



University of Maribor

Faculty of Mechanical Engineering

Simulations and Optimisation of Functionally Graded Auxetic Structures

Nejc Novak, Matej Vesenjsek, Zoran Ren

Faculty of Mechanical Engineering, University of Maribor, Maribor, Slovenia

Bamberg, 11.10.2016



Summary

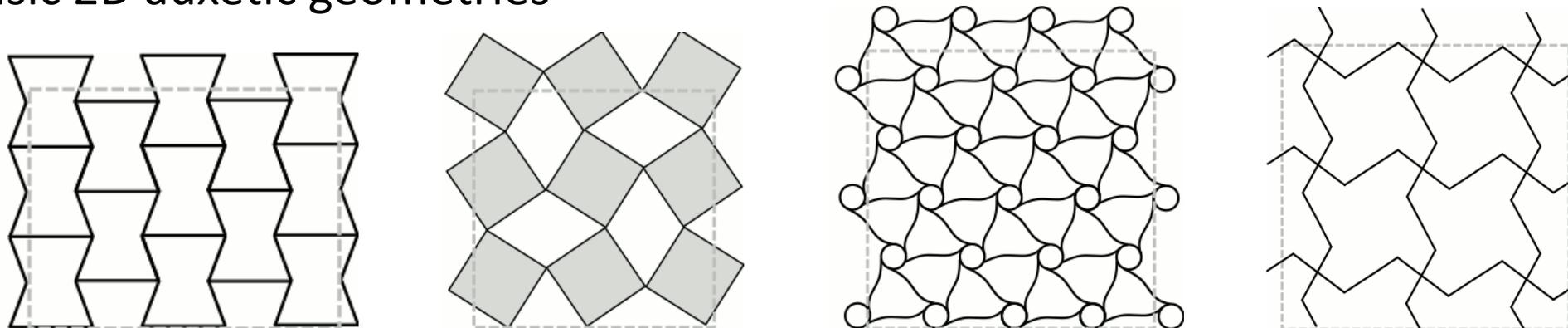
- Auxetic materials
- Motivation
- Introduction of auxetic cellular structures build from tetrapods
- Experimental testing
- Numerical modelling
 - Lattice numerical model built with beam finite elements (FE)
 - Homogenised numerical model built with volume FE
- Functionally graded porosity and response optimisation of auxetic cellular structure
- Conclusions and future prospects

Auxetic materials

- Name originates from Greek word *auxetos* – „tends to increase“ (Evans et al., Nature, 1991)
- This group of materials includes materials with negative Poisson's ratio:

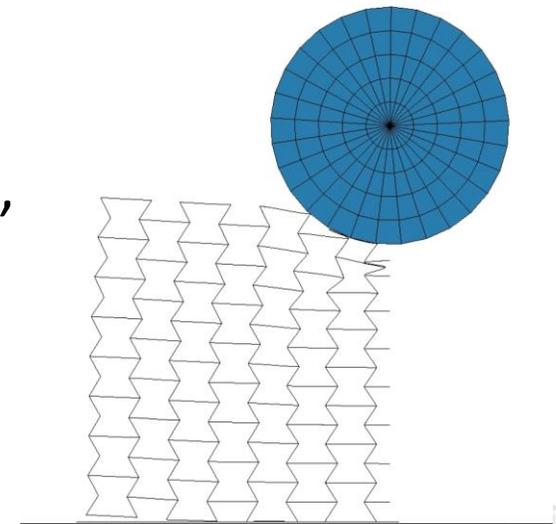
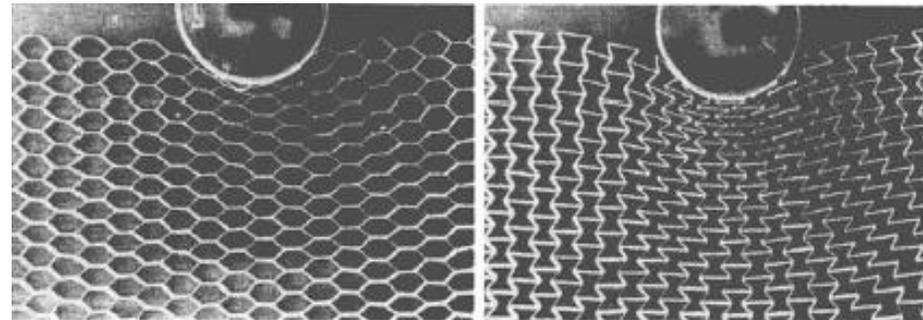


- Basic 2D auxetic geometries



Auxetic materials

- To achieve negative Poisson's ratio materials must be porous (cell walls can bend and deform in desired shape)
- The advantages that can be achieved using these materials:
 - unique deformation behaviour,
 - enhanced shear toughness $G = K \frac{3(1-2\nu)}{2(1+\nu)}$,
 - in case of impact material moves towards the impact zone,
 - better energy absorption.



