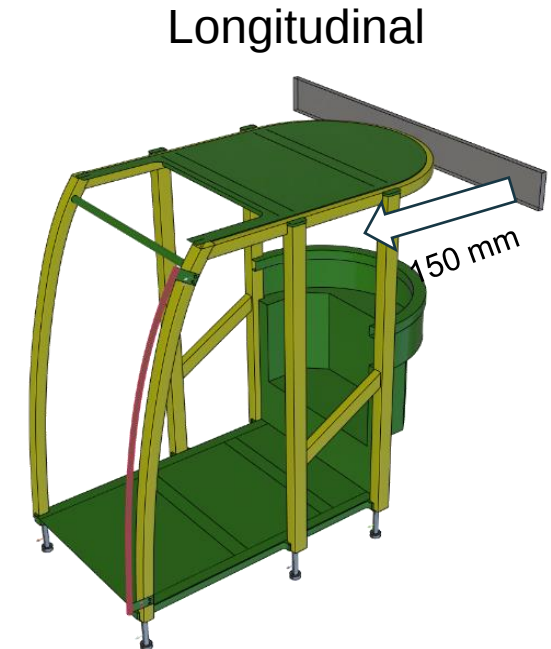
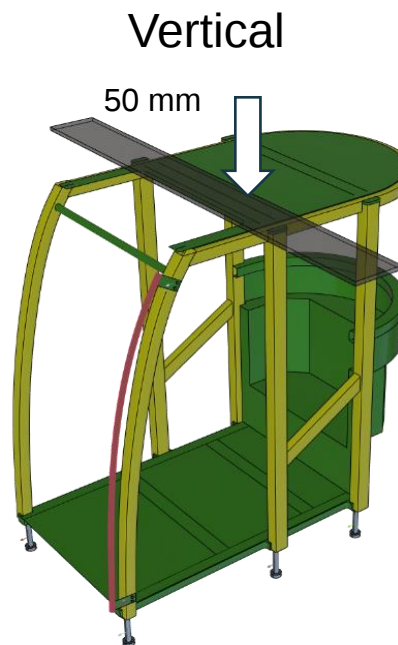
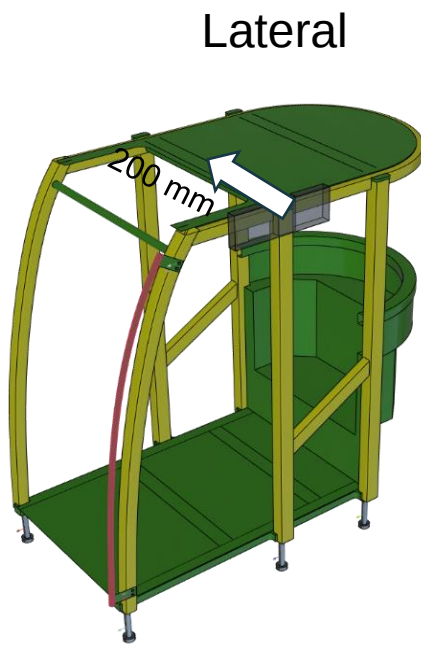
dynain.lsd file from previous analysis.
In this case the FOPS simulation.

Simulation of ROPS Test – *CASE



Simulation of ROPS Test – Loading

- In a ROPS test, the loading is applied in a quasi-static manner through load distribution devices.
- The LDD:s are rigid bodies and have all except one degree of freedom constrained.
- The LDD:s are given prescribed displacements of 200 mm, 50 mm, and 150 mm.



Simulation of ROPS Test – Loading

Generic steel properties for reasonable contact behaviour

Keyword Input Form

MatDB RefBy Pick Add Accept Delete Default Done

(Subsys: 4 Materials.k) Setting

*MAT_RIGID_(TITLE) (5)

TITLE

LDD lateral

1	MID	RO	E	PR	N	COUPLE	M	ALIAS
	201	7.800e-09	2.100e+05	0.3000000	0.0	0	0.0	
2	CMO	CON1	CON2					
	1.0	6	7					
3	LCO OR A1	A2	A3	V1	V2	V3		
	0.0	0.0	0.0	0.0	0.0	0.0		

COMMENT:

Places a constraint on the center of mass of the rigid body.

Constraints on translational DOF:s. 6 = constrained x and z displacements

Constraints on rotational DOF:s. 7 = constrained x, y, and z rotations

Simulation of ROPS Test – Loading

2 indicates displacement

2 indicates y translation

The value of curve 201 is scaled with a factor -200, meaning 200 mm in the negative direction

Keyword Input Form

RefBy Pick Add Accept Delete Default Done 1 LDD lateral

☐ Use *Parameter ☐ Comment (Subsys: 2 Main_lateral.k) Setting

*BOUNDARY_PRESCRIBED_MOTION_RIGID(ID) (1)

ID	TITLE	PID	DOF	VAD	LCID	SF	VID	DEATH	BIRTH
0	LDD lateral								
1		201	2	2	201	-200.00000	0	1.000e+28	0.0
2		OFFSET1	OFFSET2	LRB	NODE1	NODE2			
		0.0	0.0	0	0	0			

