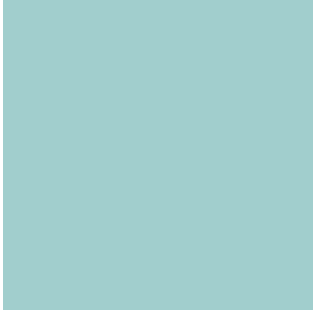




Segment based contact - soft=2

Jimmy Forsberg

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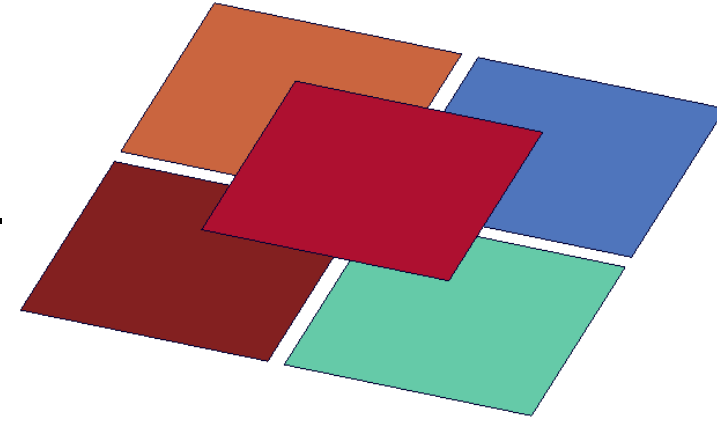
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Agenda

- Basic idea
- *CONTACT_'s for soft=2
- Parameters for SOFT=2
- Comparison with other contacts in different situations

Basic idea

- Comes from airbag simulation
 - Robust contact search
 - Speed is crucial
 - Many parameters originates from the airbag folding/deployment.
- Treat interaction between a segment pair once.
- Each segment pair treated individual.
- Default – fast, accuracy can be turned up (compare with _MORTAR).
- Master segment selected internally (ONE_WAY) contacts override this.
- Forces applied in normal direction of master surface (see DEPTH parameter).



Supported elements

- All 3D- analysis elements except beams/springs – need a surface definition.
 - Shells
 - Solids
- Higher ordered element treatment – multiple bilinear segments
 - Shells
 - Tets
 - Hex
- Beam elements are NOT supported

Un-supported options

- *CONTACT_xxx_ORTHO_FRICTION
- *CONTACT_xxx_SMOOTH
- Any constraint based contact
 - TIEBREAK contacts
 - TIED contacts
 - CONSTRAINT contacts
- Beam elements are NOT supported

Parameters affecting soft=2

■ _MPP

The optional card(s) activated by _MPP – read but ignored if soft=2...

Card 1	1	2	3	4	5	6	7	8
Variable	IGNORE	BCKT	LCBCKT	NS2TRK	INITITR	PARMAX		CPARM8
Type	I	I	I	I	I	F		I
Default	0	200	None	3	2	Depends		0
Card 2	1	2	3	4	5	6	7	8
Variable	&	CHKSEGS	TENSF	GRPABLE				
Type		I	F	I				
Default		0	0.0	0				

*CONTACT (1-3)

Card 1	1	2	3	4	5	6	7	8
Variable	SSID	MSID	SSTYP	MSTYP	SBOXID	MBOXID	SPR	MPR
Type	I	I	I	I	I	I	I	I
Card 2	1	2	3	4	5	6	7	8
Variable	FS	FD	DC	VC	VCD	PENCHK	BT	DT
Card 3	1	2	3	4	5	6	7	8
Variable	SFS	SFM	SST	MST	SFST	SFMT	FSF	VSF
Type	F	F	F	F	F	I	F	F
Default	1.0	1.0	Elem. Thick.	Elem. Thick	1.0	1.0	1.0	1.0

- PENCHK does not apply for SOFT=2.
- VSF does not apply for SOFT=2.

*CONTACT - optional cards

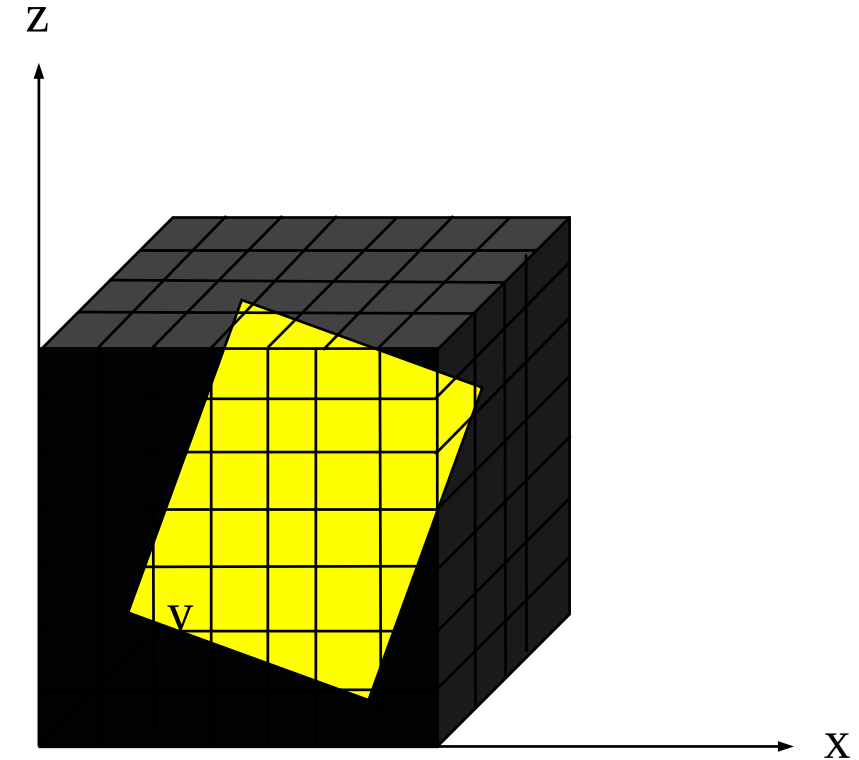
Opt. A	1	2	3	4	5	6	7	8
Variable	SOFT	SOFTSCL	LCIDAB	MAXPAR	SBOPT	DEPTH	BSORT	FRCFRQ
Opt. B	1	2	3	4	5	6	7	8
Variable	PENMAX	THKOPT	SHLTHK	SNLOG	ISYM	I2D3D	SLDTHK	SLDSTF
Opt. C	1	2	3	4	5	6	7	8
Variable	IGAP	IGNORE	DPRFAC/	DTSTIF/M			FLANGL	CID_RCF
Opt. D	1	2	3	4	5	6	7	8
Variable	Q2TRI	DPTCHK	SFNBR	FNSCL	DNSCL	TCSO	TIEDID	SHLEDG
Opt. E	1	2	3	4	5	6	7	8
Variable	SHAREC	CPARM8	IPBACK	SRNDE	FRICSF	ICOR	FTORQ	REGION
Opt. F	1	2	3	4	5	6	7	8
Variable	PSTIFF	IGNROFF		FSTOL	2DBINR	SSFTYP		
Type	I	I		F	I			
Default	0	0		2.0	0			

Running through the basic for a contact

- Contact search
- Penalty stiffness in contact
- Frictional behavior of contact
- Contact thickness
- Initial penetration treatment
- Release condition

Contact search for SOFT=2

- Bucket sort
 - BSORT parameter
 - Find contact pairs
 - Depends on
 - SBOPT
 - DEPTH
 - Evaluate segment overlap
 - Evaluate contact point
 - Apply contact force
- Volume partitioned into buckets
 - Find closest buckets to each slave node.
 - A list closest nodes are set. Typical 2 for most contacts.
 - The segment corresponding to those nodes and their neighbors are then checked for penetration in the subsequent cycles.
 - Incremental search each cycle for new closest node of closest segments.
 - Execution of bucket sort every 10-200 cycles, implicit every cycle.
 - Depending on contact used, modified on _MPP card or Optional card A.



More on contact search

■ SBOPT

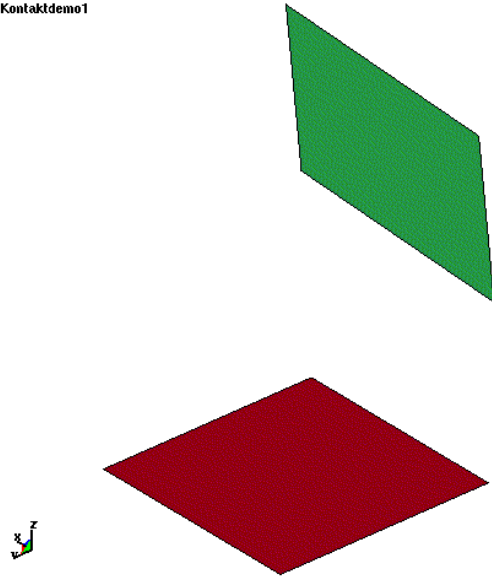
- SBOPT=3 → Check for warped segments
- SBOPT=5 → Check for sliding – primarily solid elements

■ DEPTH

- Many different options exist (1,2,3,4,5,13,23,33,25,35,45)
- If ending with 3 – no edge2edge checking
- If ending with 5 – edge2edge checking
- Recommended variants: 3/5/35/45.
- 45 also changes the geometry of the segment interpretation more on that later...