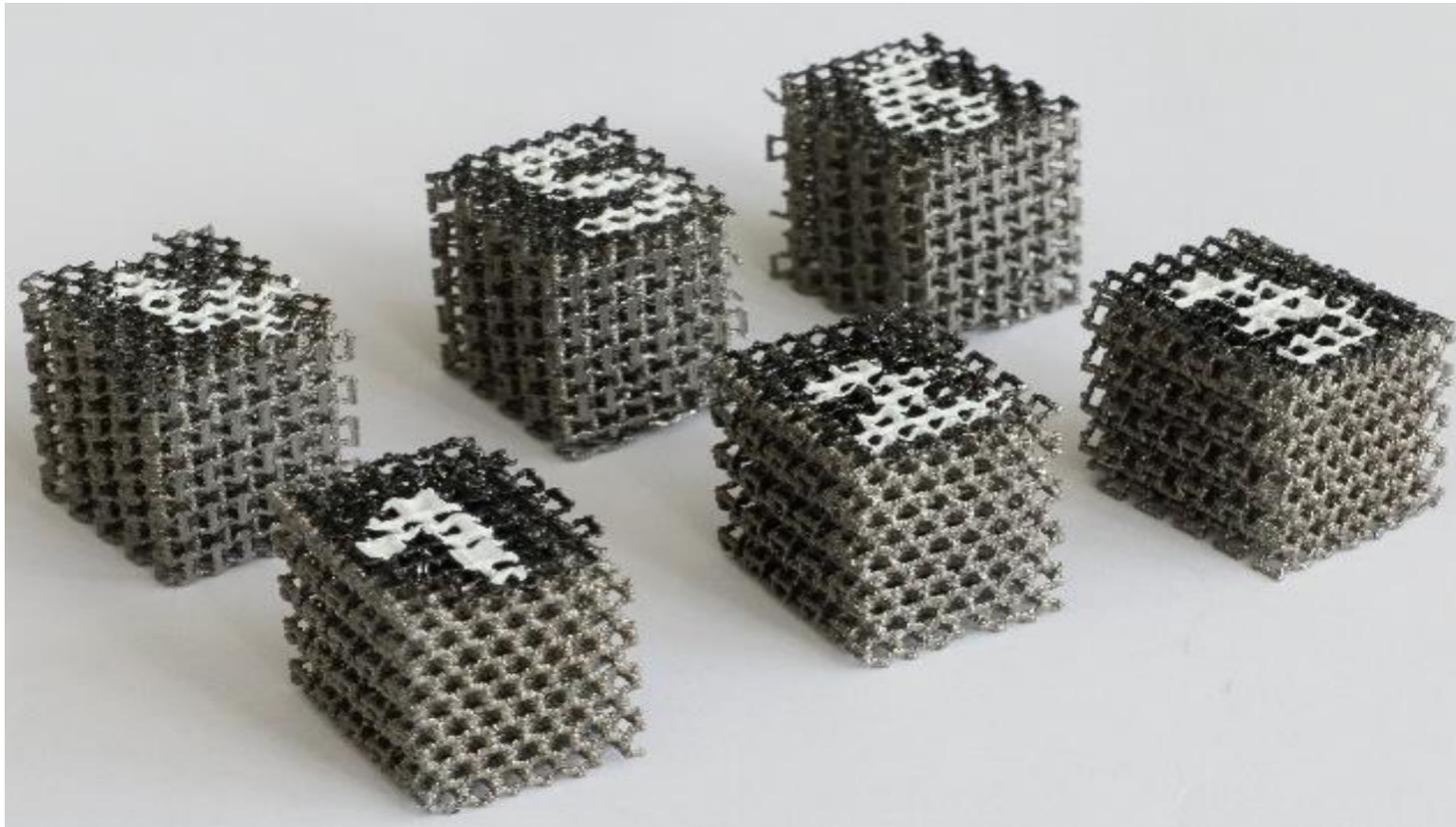


Motivation

- Great potential of auxetic structures in improving energy absorption in case of an impact
- This can be further enhanced with introduction of graded porosity (N. Novak, M. Vesenjāk, and Z. Ren, “Auxetic cellular materials - a Review,” *Strojniški Vestn. - J. Mech. Eng.*, vol. 62, no. 9, pp. 485–493, 2016)
- User defined response of graded auxetic structures can be achieved using optimisation techniques and numerical simulations
- Dynamic response of graded auxetic structures at different strain rates must be evaluated with numerical models and experiments

Geometry of auxetic structure

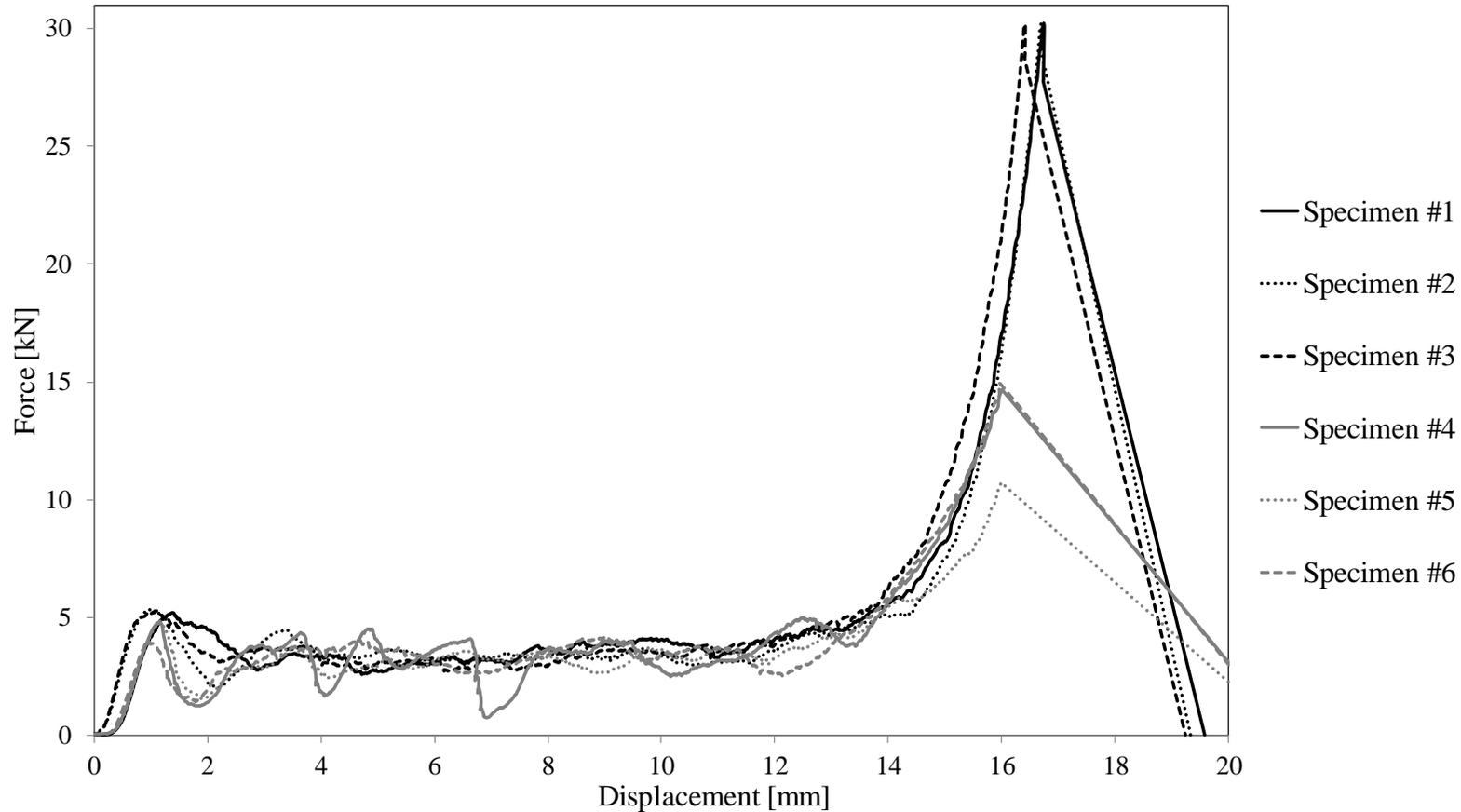
- Build from „inverted tetrapods“ (Schwerdtfeger et al., Physica Status Solidi (B), 247 (2), 2010)



