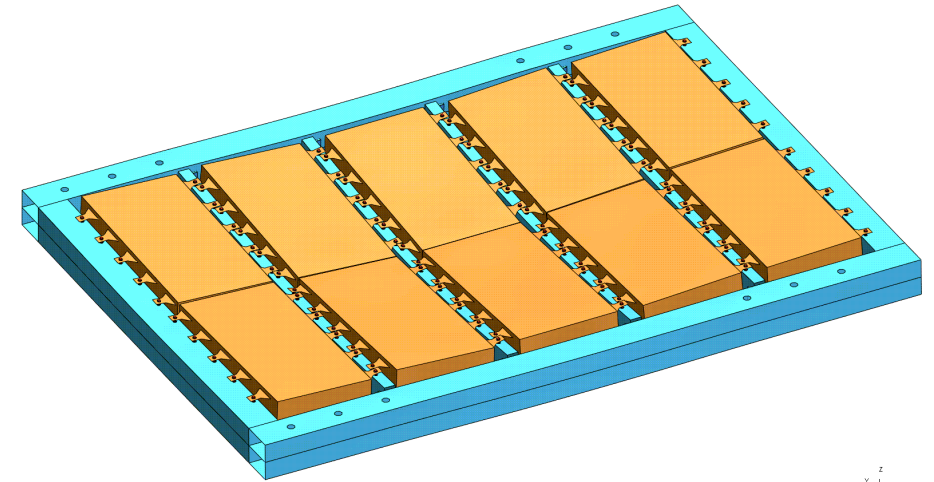


Fatigue assessment of an adhesively bonded EV battery enclosure

Using LS-DYNA implicit tools



David McLennan

Presented by *Emily Owen*

Oasys | LS-DYNA ENVIRONMENT

**Automotive
consulting**

Crash performance

Pedestrian safety

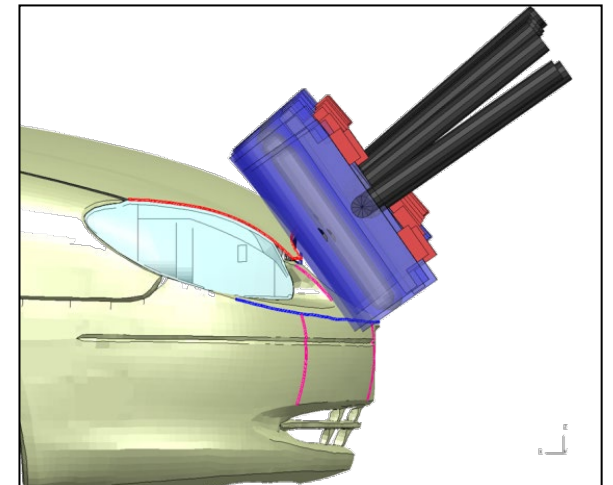
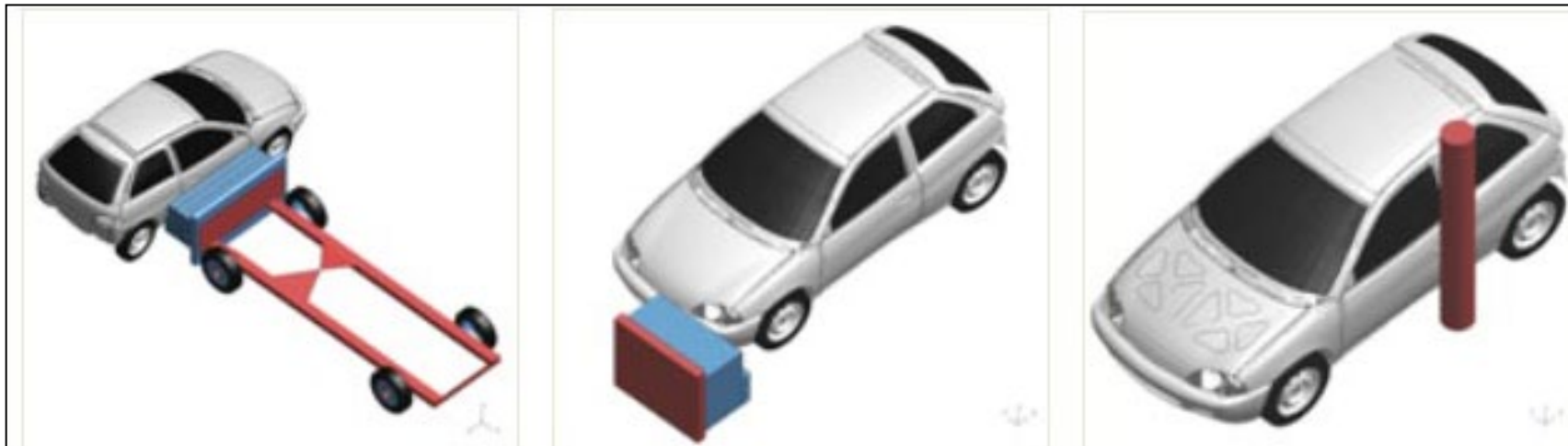
Occupant safety