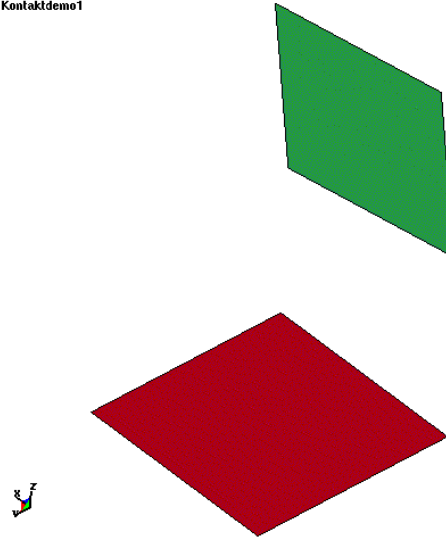
Soft=2, segment based contact

Kontakdemo1



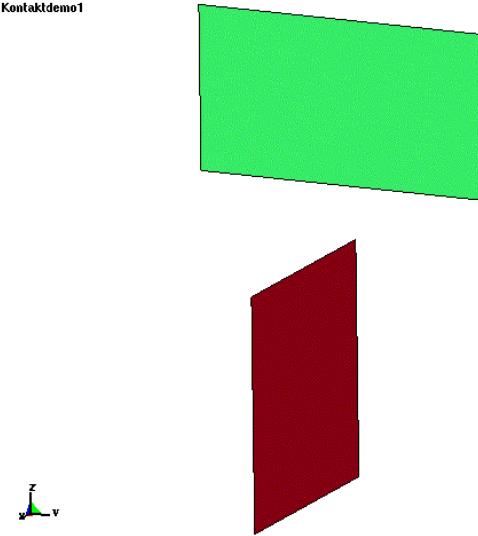
SBOPT = 3, DEPTH = 2
Surface Penetration measured
at nodes.

Kontakdemo1



SBOPT = 3, DEPTH = 3
Surface Penetration measured at edges
at nodes and edges

Kontakdemo1

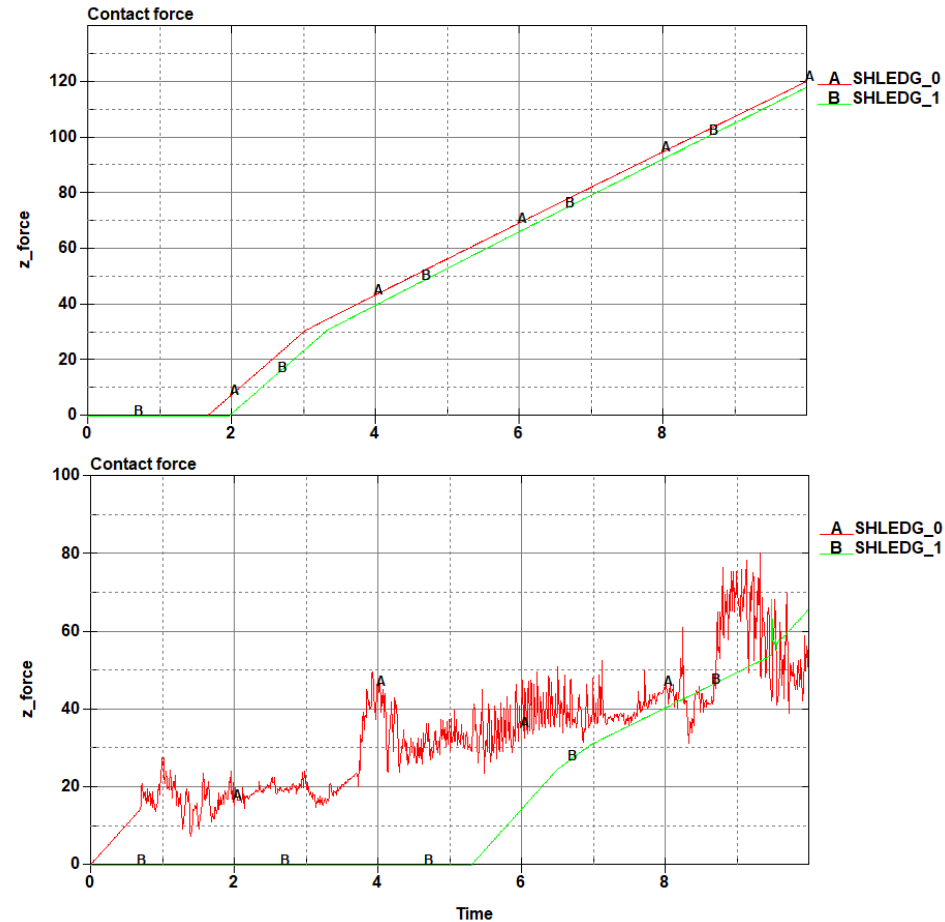
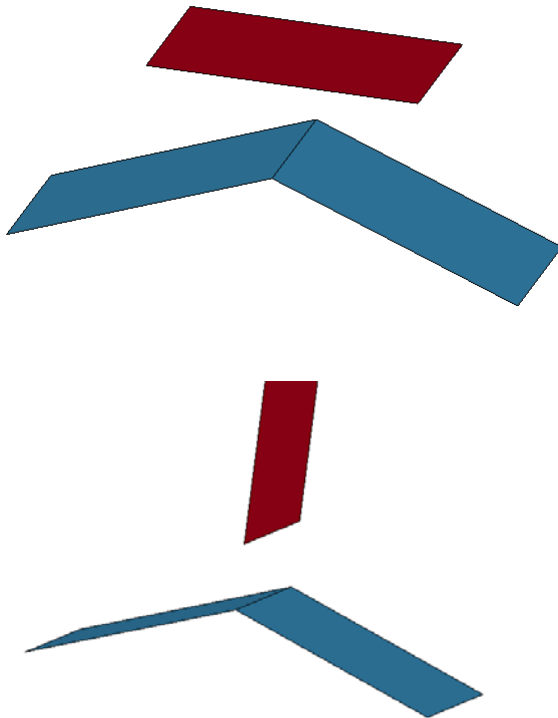


SBOPT = 3, DEPTH = 5
Surface Penetration and Edge-to-Edge
Penetration checked

Soft=2 – SHLEDG parameter

- Affects ALL segment edges – also internal edges between shells.
 - Simple flat surface coming into contact with an internal shell edge.
 - SBOPT=3, DEPTH=5, SHLEDG=0/1

■ Rotate



Edge geometry

■ SOFT=2

- Normal use is SHLEDG parameter
- SRNDE=2
 - Optional card E, position 4.
- Changes the extension of the cylindrical edges for soft=2 contacts
- No extension when DEPTH=35.



SHLEDG=0



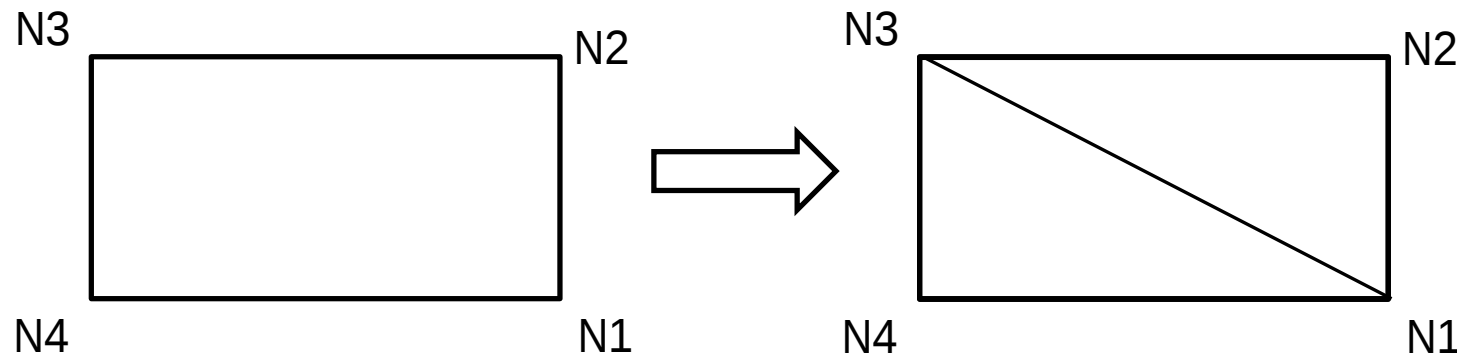
SRNDE=1



SHLEDG=1/SRNDE=2

Segment geometry

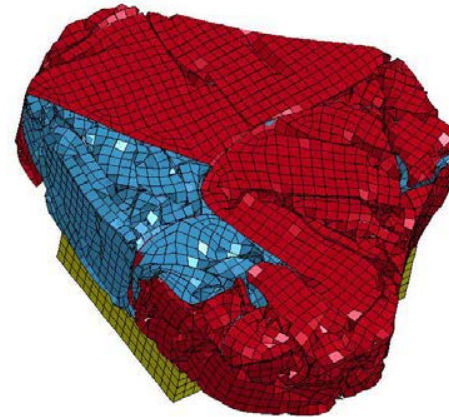
- There are a couple of flags that will change the geometry of the segment:
 - QUAD2TRIA
 - DEPTH=45
- QUAD2TRIA
 - Split each 4 noded segment into 2 quads based on their nodal topology. Same nodal topology will always give the same split.