COMMENT:

Keyword Input Form

RefBy Add Accept Delete Default Done 20 Hardening curve 1 201 LDD lateral 355 Hardening curve 480 Hardening curve 700 Time step

☐ Use *Parameter ☐ Comment (Subsys: 2 Main_lateral.k) Setting

*DEFINE_CURVE(TITLE) (5)

TITLE	LCID	SIDR	SEA	SFO	OFFA	OFFO	DATTYP	LCINT
LDD lateral								
1	201	0	1.0000000	1.0000000	0.0	0.0	0	0

Repeated Data by Button and List

A1	O1
0.0	0.0

1	0.0	0.0
2	10.0	1.0
3	20.0	0.0

Data Pt. 1 Load XYData

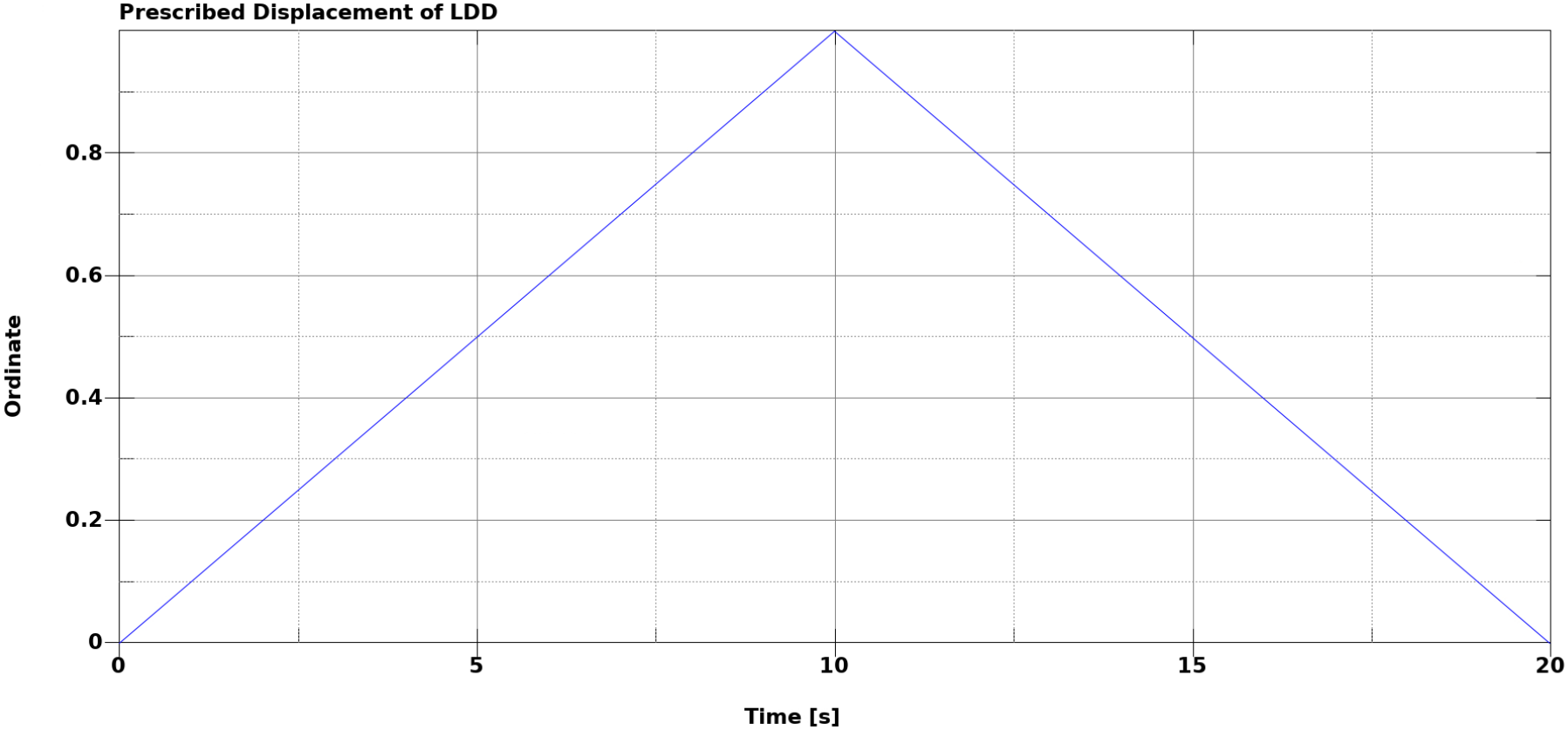
Replace Insert Plot Raise

Delete Help New Padd

ChangeXY Copy Paste

Total Card: 5 Smallest ID: 20 Largest ID: 700 Total deleted card: 0

Simulation of ROPS Test – Loading

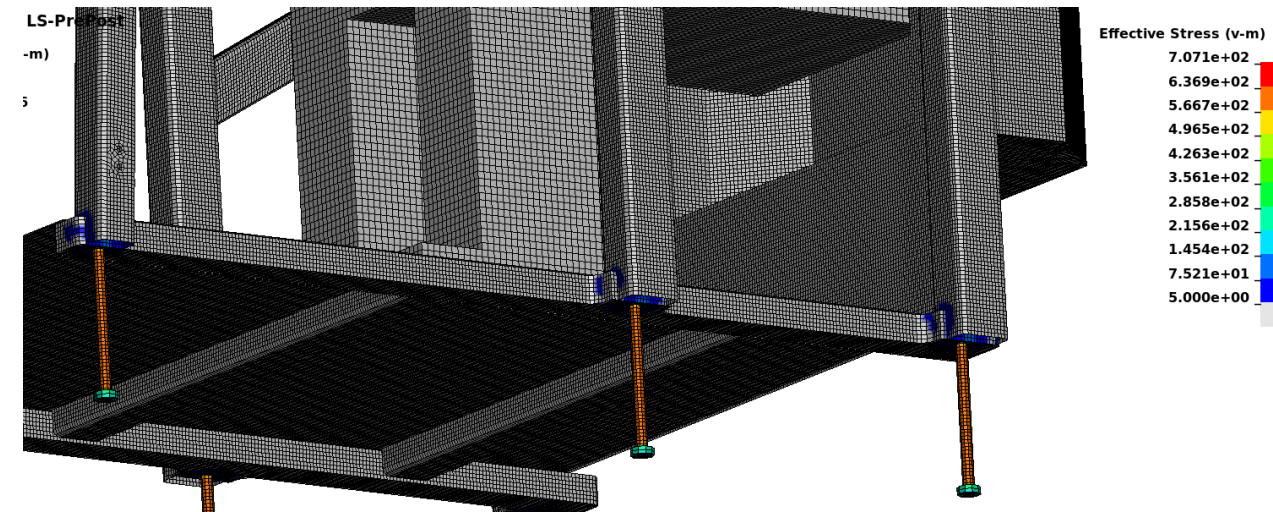
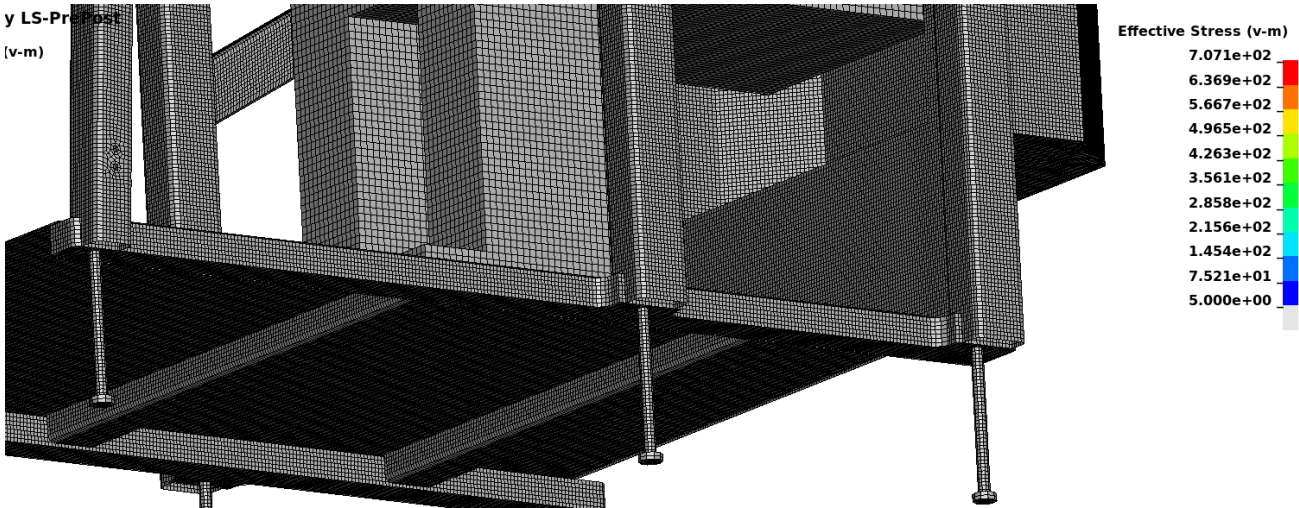