Interior systems

Noise, Vibration, Harshness

Durability performance

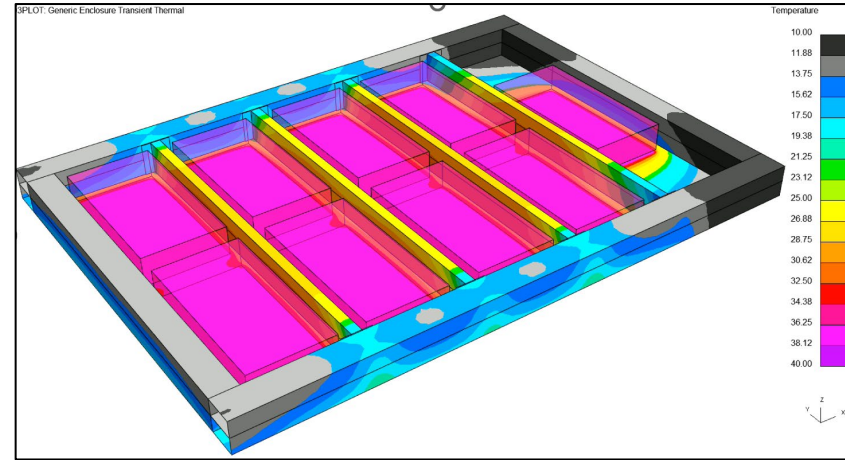
Closures performance



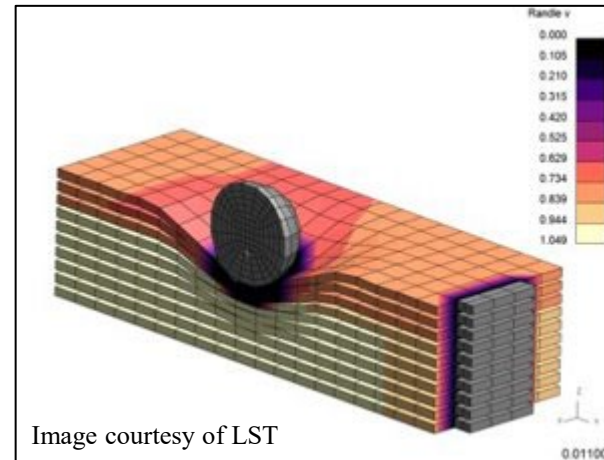
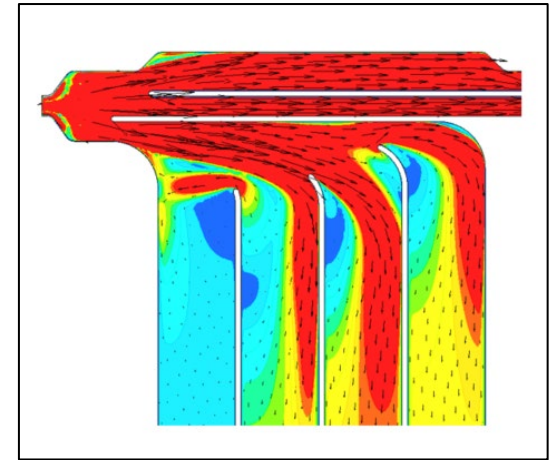
Automotive
consulting