From airbag application – folding/inflating

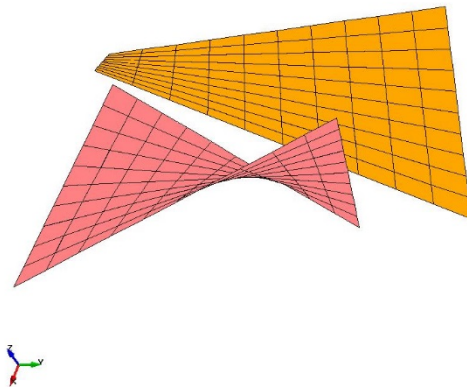
- DEPTH=45
 - Q2TRI=0 recommended

dilipdemo8 (UNIT: kg-mm-ms-K) simfold step1
Time = 80

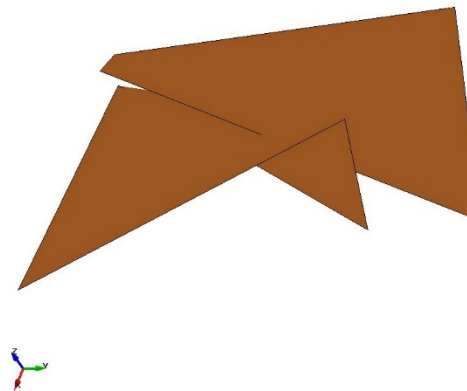


LS-DYNA keyword deck by LS-PrePost

Assembly 1
Green Parts
Part 1



Assembly 1
Green Parts
Part 1

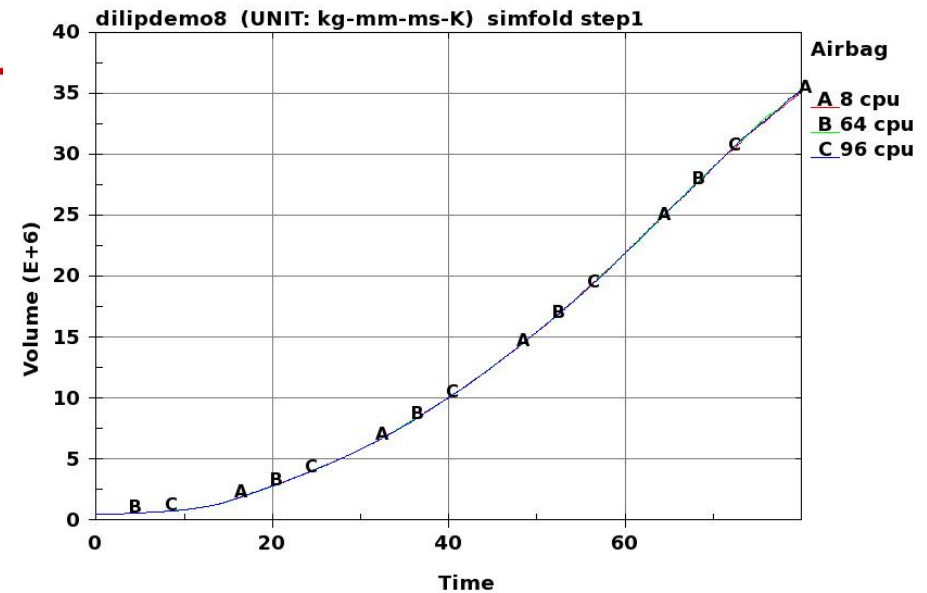
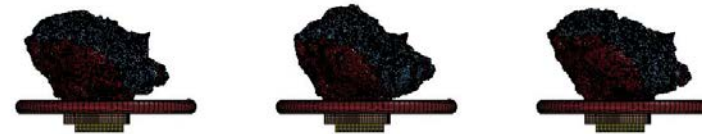


Soft=2, Depth=45

dilipdemo8 (UNIT: kg-mm-ms-K) simfold step1
Time = 9.992



dilipdemo8 (UNIT: kg-mm-ms-K) simfold step1
Time = 29.999



Penalty Scale Factor

- Soft = 2 Segment Based Contact (Optional Card A, Flag 1 on *CONTACT...)

$$k_{\text{SOFT}=2} = 0.5 * \text{SLSFAC} \begin{cases} \text{SFS} \\ \text{or} \\ \text{SFM} \end{cases} \left(\frac{m_1 m_2}{m_1 + m_2} \right) \left(\frac{1}{\Delta t} \right)^2$$

- Where:
 - m_1, m_2 = segment mass of contact partners.
 - shells: mass of element.
 - solids: half the mass of the element.
 - Δt = initial global time step (or larger).

Parameters affecting penalty scale factor

- SFS/MSF on Card 3 of contact definition

$$k_{\text{SOFT}=2} = 0.5 * \text{SLSFAC} \begin{cases} \text{SFS} \\ \text{or} \\ \text{SFM} \end{cases} \left(\frac{m_1 m_2}{m_1 + m_2} \right) \left(\frac{1}{\Delta t} \right)^2$$

- DTSTIFF

- Set the timestep size used for calculation for the penalty stiffness.

- PSTIFF

- Default segment volume times density gives segment mass.
 - PSTIFF=1, sum nodal masses and divide with a number giving the 'normal' amount of elements attached to a node.
 - Added mass due to mass-scaling/*ELEMENT_MASS can increase the stiffness.
 - Edge nodes mass underestimated - probably attached to fewer elements.

- SSFTYP on Optional card F

- If contact used with *PART_CONTACT and SSF parameter use

Parameters affecting penalty scale factor – nonlinear scaling

Opt. D	1	2	3	4	5	6	7	8
Variable	Q2TRI	DPTCHK	SFNBR	FNSCL	DNSCL	TCSO	TIEDID	SHLEDG
Type	I	F	F	F	F	I	I	I
Default	0	0.0	0.0	0.0	0.0	0	0	0

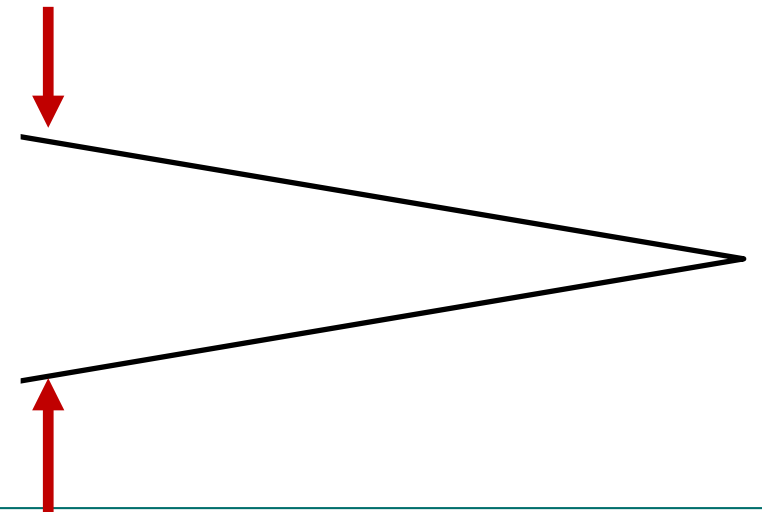
■ Using combination of FNSCL (f) and DNSCL (d)

- FNSCL<0; DNSCL>0: $k \rightarrow k \left[\frac{0.01fA_0}{d(d-\delta)} \right]$ $A_0 = \text{overlap area of segment in contact.}$
- FNSCL>0; DNSCL>0: $k \rightarrow kf \sqrt{\frac{\delta}{d}}$
- FNSCL>0; DNSCL=0: $k \rightarrow kf \left(\frac{A_0}{A_m} \right)$ $A_m = \text{mean area of all segment in contact.}$

Final parameter for stiffness scaling

Opt. D	1	2	3	4	5	6	7	8
Variable	Q2TRI	DPTCHK	SFNBR	FNSCL	DNSCL	TCSO	TIEDID	SHLEDG
Type	I	F	F	F	F	I	I	I
Default	0	0.0	0.0	0.0	0.0	0	0	0

- SFNBR: originates from folding simulations of airbags. Neighbor segments contact reduced possibility to make tight folded bags.
 - <0 : (recommended -0.5 to -1.0) $\rightarrow$ improve energy balance
 - >0 : scale the contact stiffness: $k \rightarrow SFNBR * k$
 - Only shell elements are checked.