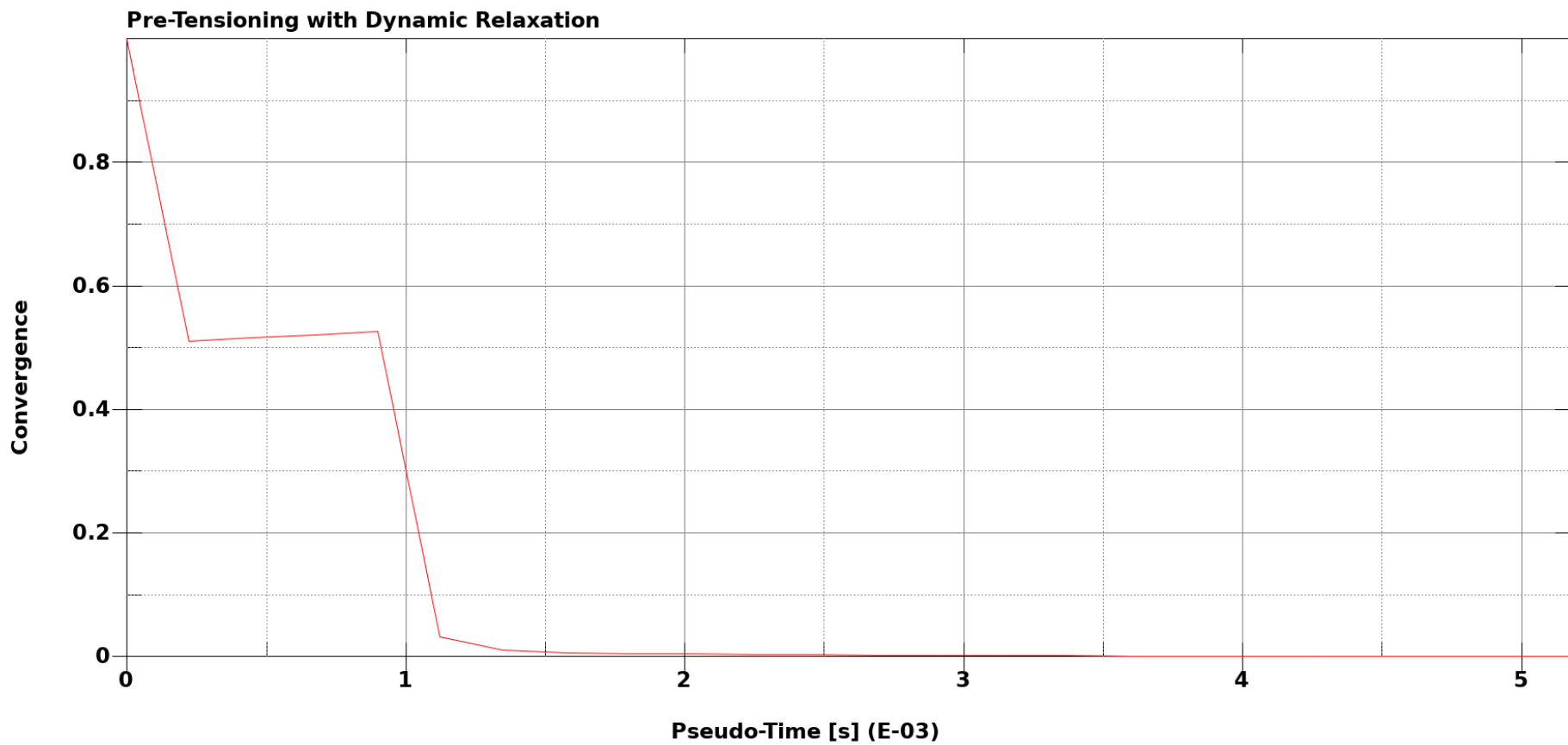
Simulation of ROPS Test – Contacts



- The ROPS test has the same contacts as the FOPS test except that *CONTACT_AUTOMATIC_SURFACE_TO_SURFACE_MORTAR is used.
- Additionally, there are contacts between the respective LDDs and the cab structure.
- Using Mortar type contacts allows information about contacts to be written to the dynain.lsda file between cases.