EV battery
consulting

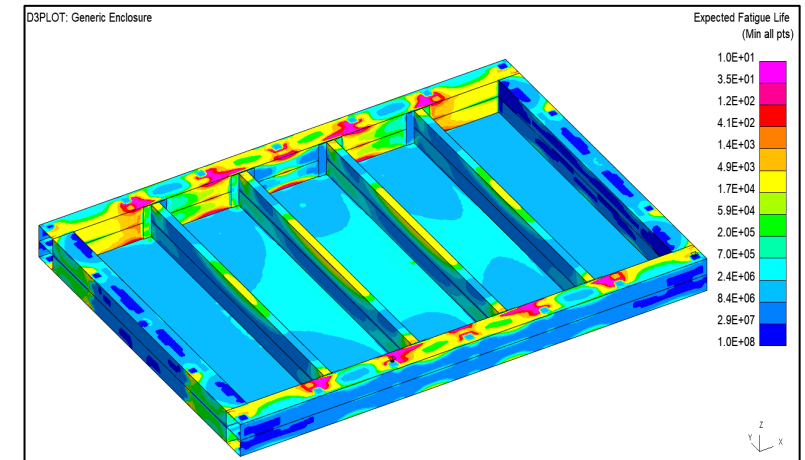
Transient thermal analysis



Coolant flow optimisation



Cell penetration analysis



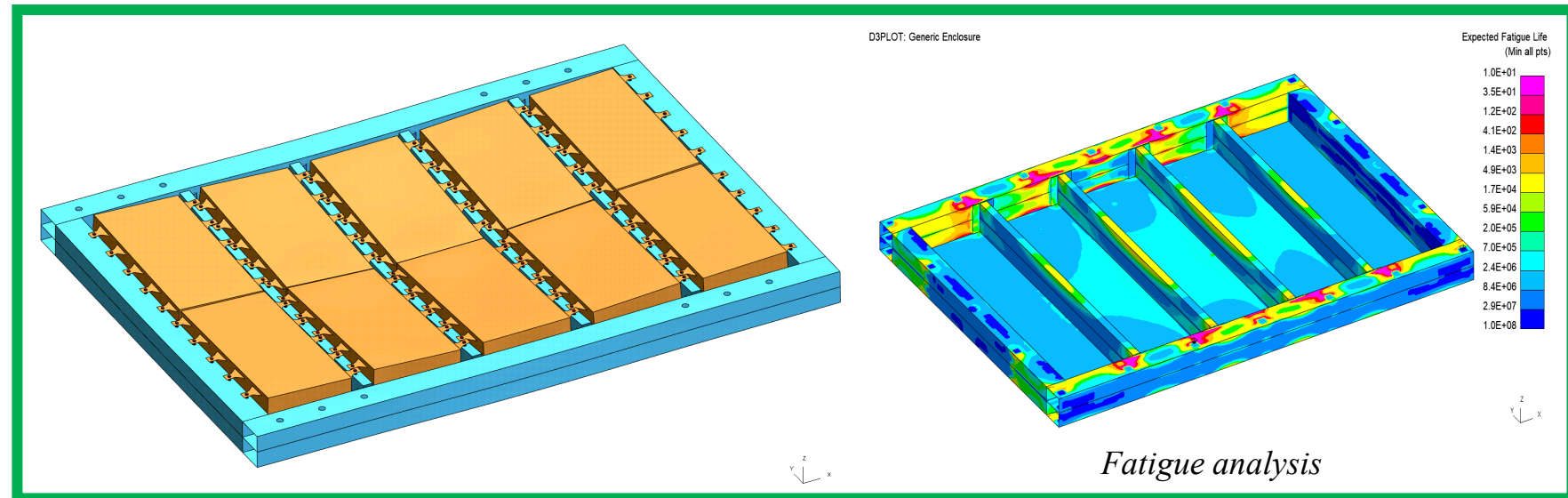
Fatigue analysis

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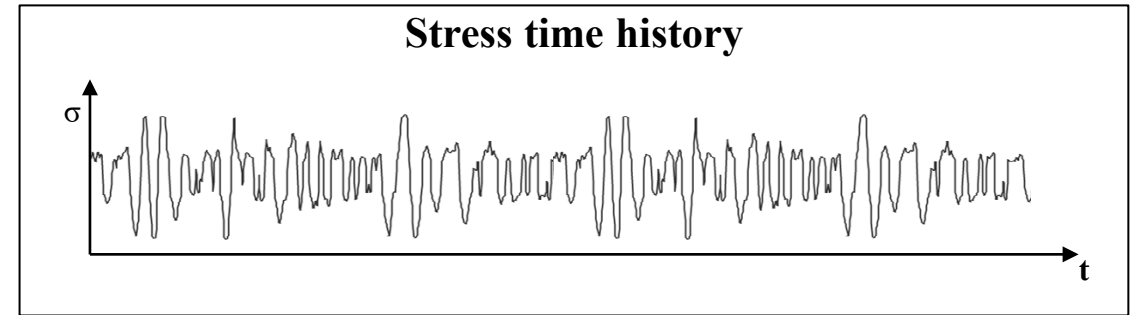
Automotive
consulting