Method: SEBM
Material: Ti6Al4V
Struts thickness: ≈ 0.5 mm

Compression testing

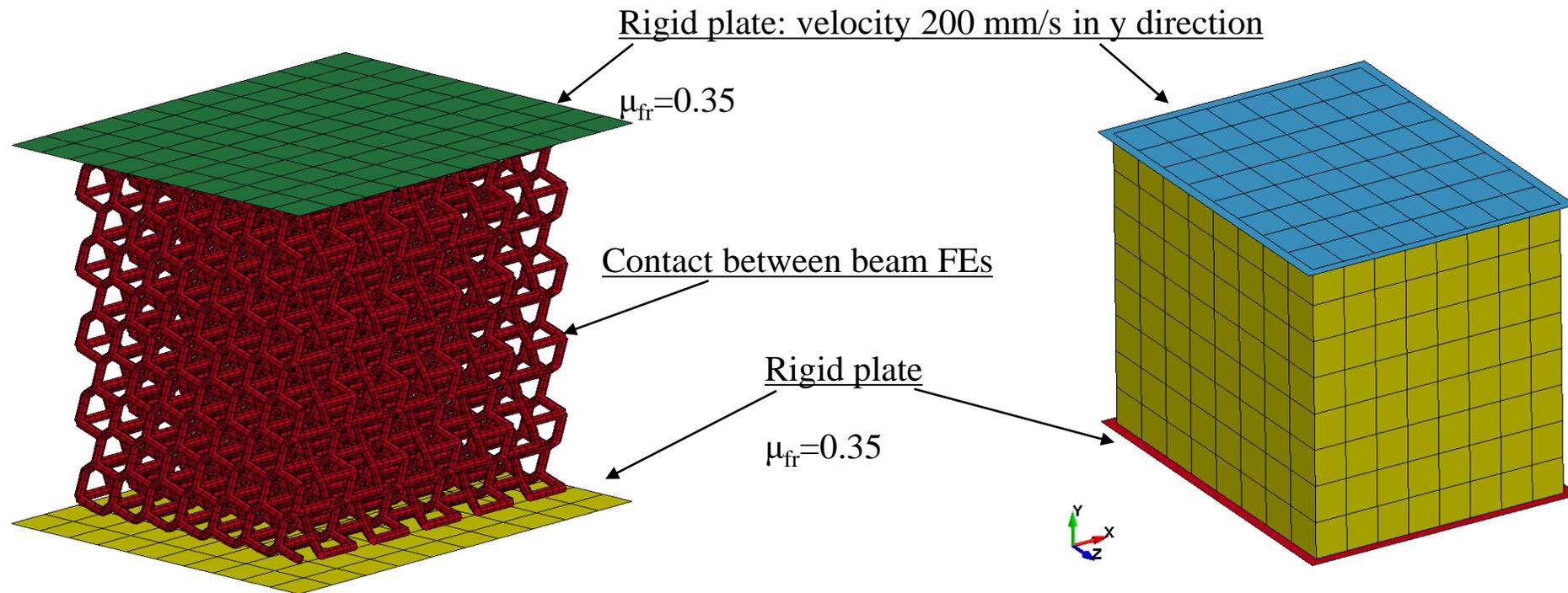
- Instron 8801 testing machine
- Cross-head rate 0.1 mm/s
- Specimens were compressed in two orthogonal directions