Results – Pre-Tensioning

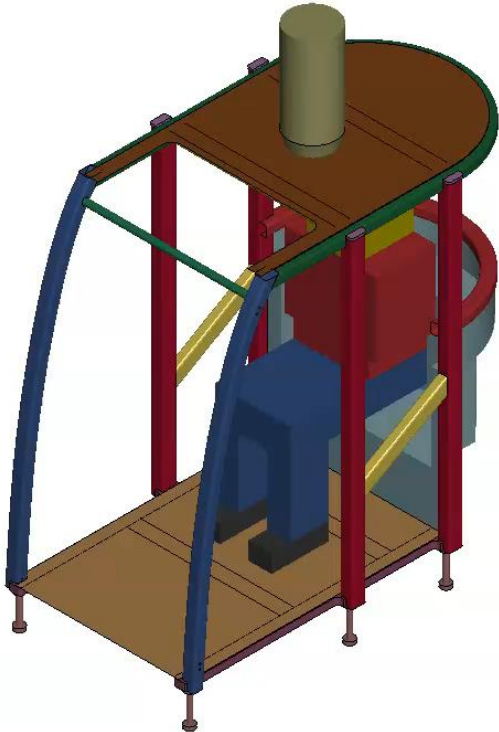




Results – FOPS Simulation



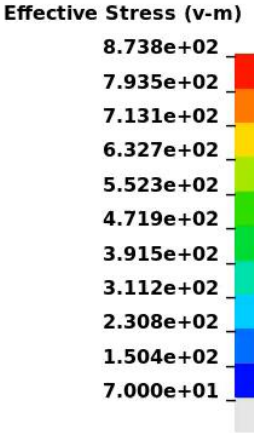
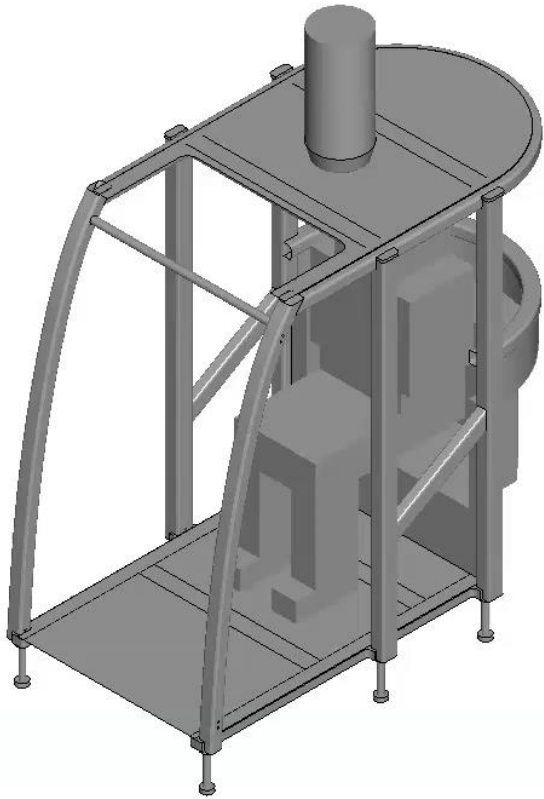
LS-DYNA keyword deck by LS-PrePost
Time = 0