EV battery
consulting

EV battery
enclosure
fatigue

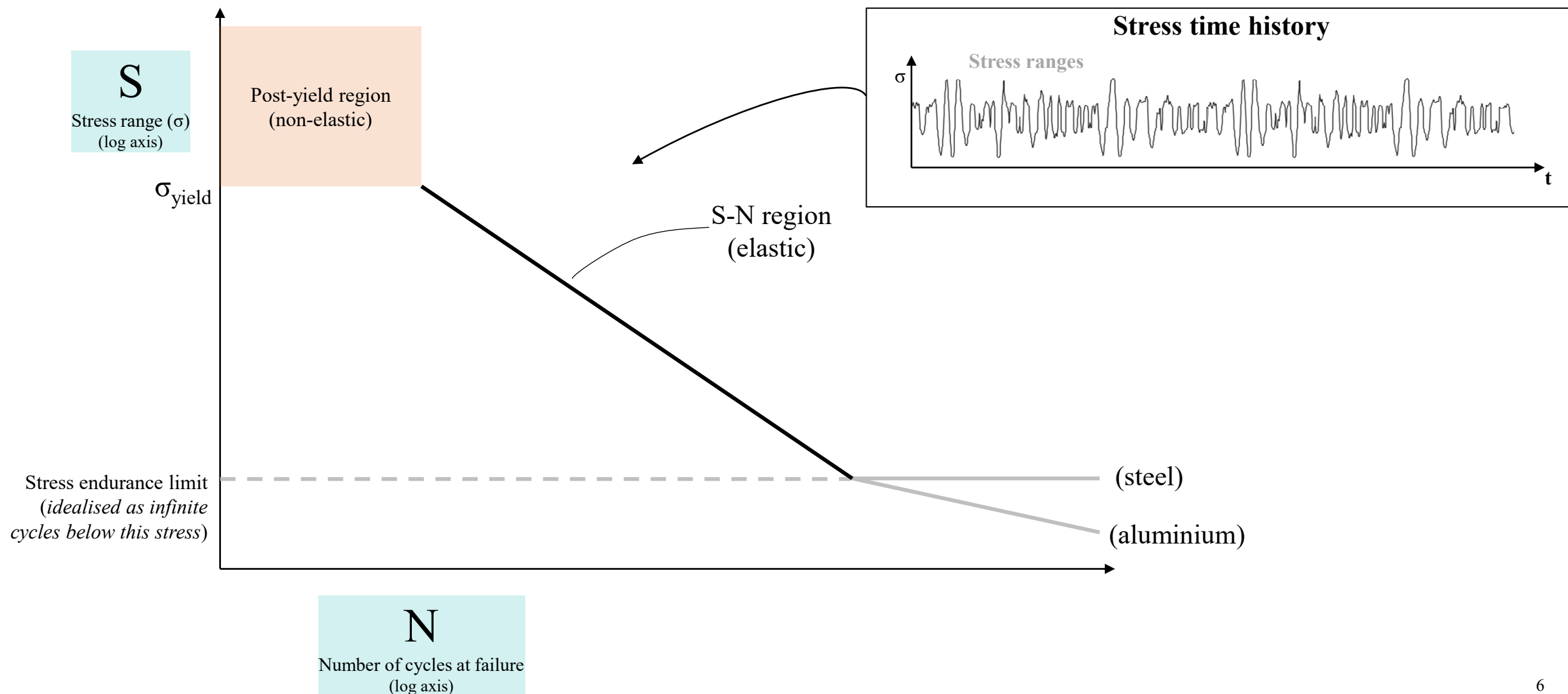


What is fatigue?

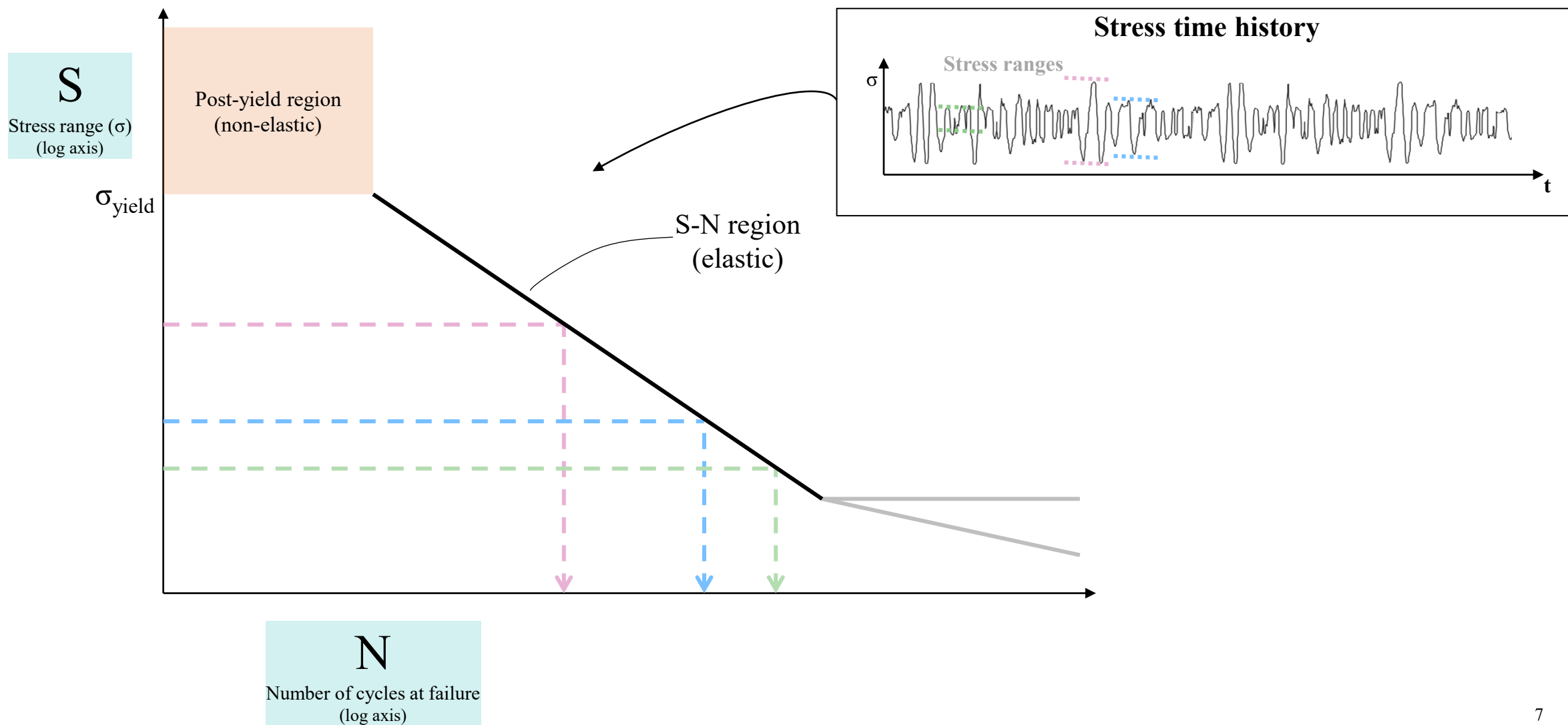


- Eurocode 9 definition:
“weakening of a structural component, through crack initiation and propagation, caused by repeated stress fluctuations”
- Fatigue failure occurs from stress cycles *lower* than the component’s yield stress