Numerical models in Ls-Dyna

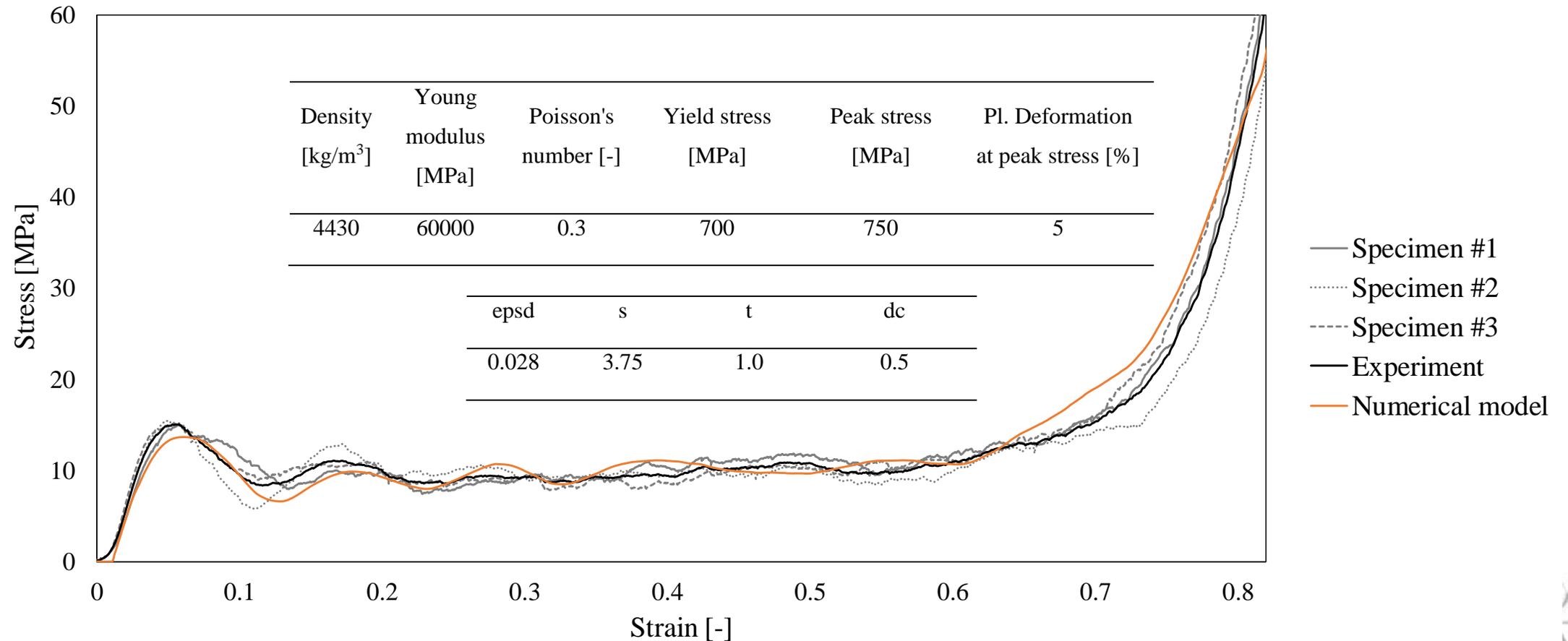
Lattice model
described with beam FE

Homogenised numerical model
described with volume FE



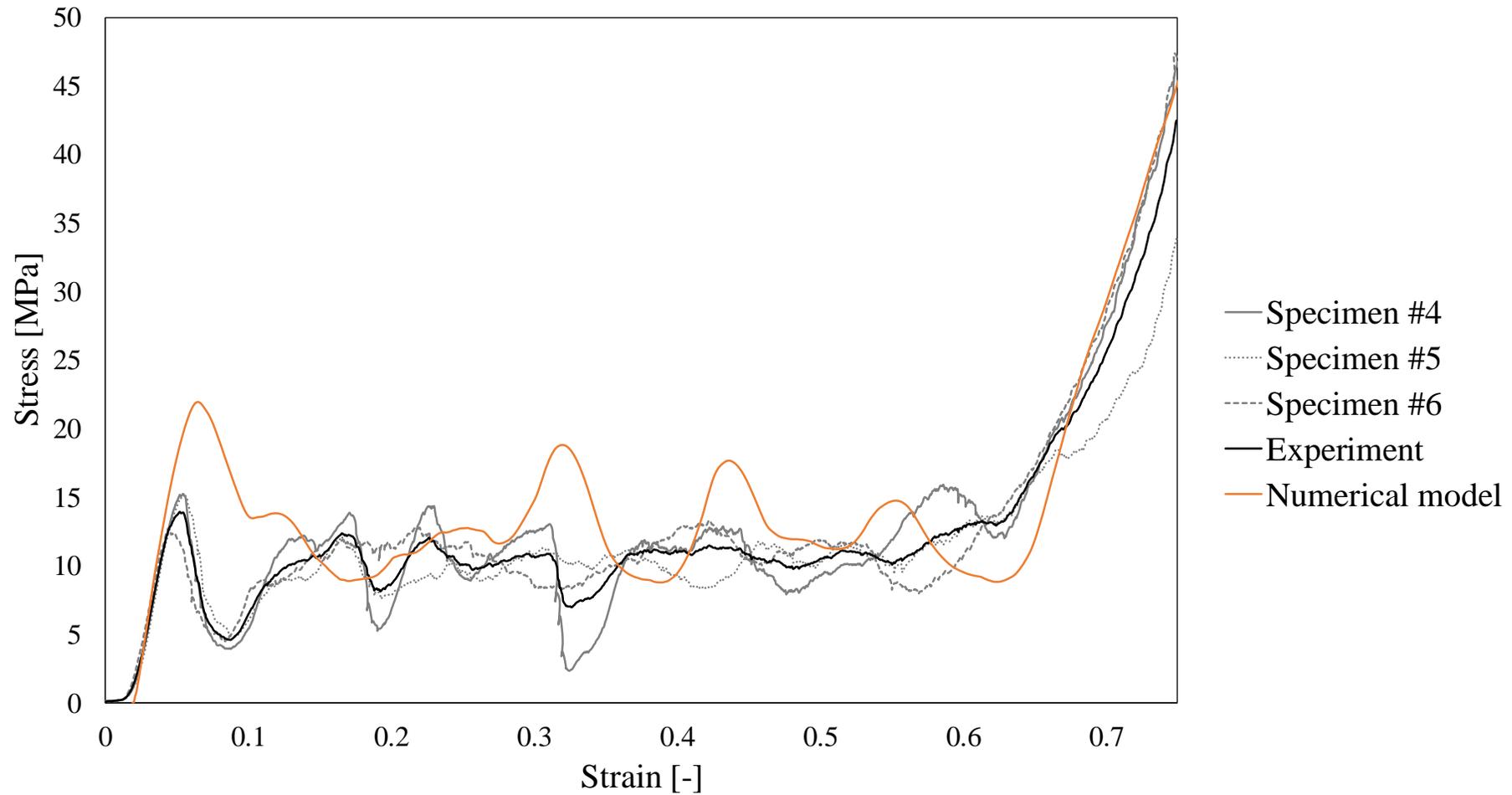
Results from numerical models (beam FE)

- Material parameters of MAT_153 were determined using parametrical simulations



Results from numerical models (beam FE)

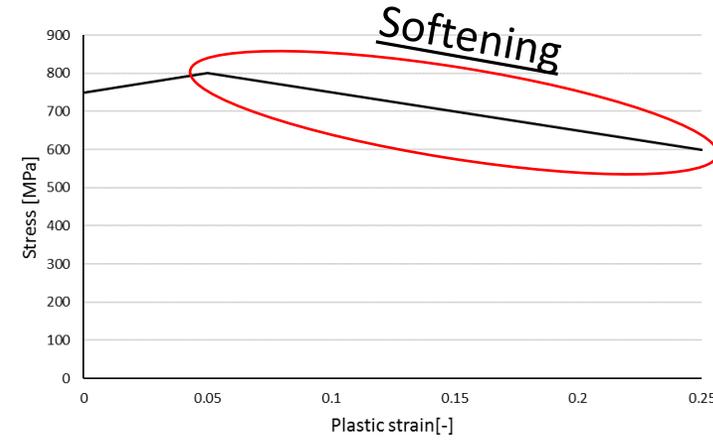
Specimens #4 - #6



MAT_024

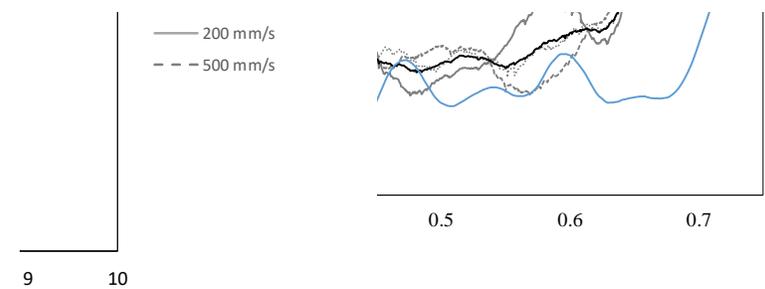
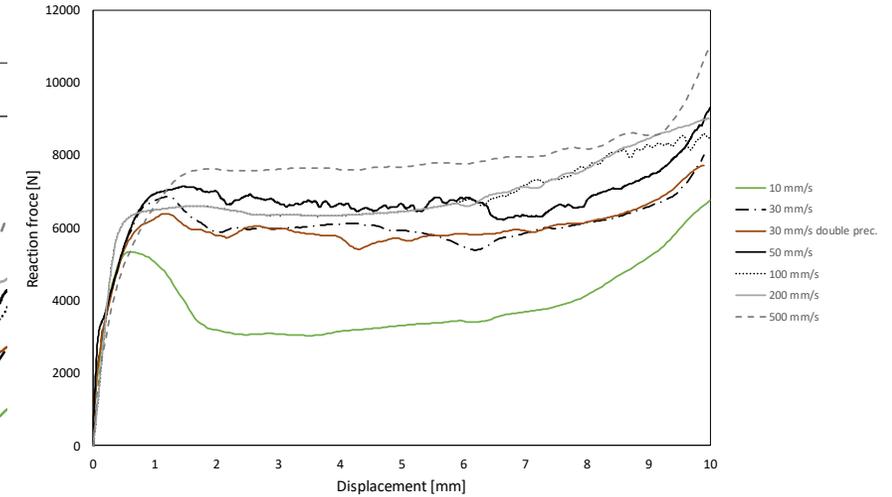
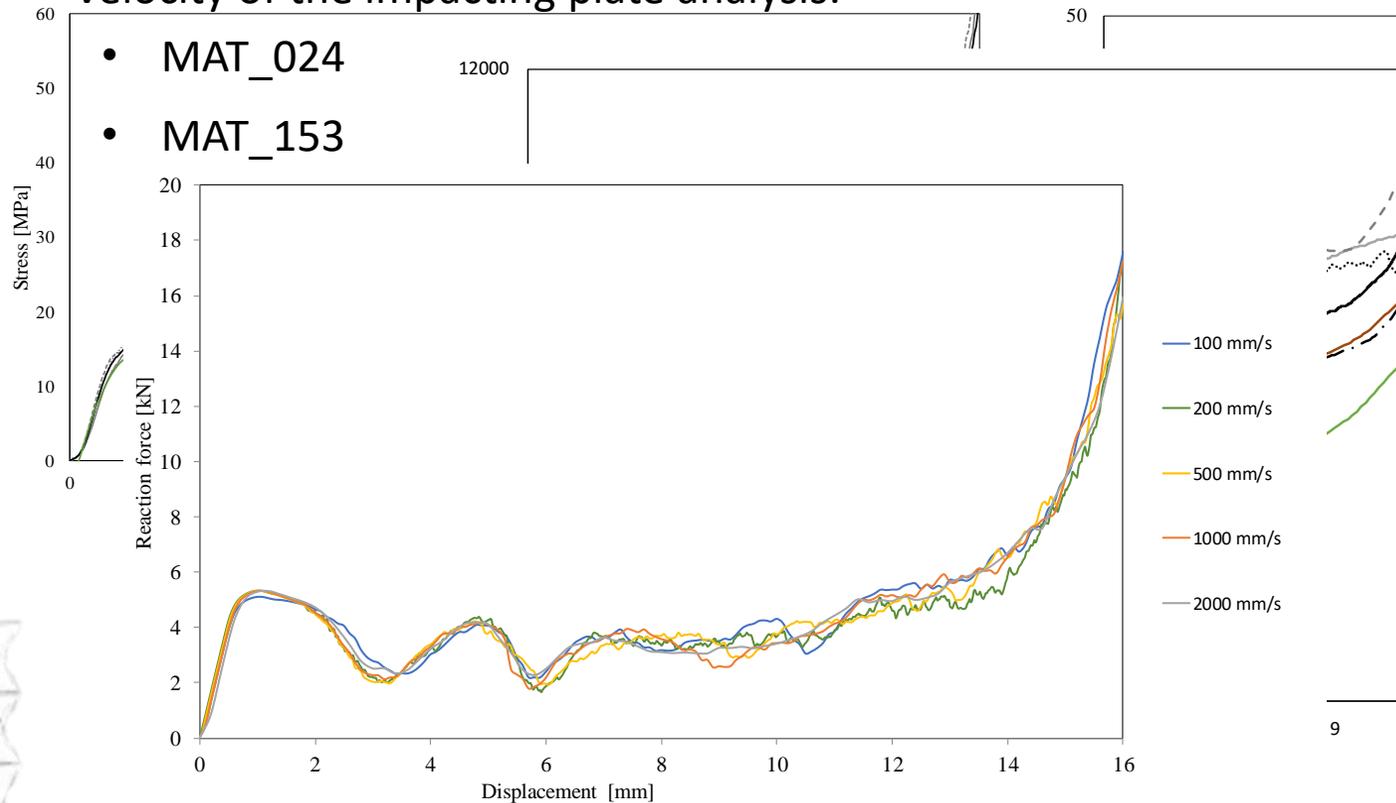
- Material parameters:

E [MPa]	$\sigma_{y,1}$ [MPa]	$\sigma_{y,2}$ [MPa]	$\epsilon_{pl,2}$ [%]	$\sigma_{y,3}$ [MPa]	$\epsilon_{pl,3}$ [%]
60000	750	800	5	600	25



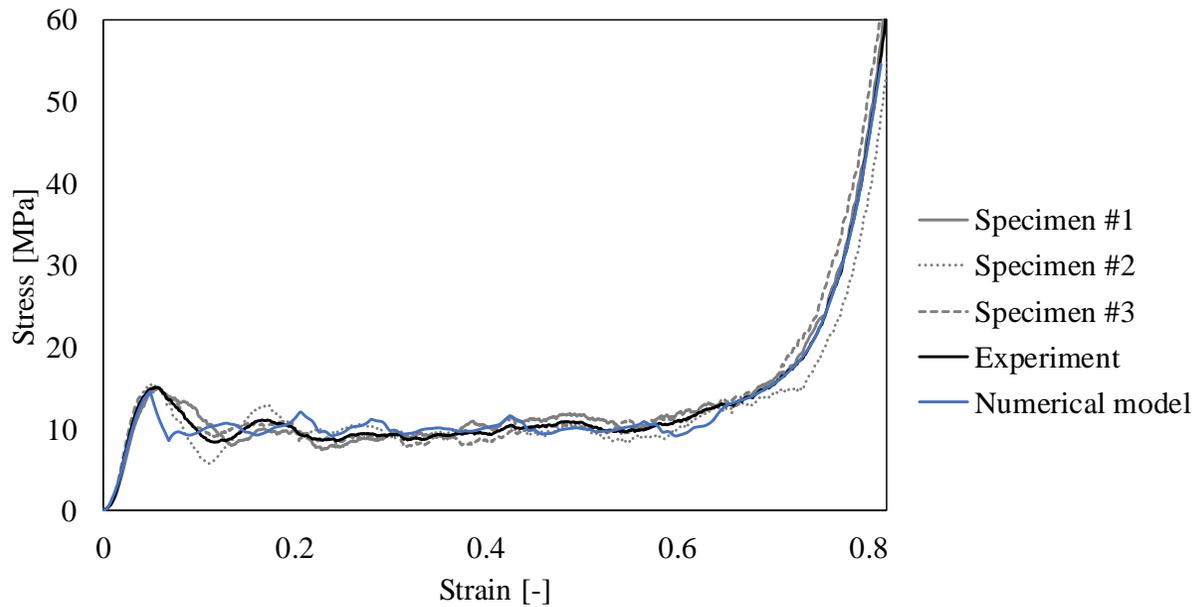
- Velocity of the impacting plate analysis:

- MAT_024
- MAT_153



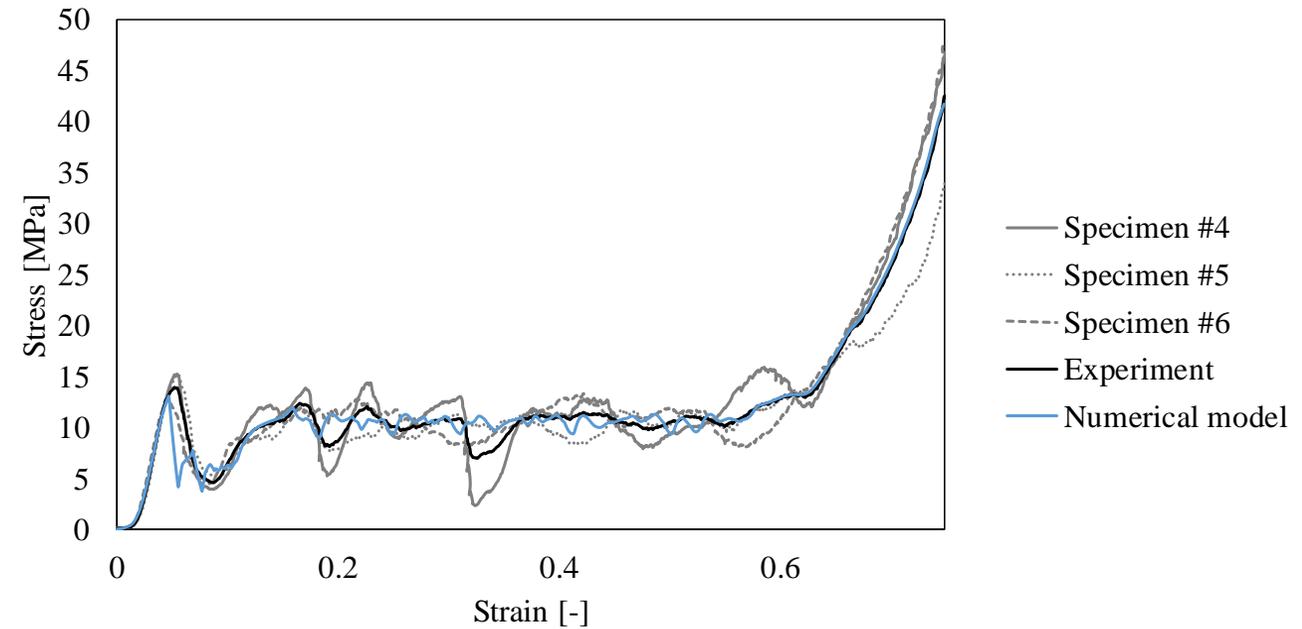
Results from homogenised numerical model with material model MAT_063