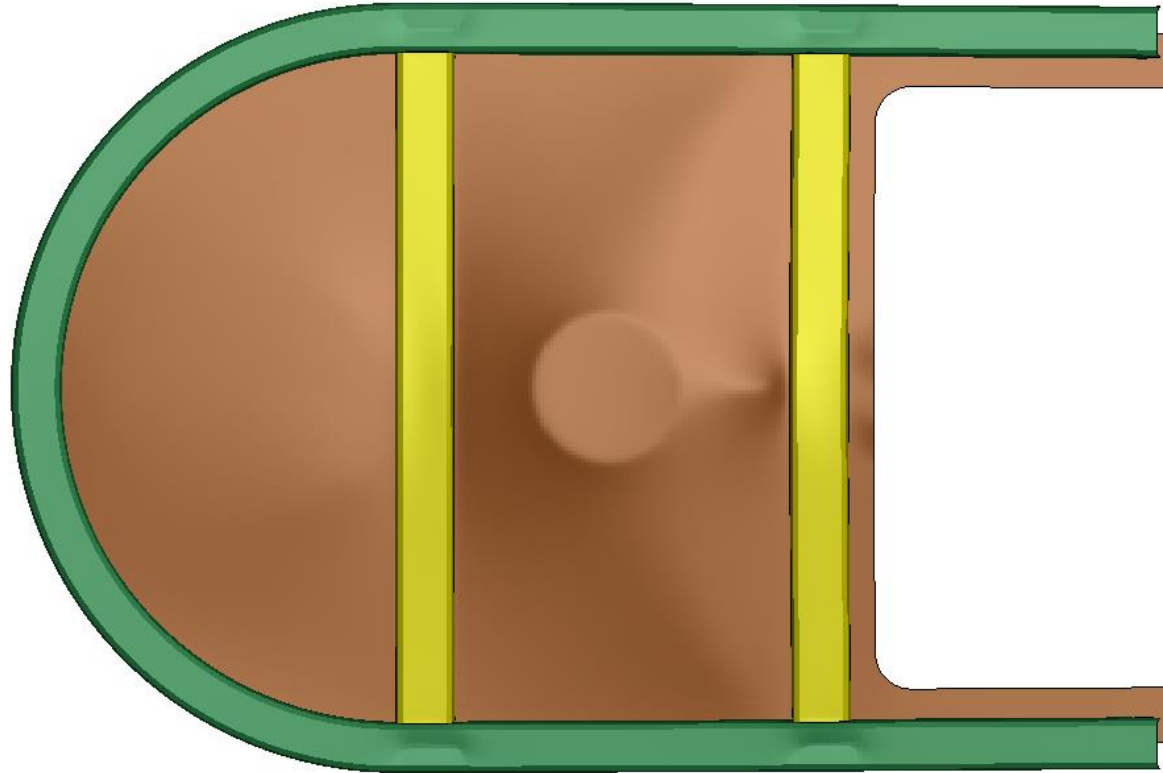
Results – FOPS Simulation



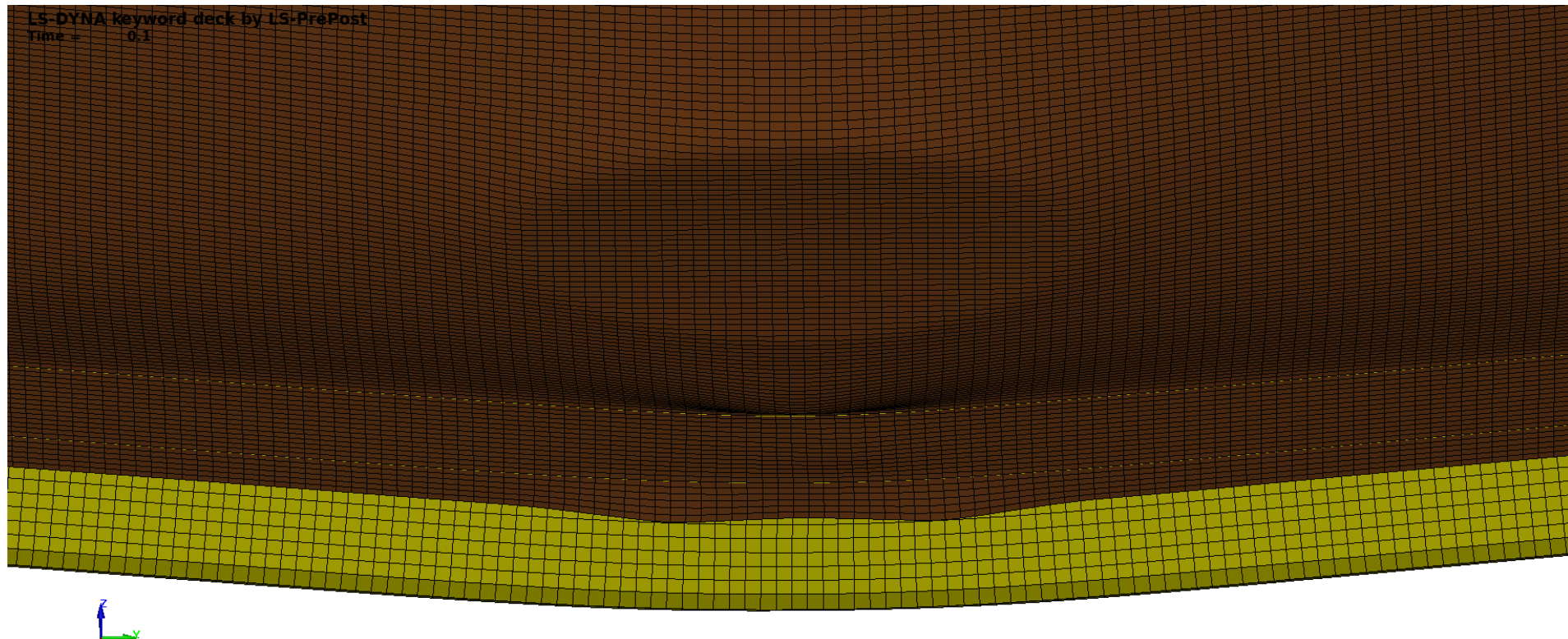
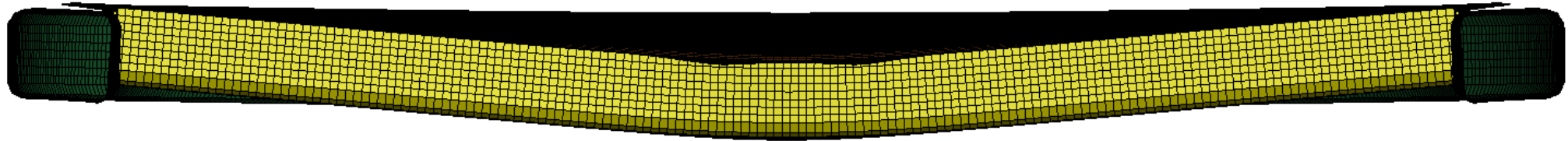
LS-DYNA keyword deck by LS-PrePost
Time = 0
Contours of Effective Stress (v-m)
max IP. value
min=0, at elem# 58099
max=707.118, at elem# 384226