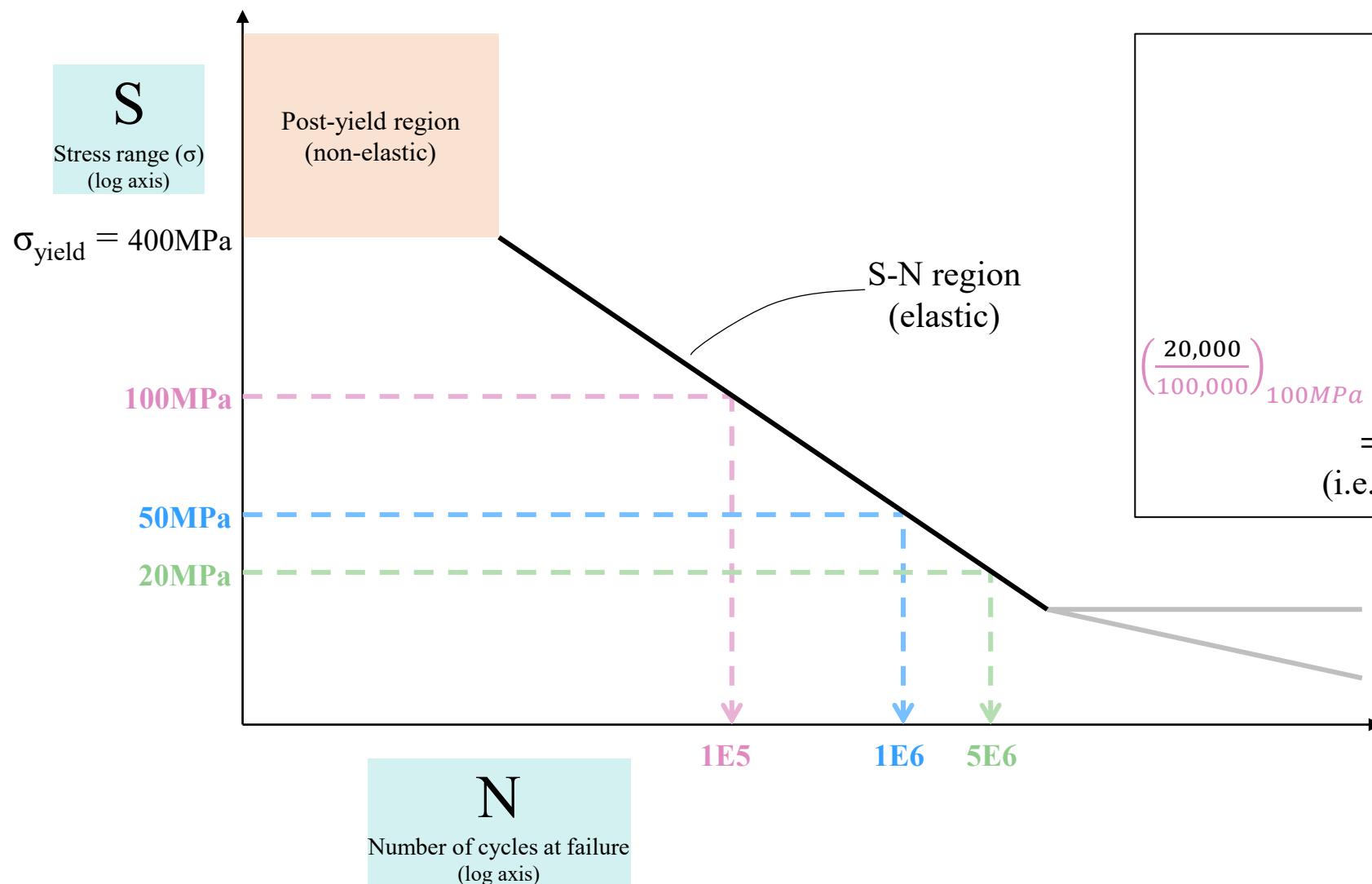
Fatigue assessments – S-N curves



Fatigue assessments – S-N curves



Fatigue assessments – S-N curves



Miner's rule
(Cumulative Damage Ratio)

$$\sum_i \frac{n_i}{N_i}$$

For example:

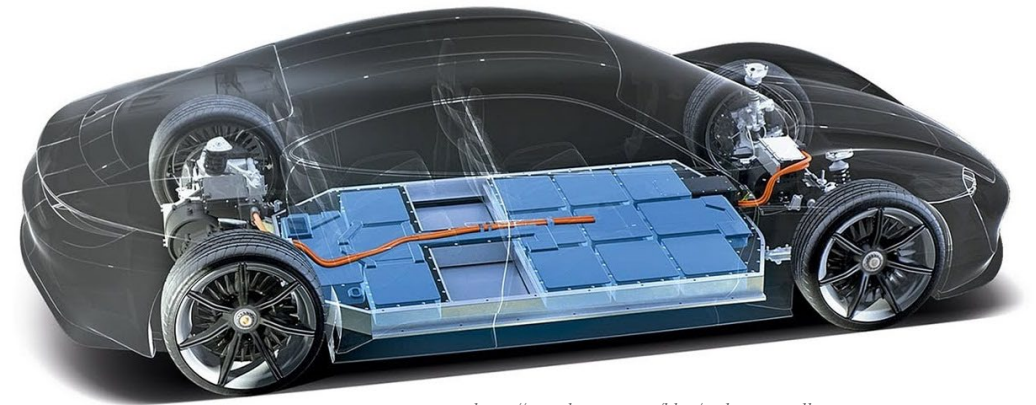
$$\left(\frac{20,000}{100,000}\right)_{100\text{MPa}} + \left(\frac{100,000}{1,000,000}\right)_{50\text{MPa}} + \left(\frac{2,000,000}{5,000,000}\right)_{20\text{MPa}}$$

$$= 0.2 + 0.1 + 0.4 = 0.7$$

(i.e. 70% of fatigue life used)

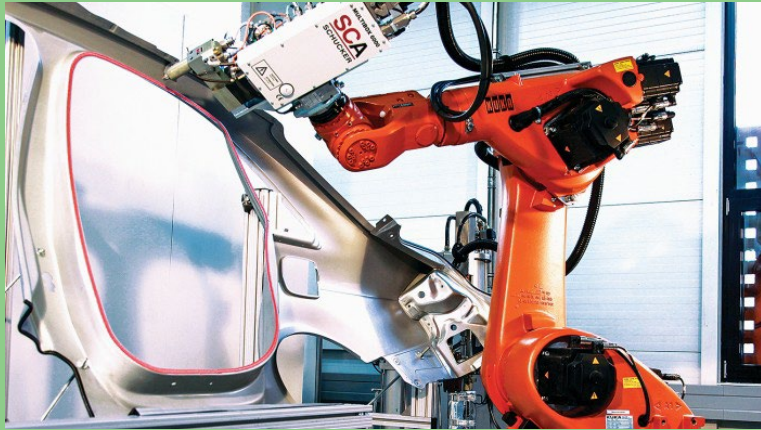
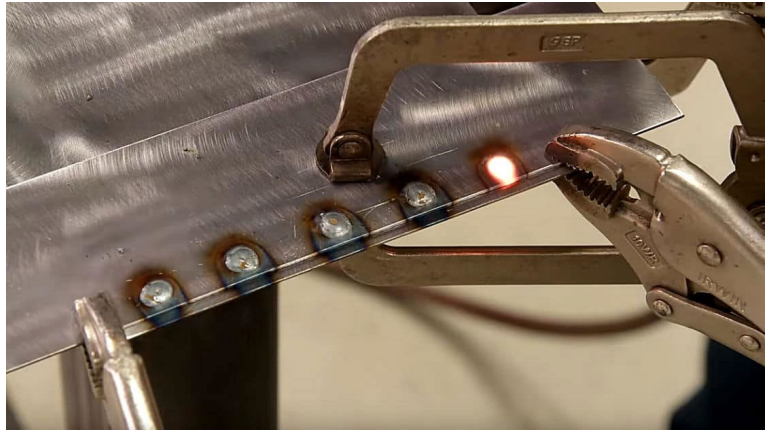
Fatigue risks for EV battery enclosures

- The battery enclosure must have sufficient strength/stiffness to:
 - Protect the batteries during a vehicle crash event
 - Contribute to overall stiffness of the vehicle
 - Provide containment in the event of thermal runaway
 - Withstand inertial loads from the mass of the batteries
- Total mass of “battery modules + enclosure” can be ~0.5-1.0 tonnes