Frictional behavior in CONTACT

Card 2	1	2	3	4	5	6	7	8
Variable	FS	FD	DC	VC	VCD	PENCHK	BT	DT
Card 3	1	2	3	4	5	6	7	8
Variable	SFS	SFM	SST	MST	SFST	SFMT	FSF	VSF
Type	F	F	F	F	F	I	F	F
Default	1.0	1.0	Elem. Thick.	Elem. Thick	1.0	1.0	1.0	1.0

- FS: static friction coefficient
- DC: exponential decay coefficient
- FD: dynamic friction coefficient
- VC: coefficient for viscous friction

$$\mu_C = FD + (FS - FD)e^{DC|v_{rel}|}$$

- FSF: coulomb friction scale factor $\longrightarrow \mu_{SC} = FSF \cdot \mu_S \longrightarrow F_{Limit} = VC \cdot VSF \cdot A_{Cont}$

Frictional behavior from *PART_CONTACT

Extra	1	2	3	4	5	6	7	8
Variable	FS	FD	DC	VC	OPTT	SFT	SSF	CPARM8
Type	F	F	F	F	F	F	F	
Default	0.0	0.0	0.0	0.0	0.0	0.0	0.0	

- The average between friction for master and slave segment is used.
 - The master segment is selected by contact (least penetrated segment) and normally the frictional behavior is picked up from master segment).
- FS=-1 on *CONTACT definition

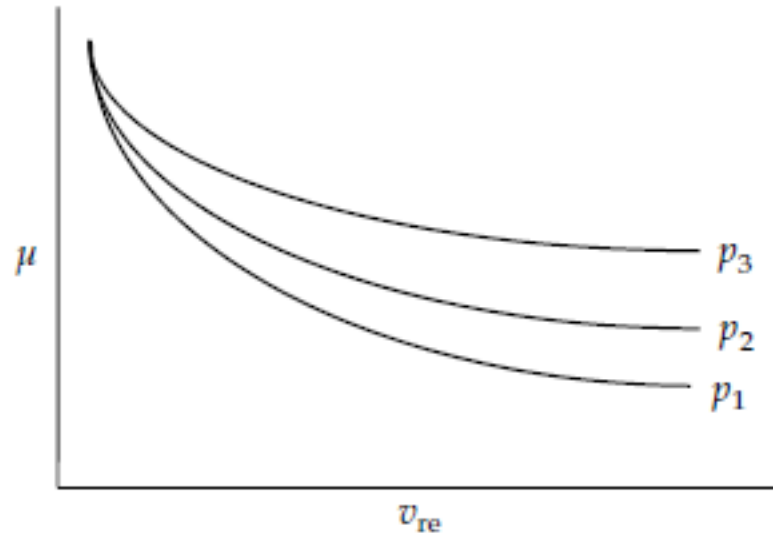
Frictional behavior using *DEFINE_FRICTION

Card 1	1	2	3	4	5	6	7	8
Variable	ID	FS_D	FD_D	DC_D	VC_D			
Type	I	F	F	F	F			
Default	0	0.0	0.0	0.0	0.0			
Card 2	1	2	3	4	5	6	7	8
Variable	PIDi	PIDj	FSij	FDij	Dcij	VCij	PTYPEi	PTYPEj
Type	I	I	F	F	F	F	A	A
Default			0.0	0.0	0.0	0.0		

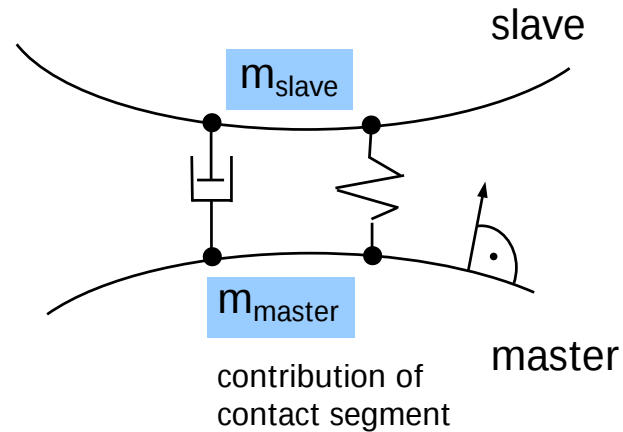
- *DEFINE_FRICTION superseeds *PART_CONTACT
- Definition in *contact_xxx using FS=-2 (-2 and FD gives table ID if multiple tables used).

Having a pressure/velocity dependent friction behavior

- Implemented for all contacts for SOFT=2.
 - Recommended when SOFT=2, FS=2 (FD gives table id):
 - FNLSCL=-1
 - DNLSCL=1/10:th of element thickness.
 - (DPRFAC=0.01 if significant sliding).



Contact damping – viscous damping

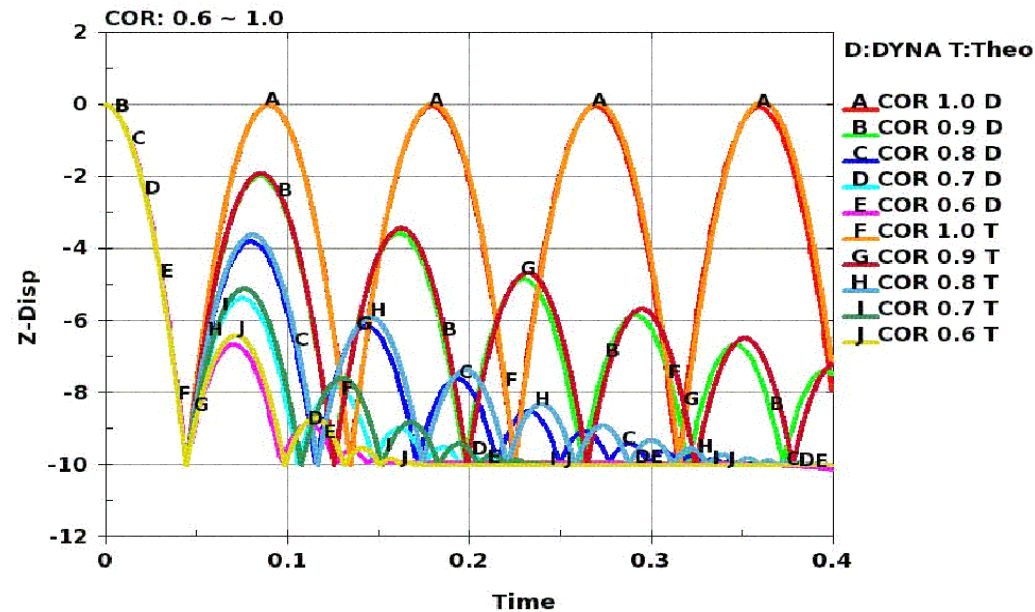


$$\xi = 2m\omega$$

$$\omega = \sqrt{\frac{k(m_{slave} + m_{master})}{m_{slave} \cdot m_{master}}}$$

- Parameter: VDC (*CONTACT, card 2)
- Contact damping is often beneficial in reducing high frequency oscillations
 - VDC=20 (corresponding to 20% of critical damping) is recommended
 - VDC=40-60 has been used for contacts with soft material
- Energies dissipated by viscous damping in contact is not reported separately.

Contact damping – ICOR



- Parameter: ICOR (*CONTACT, Optional card E)
- Applies to all soft=2 contacts and soft=0/1 when contact is one of:
 - AUTOMATIC_NODES_TO_SURFACE
 - AUTOMATIC_SURFACE_TO_SURFACE
 - AUTOMATIC_SINGLE_SURFACE
- Coefficient of Restitution set using VDC parameter
 - $0.0 \text{ (plastic collision)} \leq \text{VDC (COR)} \leq 100.0 \text{ (elastic collision)}$.

Parameters for thickness definition of segments

■ PART_CONTACT: OPTT

Extra	1	2	3	4	5	6	7	8
Variable	FS	FD	DC	VC	OPTT	SFT	SSF	CPARM8

- Solid elements → gives the segment of the solid a thickness.
- Shells → normal behavior.