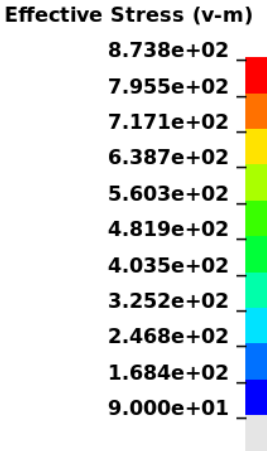
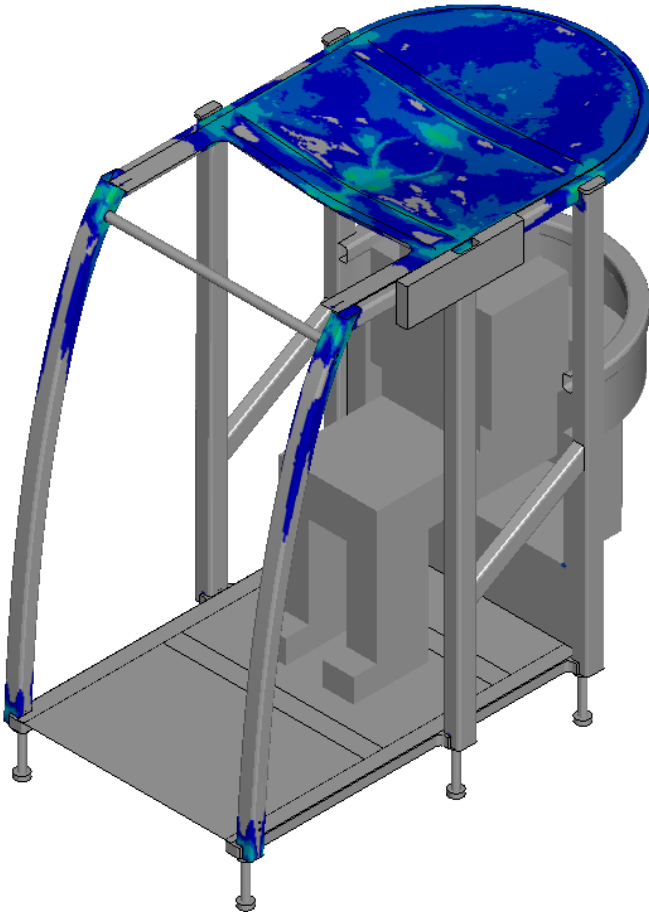
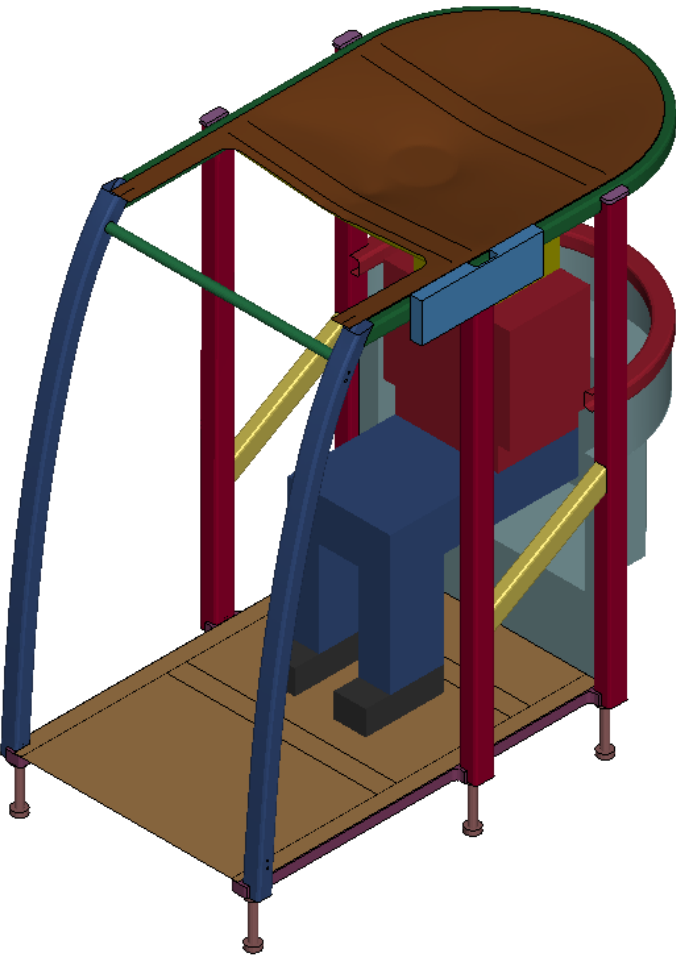
Results – FOPS Simulation