Specimens #1 - #3



	Specific deformation energy [J/kg]
Experiment	9.66
Homogenised numerical model	9.64

Specimens #4 - #6



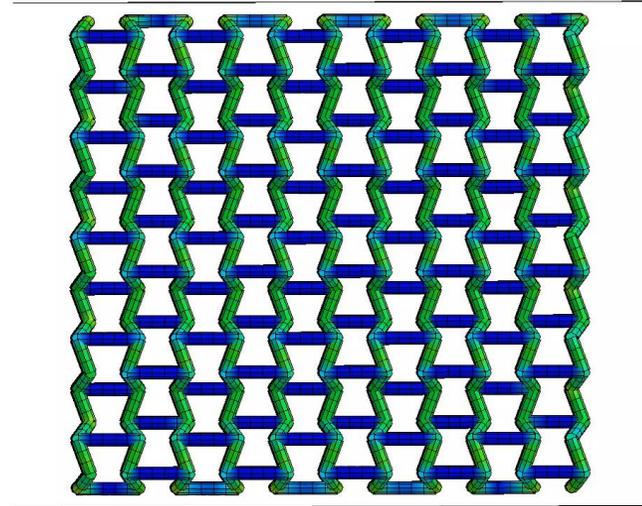
	Specific deformation energy [J/kg]
Experiment	9.19
Homogenised numerical model	9.24

Visual comparison between experiment and numerical models

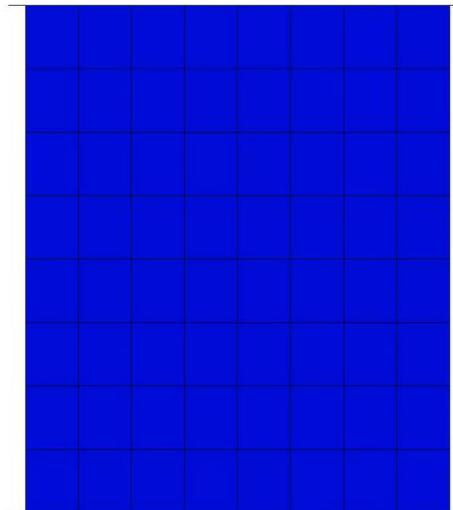


LS-DYNA keyword deck by LS-PrePost
Time = 0.00099999
Contours of Effective Plastic Strain
max IP. value
min=-0.00970312, at elem# 107814
max=0, at elem# 1

LS-DYNA keyword deck by LS-PrePost
Time = 0.00029996
Contours of Effective Stress (v-m)
max IP. value
min=0.332942, at elem# 10544
max=123.387, at elem# 12110



Effective Stress (v-m)
1.234e+02
1.111e+02
9.878e+01
8.647e+01
7.417e+01
6.186e+01
4.955e+01
3.725e+01
2.494e+01
1.264e+01
3.329e-01



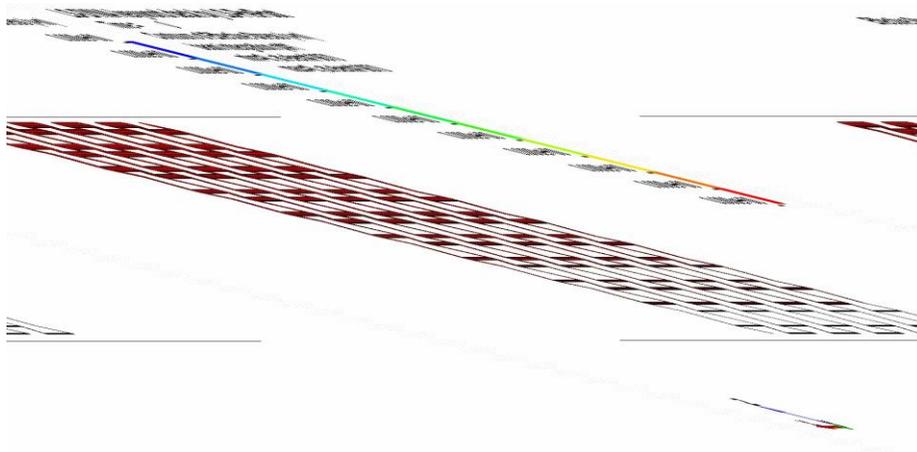
Effective Plastic Strain
1.518e-18
-9.703e-04
-1.941e-03
-2.911e-03
-3.881e-03
-4.852e-03
-5.822e-03
-6.792e-03
-7.762e-03
-8.733e-03
-9.703e-03



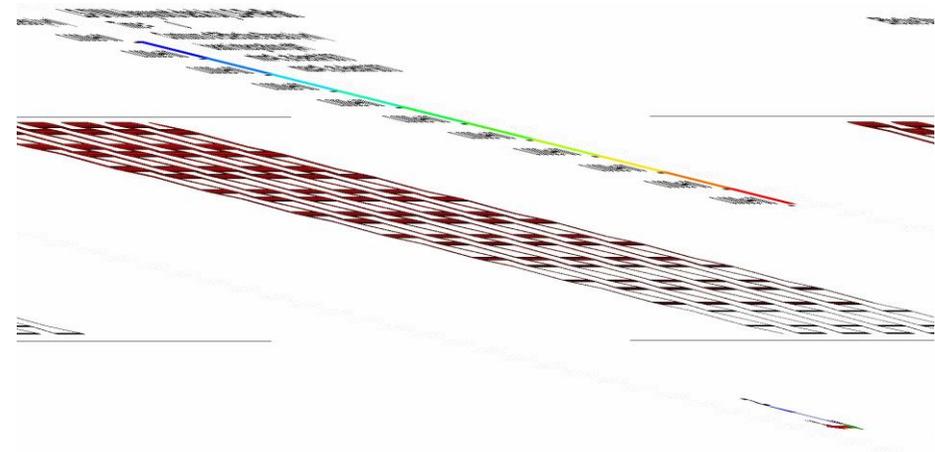
Functionally graded porosity

- With functionally graded porosity we can tailor the response of the structure
- Effect of graded porosity is more important above the critical strain rates (due to inertia effects main deformation occurs only on the deformation front between impacting plate and structure)

High velocity impact (200 m/s)