■ CONTROL_SHELL → not affected by THEORY → First node gives segment thickness If *ELEMENT_SHELL_THICKNESS is used

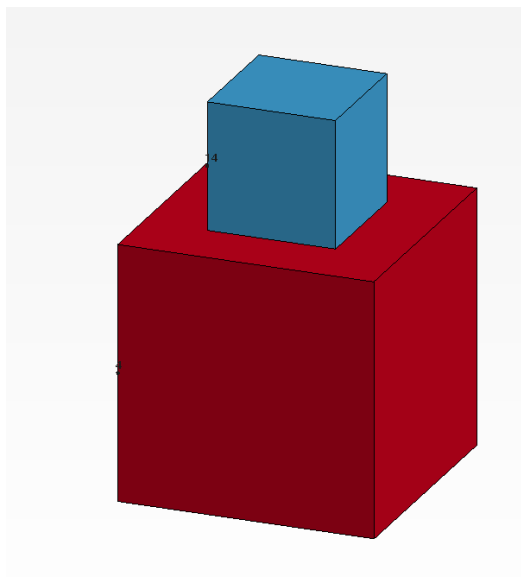
Card 1	1	2	3	4	5	6	7	8
Variable	WRPANG	ESORT	IRNXX	ISTUPD	THEORY	BWC	MITER	PROJ

Difference with large thickness elements

- **CONTROL_CONTACT** → do not use **SSTHK** → True element thickness used.

Card 2	1	2	3	4	5	6	7	8
Variable	USRSTR	USRFRC	NSBCS	INTERM	XPENE	SSTHK	ECDT	TIEDPRJ

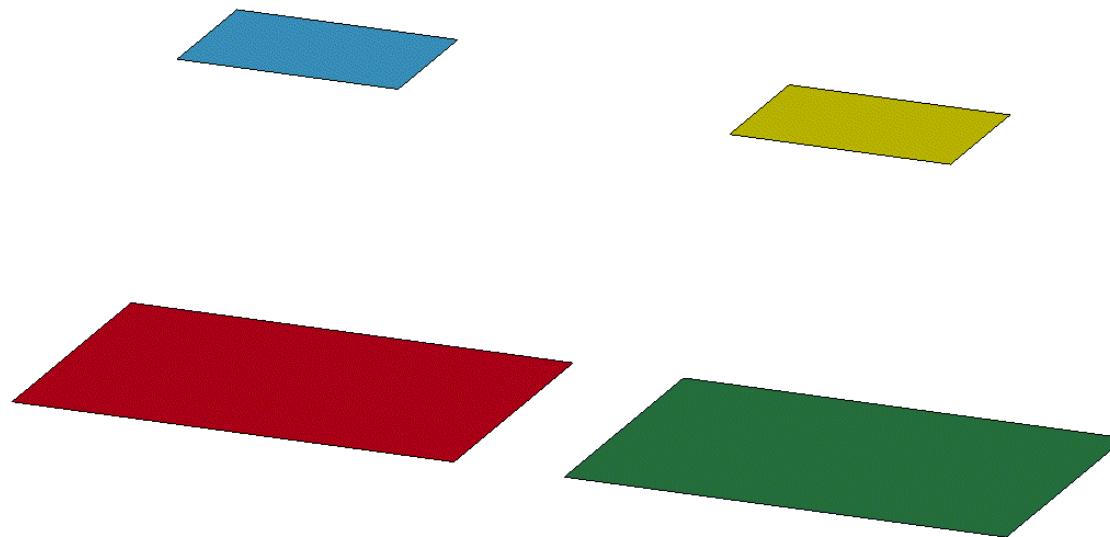
Structural geometry



Time = 0

Contact SOFT=2

Contact SOFT=1



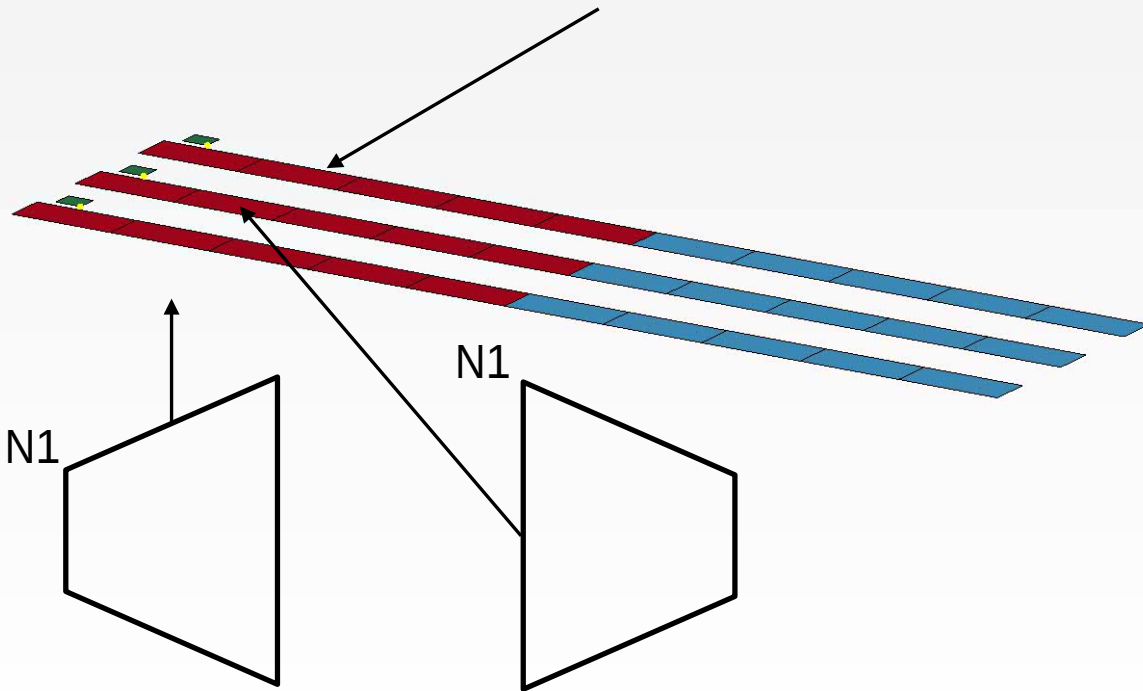
Segment thickness – tapered element

- Mechanical behavior of shells elform=2/16 – constant thickness!
 - ELEMENT_SHELL_THICKNESS_BETA → average nodal thickness value.
- Contact thickness behavior
 - Soft=2 → constant thickness using first nodal thickness
 - Soft=0/1 constant thickness using first nodal thickness
 - However segment thicknesses averaged on nodes and then interpolated over surface.
 - Soft=0/1 + THEORY=1 on *CONTROL_SHELL
 - Actual nodal thickness used and then interpolated over surface.

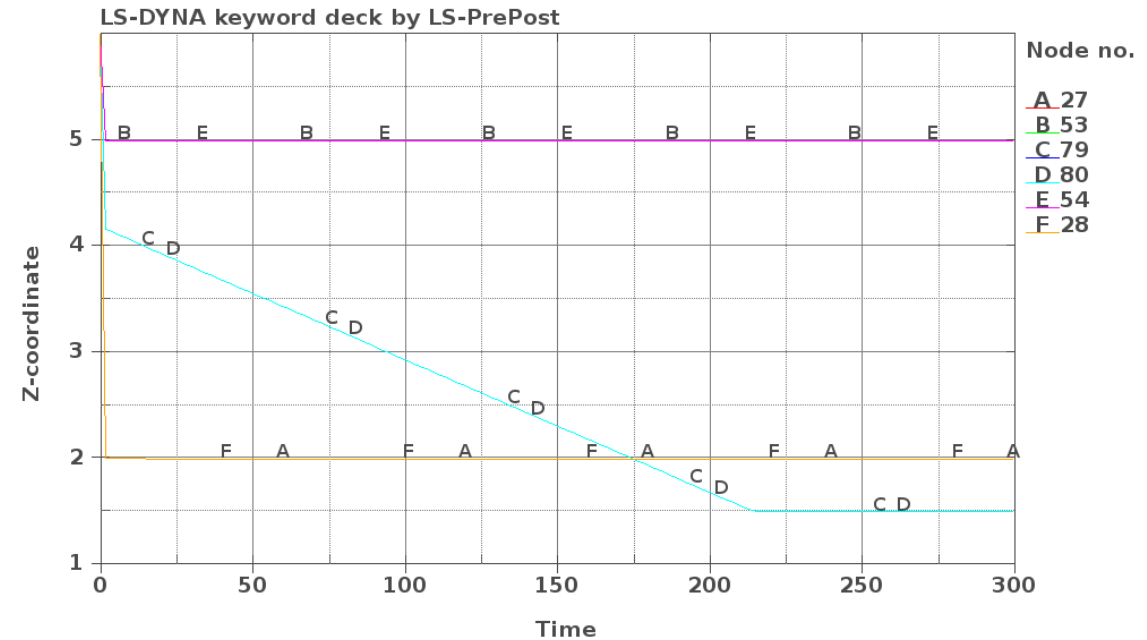
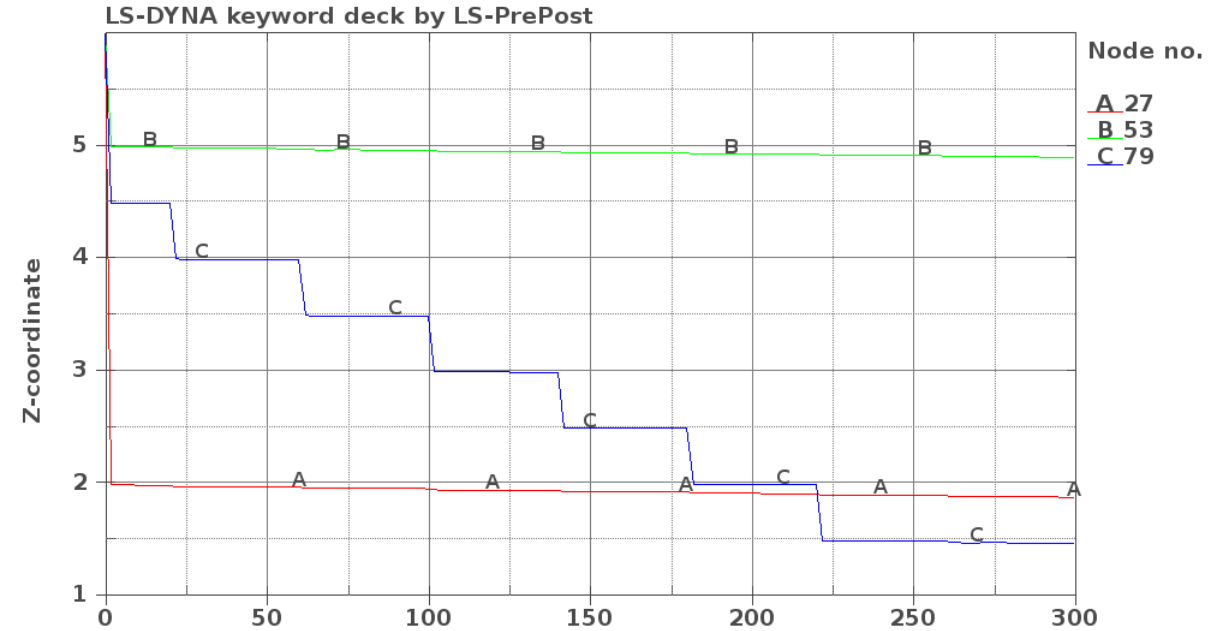
Simple test