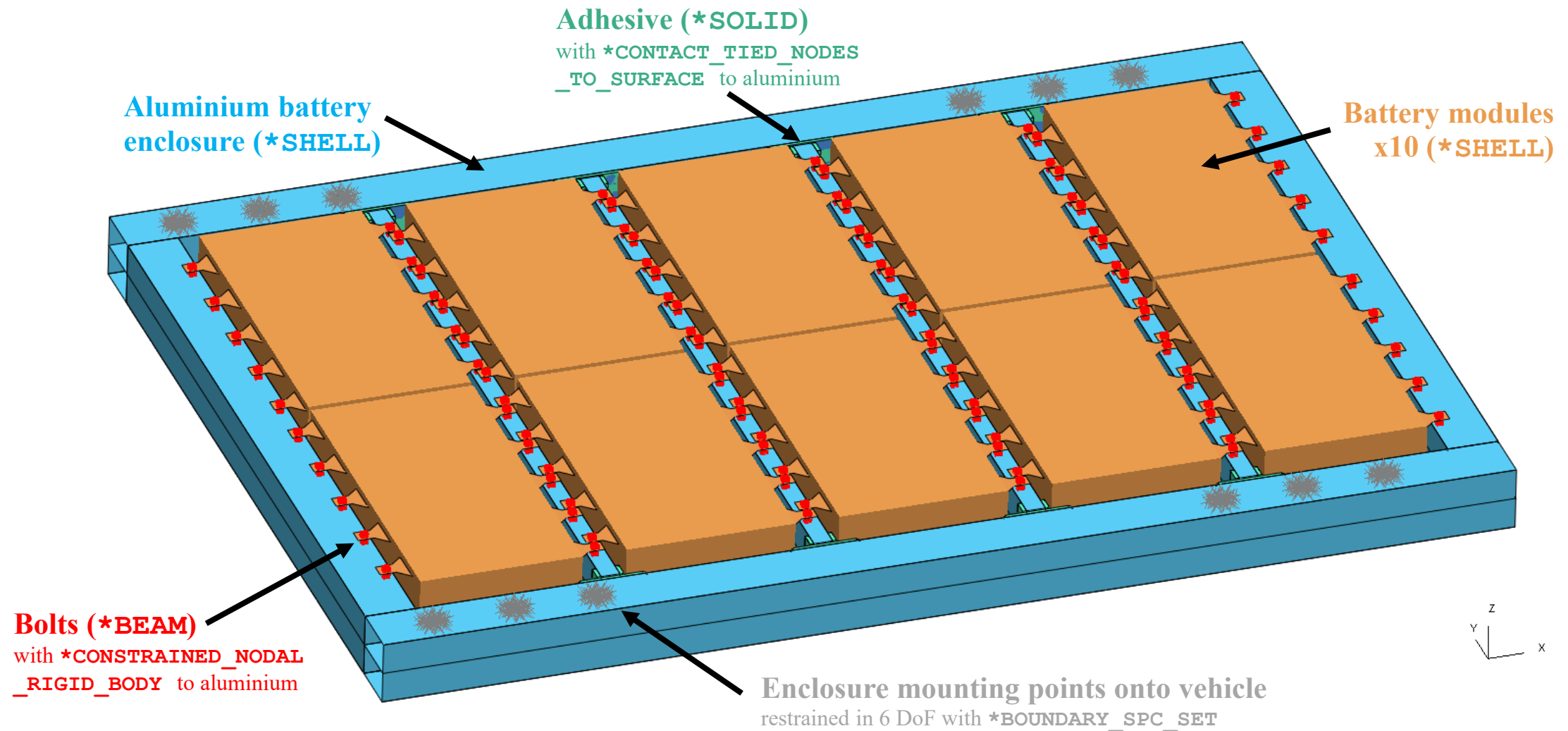


<https://www.laserax.com/blog/ev-battery-cell-types>

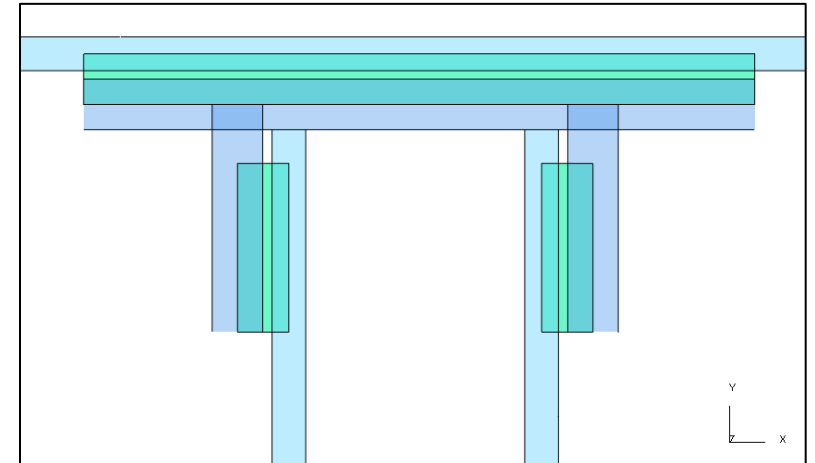
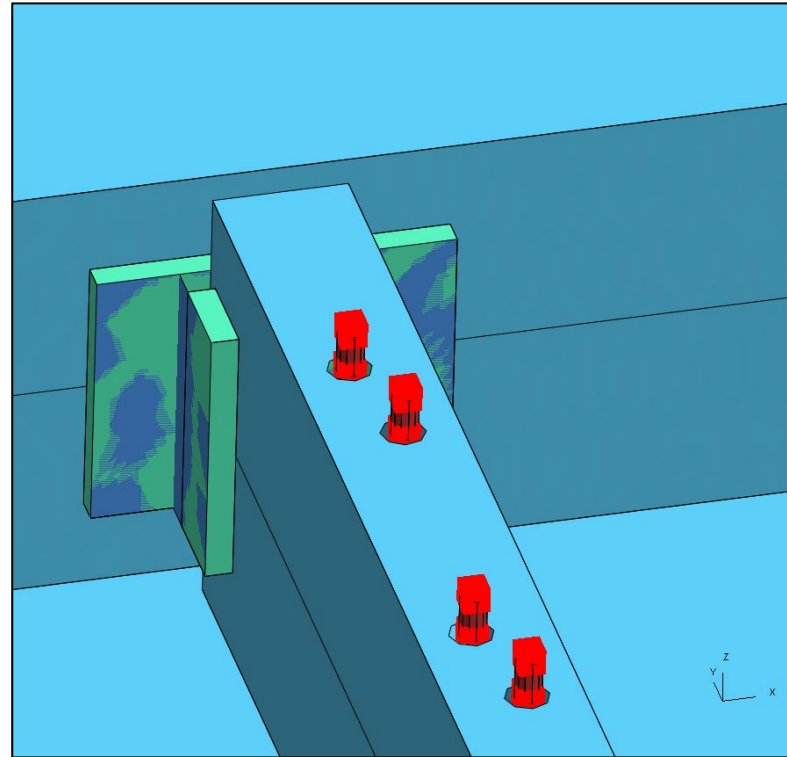
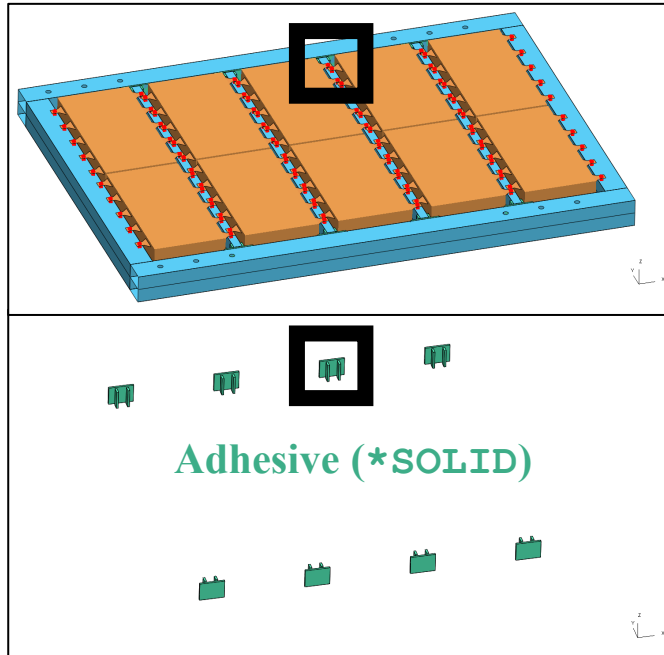
The rise of adhesively bonded designs

	Adhesive bonding	Spotwelds
Connection type	Continuous (large area) connections	Discrete (small area) connections
Most common for	Aluminium structures	Steel structures
Material properties	Overall lightweight solution, and does not affect strength of parent aluminium material	Typically not suitable for aluminium, due to heat weakened zone around the weld
Fatigue assessment	Emerging area of study	Established methods