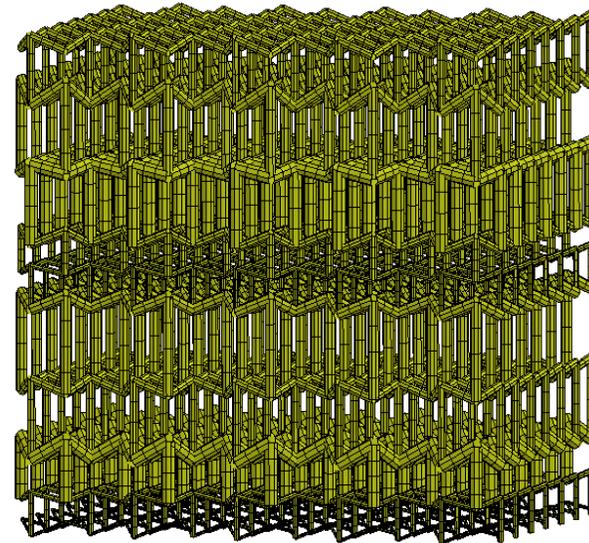
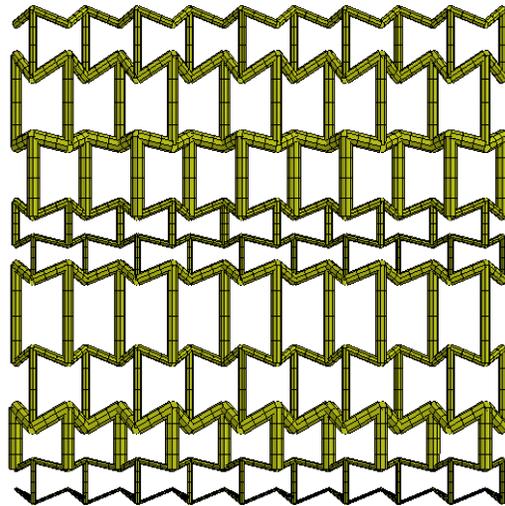
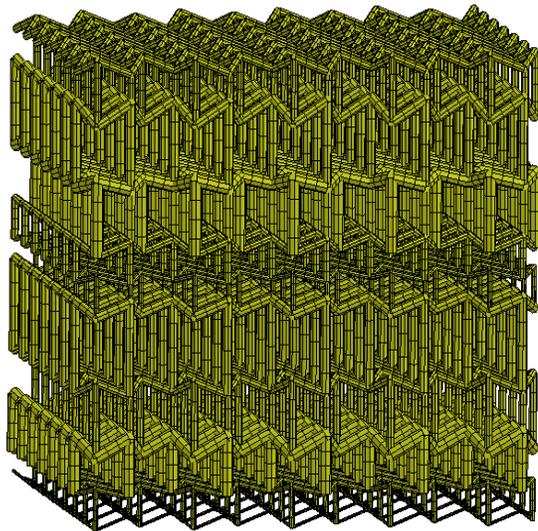


Low velocity impact (200 mm/s)



Functionally graded porosity

- How can we achieve graded porosity?
 - To modify struts thickness
 - To modify geometry of the structure
 - To modify struts thickness and geometry of the auxetic structure

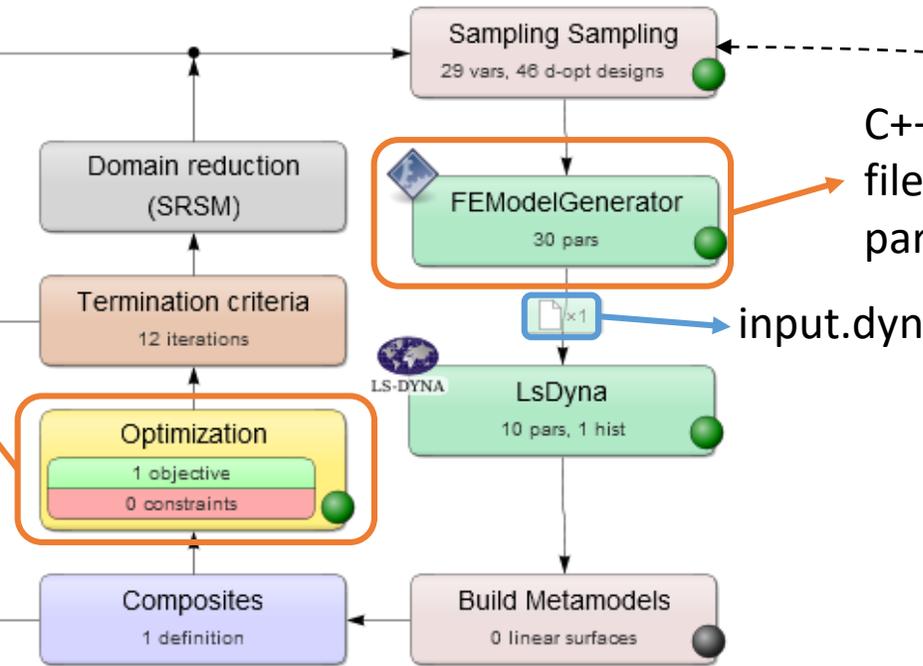
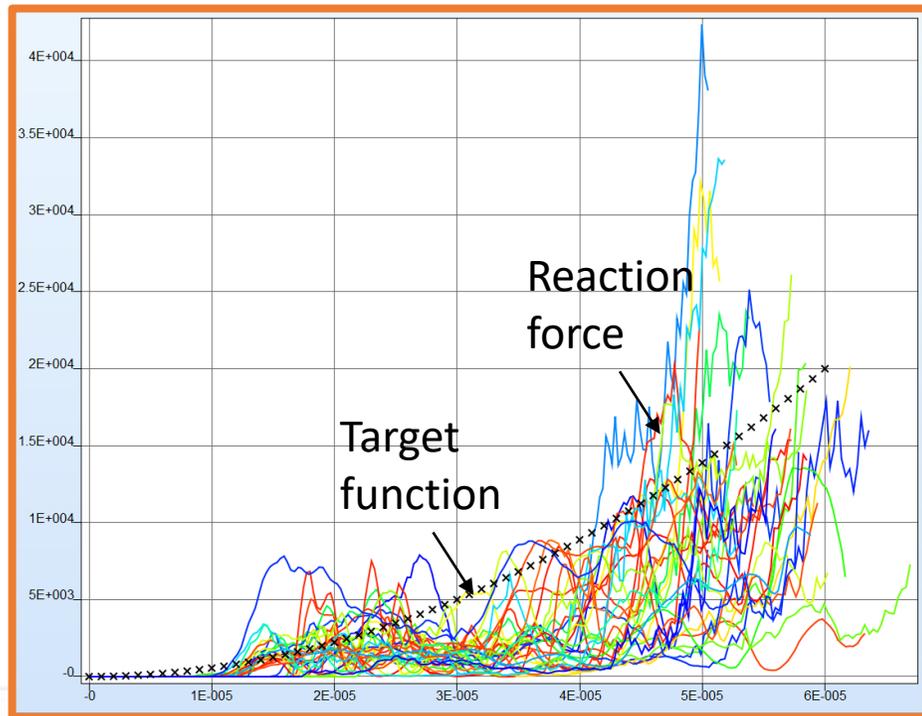