- Sliding with *ELEMENT_SHELL_THICK

Strip with decreasing nodal thickness along slide path



Constant cross-section along slide path



Initial penetrations

- IGNORE is always on.

- Penetration found during first cycle between new contact pairs is treated with ignore → do not produce any contact forces.

- DPRFAC

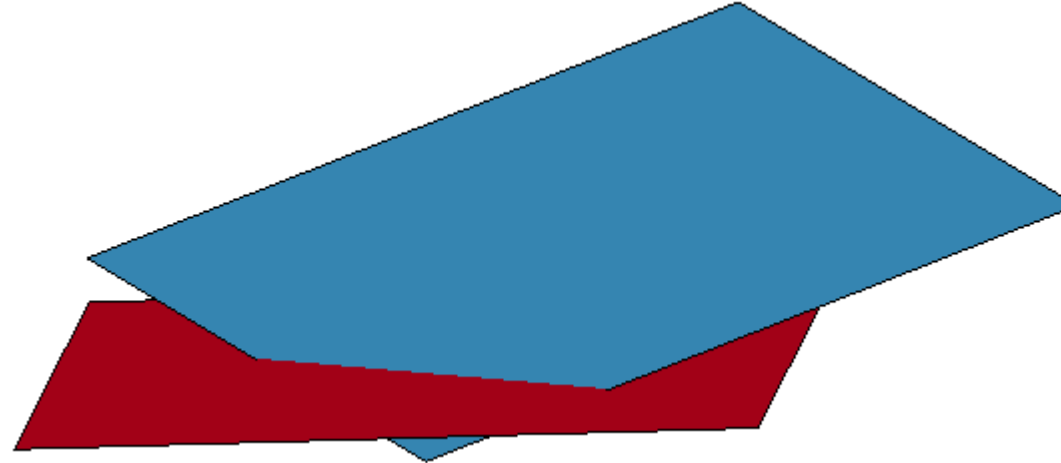
- Factor to reduce initial penetrations found after $t=0$.
 - Typical a factor of the initial penetration (which do not cause any contact force) is transformed into penetration which gives contact force:

$$\delta_i^{t+1} = \delta_i^t (1 - DPRFAC)$$

Hence a factor of 0.001 will approximately transform the initial penetration to contact pressure over 1000 cycles.

Possibility to check contact status

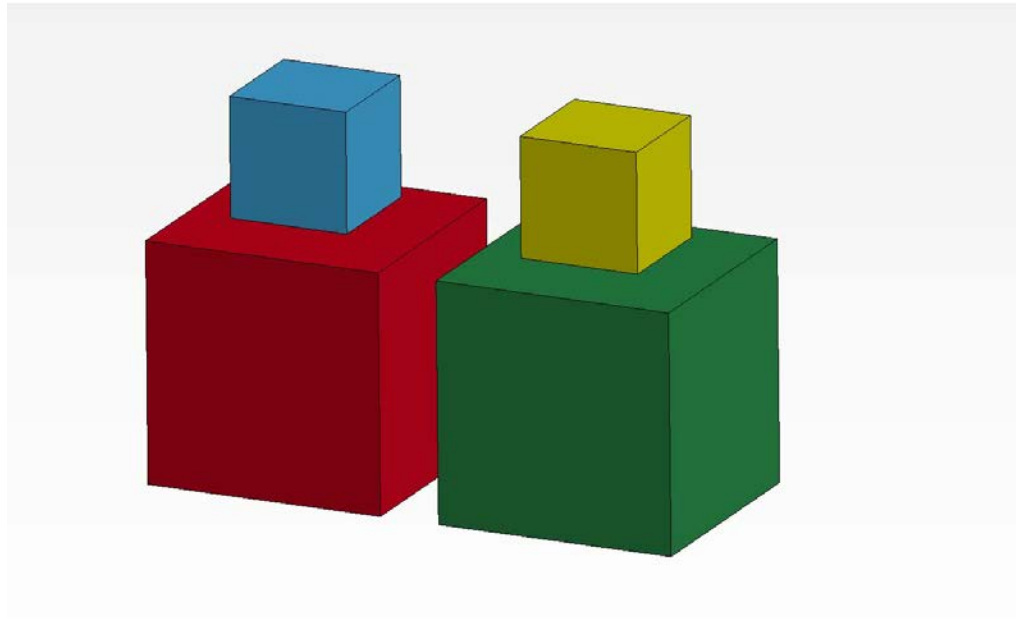
- The parameter DTPCHK gives a time interval for writing status between contact segments.
 - If a node of a segment cross the midsurface of another segment that node is reported into the d3hsp and message files.



- In an airbag deployment this is likely to happen. If reported once – no problem. If the same segment is reported several times in a row – slow down of unfolding should be expected.

*SECTION_SHELL

- NLOC parameter – which surface is meshed
- Similar functionality as _OFFSET on some element definitions.
- Requires CNTCO to be set on *CONTROL_SHELL to be honored in contact routines.



Soft=2 (NLOC/CNTCO)

Soft=0/1 (NLOC/CNTCO)

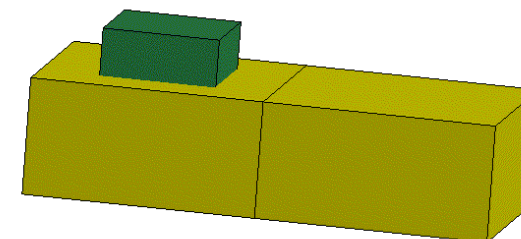
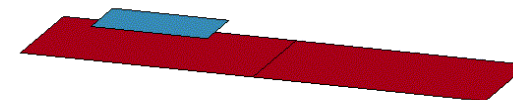
SSTHK flag operates first