Results – FOPS Simulation

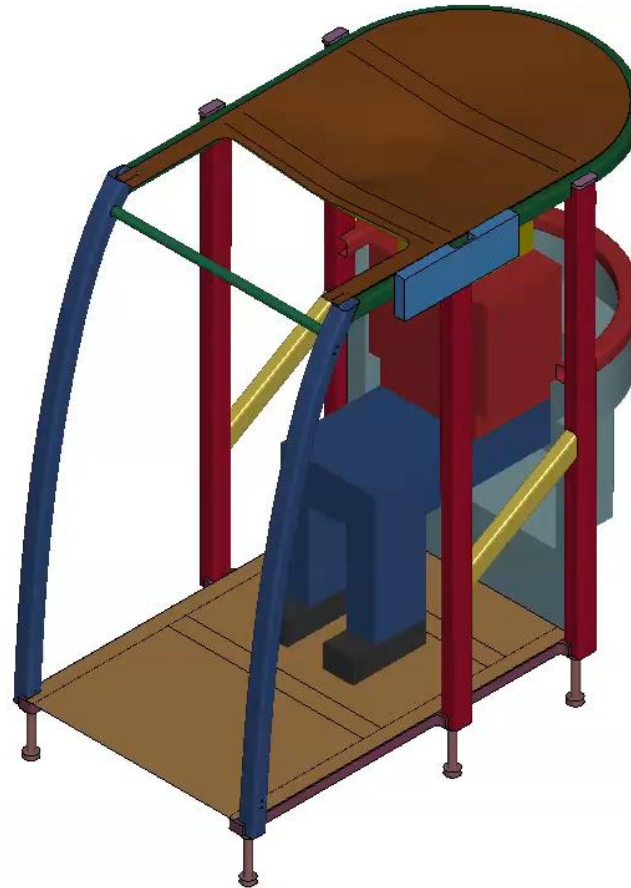


Results – ROPS Simulation



Results – ROPS Simulation

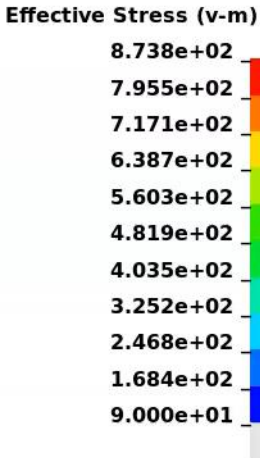
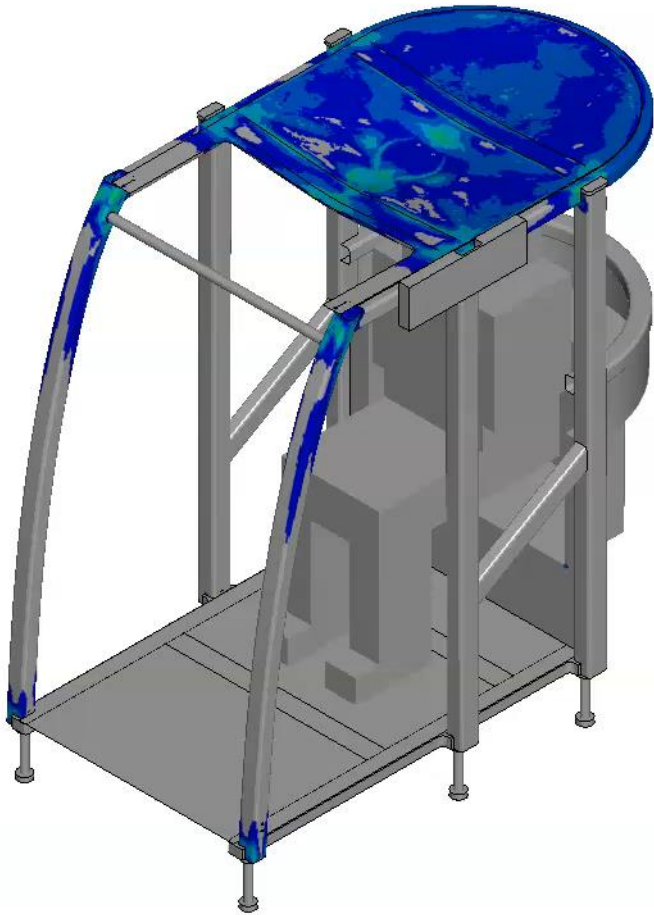
LS-DYNA keyword deck by LS-PrePost
Time = 0



Results – ROPS Simulation



LS-DYNA keyword deck by LS-PrePost
Time = 0
Contours of Effective Stress (v-m)
max IP. value
min=0, at elem# 58099
max=873.841, at elem# 387259

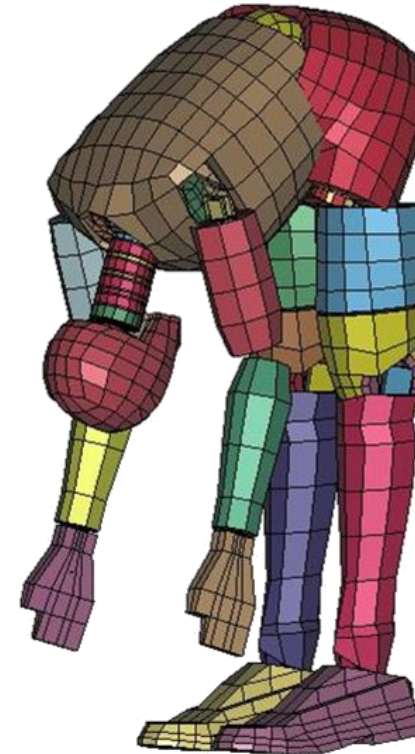


Results – ROPS Simulation

0:Z_cprd3plot : 1900201ROPS Cab Test 11-All loading,simple LDD,grabhandle+fundament pret : STATE 2 ,TIME 1.00000000E+01



Thank You



DYNAMore Nordic AB
Brigadgatan 5
587 58 Linköping, Sweden

Tel.: +46 - (0)13 23 66 80
info@dynamore.se

www.dynamore.se
www.dynaexamples.com
www.dynasupport.com
www.dynalook.com

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