Functionally graded porosity

- Ls-Opt optimisation software



- curve matching and MSE composite (e.g. compare reaction force with target function)

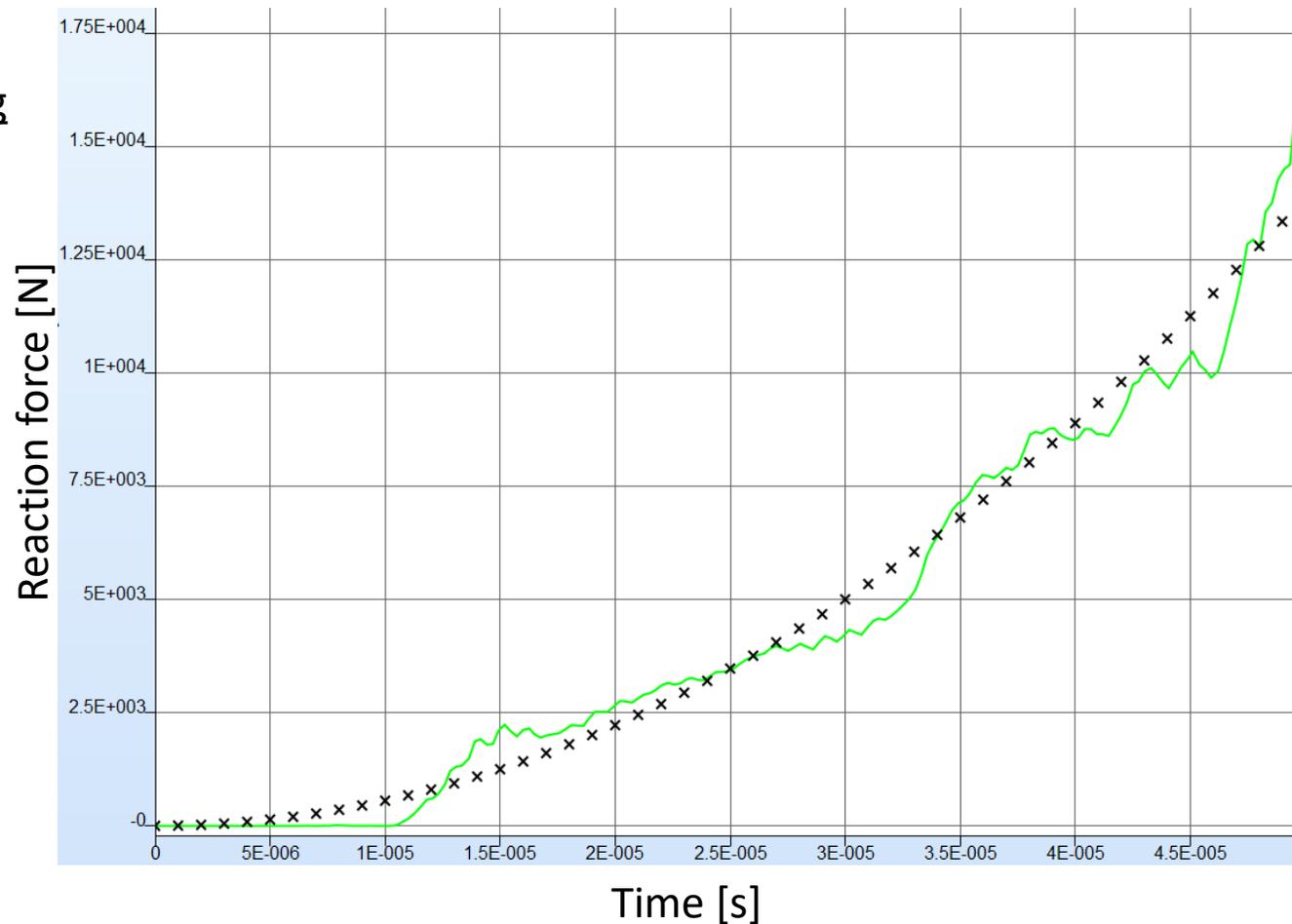


C++ code generates input file based on the geometry parameters

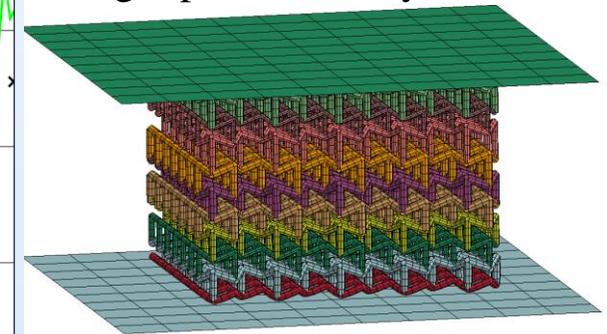
Case study

- Reaction force on bottom plate have progressive characteristic

Iteration 12
Curve mapping



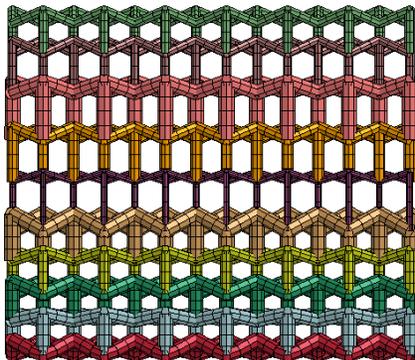
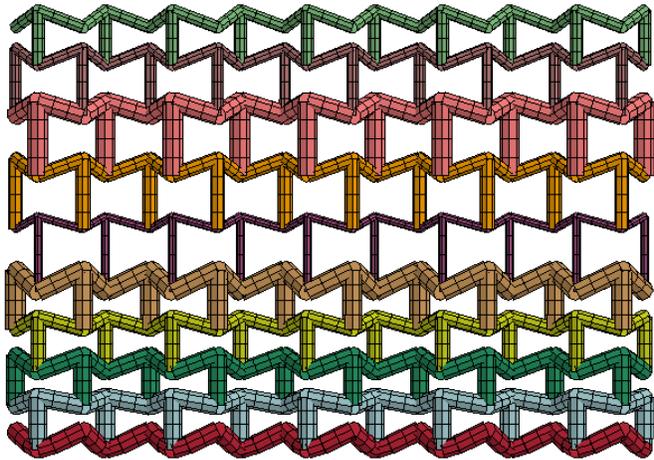
Rigid plate: velocity 200 m/s



Fixed rigid plate

Case study

- Reaction force on bottom plate have progressive characteristic



Conclusions and future prospects

- Auxetic cellular structures built from inverted tetrapods were introduced
- Auxetic structures were experimentally tested
- Two different numerical models were developed and validated
- New auxetic geometries with functionally graded porosity were developed based on validated numerical models
- Future work:
 - Auxetic structures built from more ductile material
 - Validation of numerical models with dynamic experimental testing of functionally graded auxetic materials
 - Detect limit velocity at which structure still have adequate time to react in Ls-Dyna and experiments
 - Development of new graded auxetic structures with user defined response on particular loading conditions



Thank you for your attention!