Simple sliding behavior of SOFT=2

■ Simple model

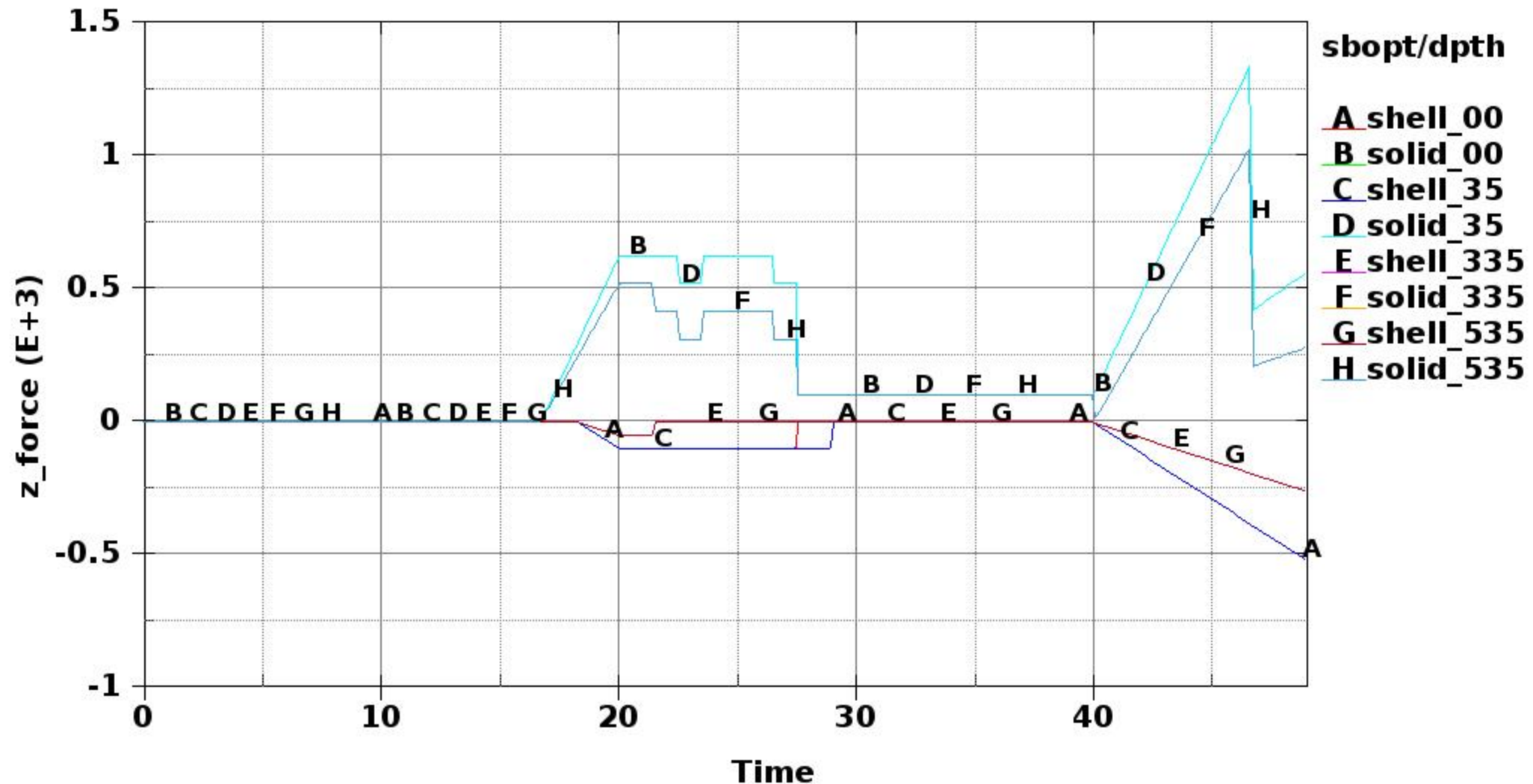
- Shell in initial penetration goes out of initial penetration and back again and slides to adjacent shell.
- Solid in initial penetration penetration goes out of initial penetration and back again and slides to adjacent solid.

Time = 0

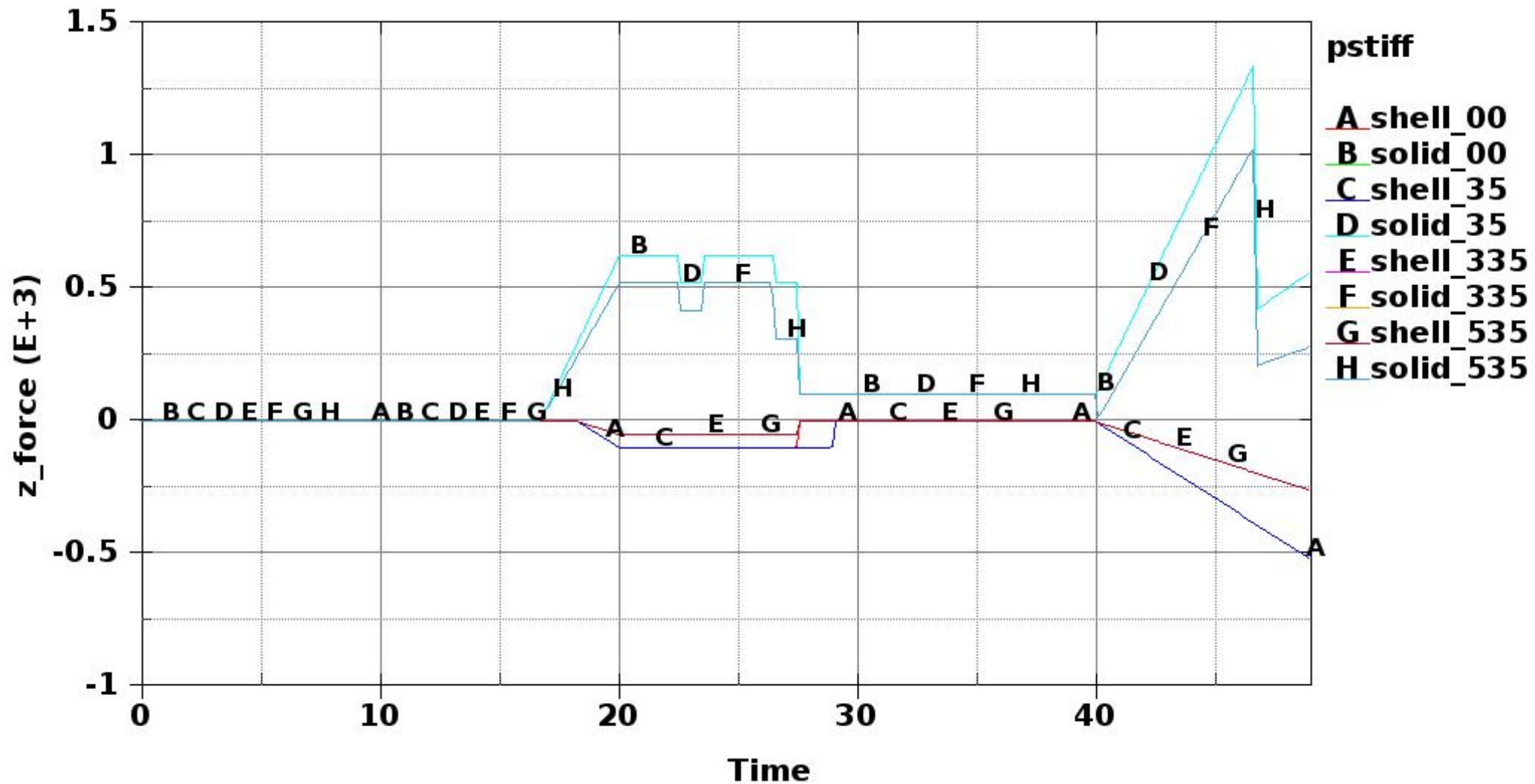


100.00 frame/sec

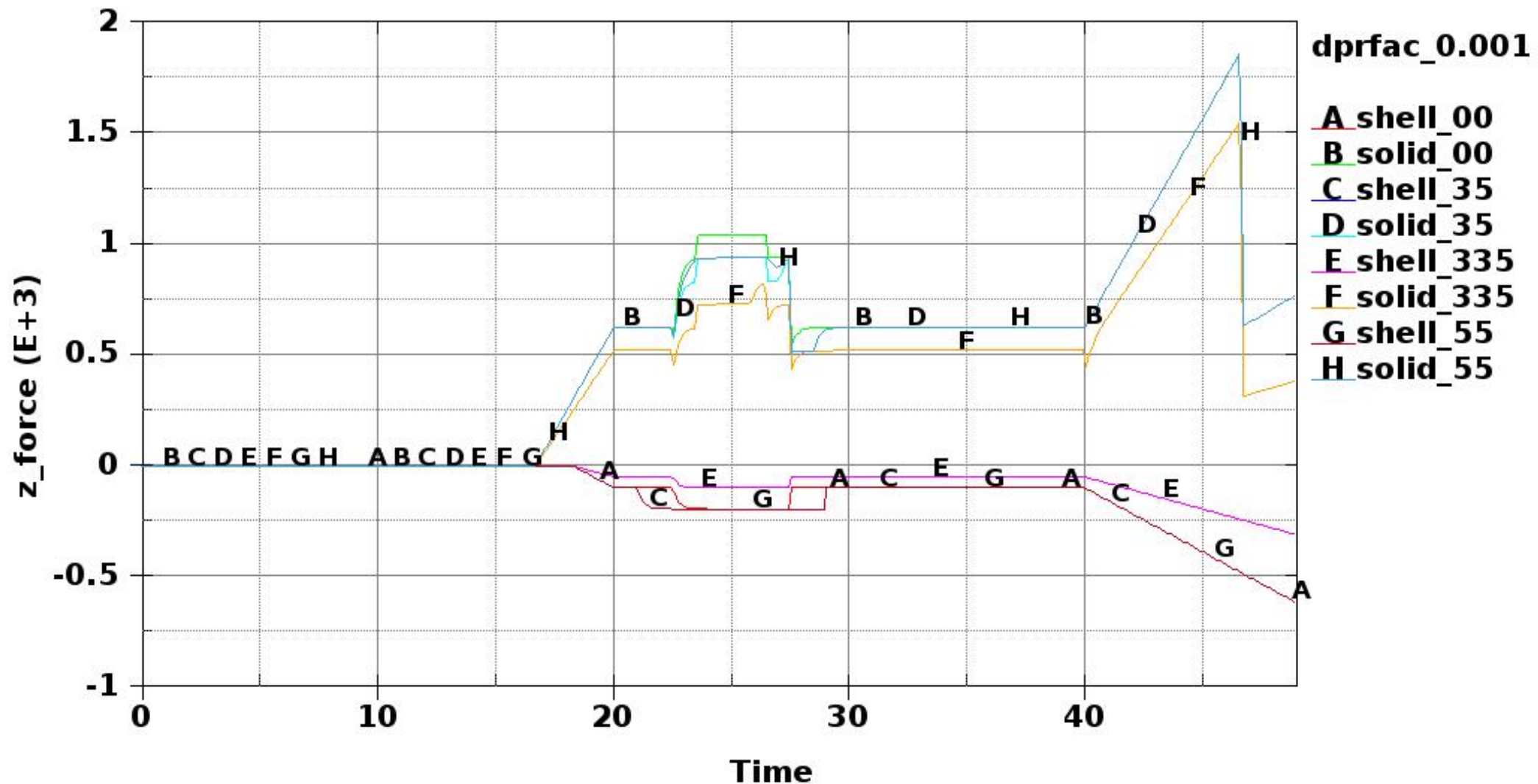
Sliding contact force with different settings SBOPT/DEPTH



Sliding contact force with different settings PSTIFF=1

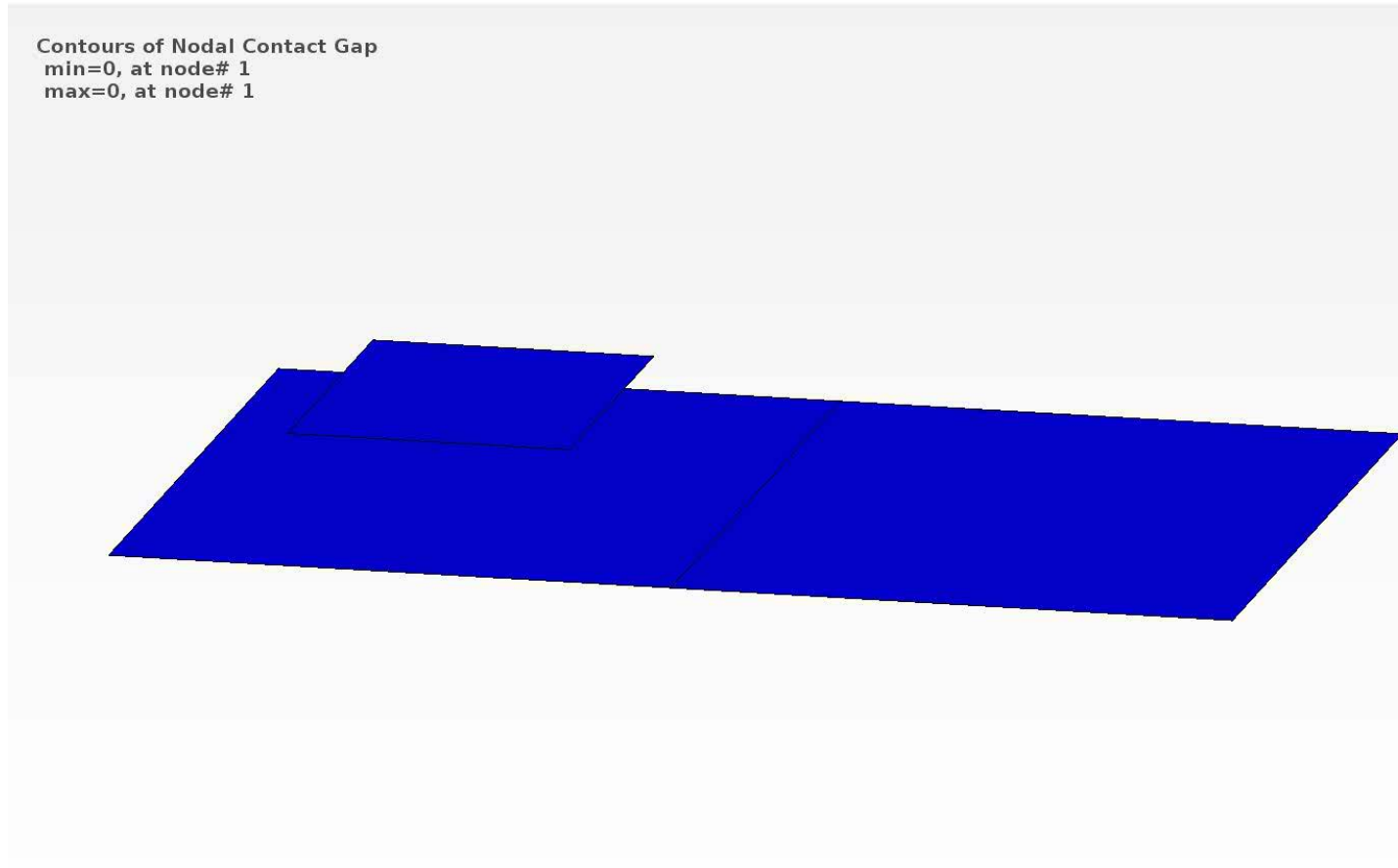


Sliding contact force with different settings DPRFAC=0.01



Special output for SOFT=2 in intfor

- Gap parameter for definition of gap/penetration fringe plots



Conclusions & Recommendations

- Major problem of contact failure today:
 - Contact search!
 - High loading on single node – rare today (decreased use of rigid material and finer meshes)
 - Searching for segment2segment overlap rather than a vector feels more robust.
 - SOFT=2 best way to handle solid contact (and also a possibility to get edge treatment of the solid in a good way).
 - SOFT=2 and eroding solid elements seems to be the future.

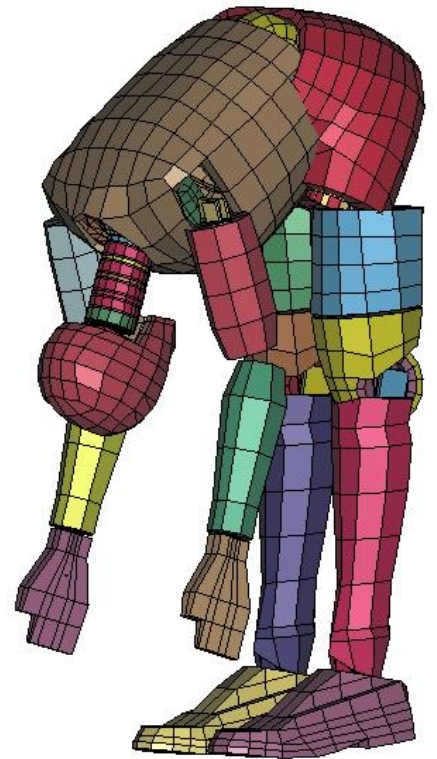
Final recommendations

- Use friction.
- VDC=20-40%
- SBOPT=3/5
- DEPTH=5 or 35 (45)
- SHLEDG=1
- PSTIFF=0/1
- SFNBR=0/0.5/-1.0
- DTSTIFF=initial timestep used

Thank you!



Your LS-DYNA distributor and
more



*DEFINE_FRICTION

Card 1	1	2	3	4	5	6	7	8
Variable	ID	FS_D	FD_D	DC_D	VC_D			
Type	I	F	F	F	F			
Default	0	0.0	0.0	0.0	0.0			
Card 2	1	2	3	4	5	6	7	8
Variable	PIDi	PIDj	FSij	FDij	DCij	VCij	PTYPEi	PTYPEj
Type	I	I	F	F	F	F	A	A
Default			0.0	0.0	0.0	0.0		

*DEFINE_FRICTION_ORIENTATION

Card 1

1

2

3

4

5

6

7

8

Variable	PID	LCID	LCIDP	V1	V2	V3		
Type	I	I	I	F	F	F		
Default	none	0	0	0.0	0.0	0.0		