	 <p>https://cen.acs.org/articles/92/i16/Automakers-Look-Adhesives-Aluminum-Gas.html</p>	 <p>https://m.roadkillcustoms.com/how-to-simulate-resistance-spot-welds/</p>

Fatigue assessment: LS-DYNA model



Fatigue assessment: LS-DYNA model



↑ *SHELL visualised as “true thickness”

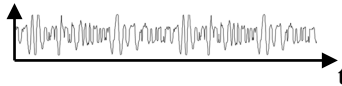
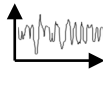

← *SHELL visualised as “thin line”

- Adhesive ***SOLID** elements modelled from mid-surface to mid-surface of adjacent aluminium plates
- Using ***MAT_ARUP_ADHESIVE**, defined with 0.3mm bond thickness

LS-DYNA implicit solvers

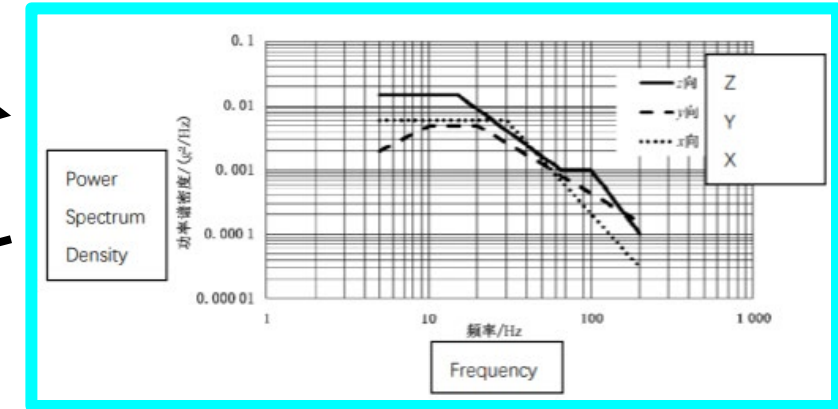
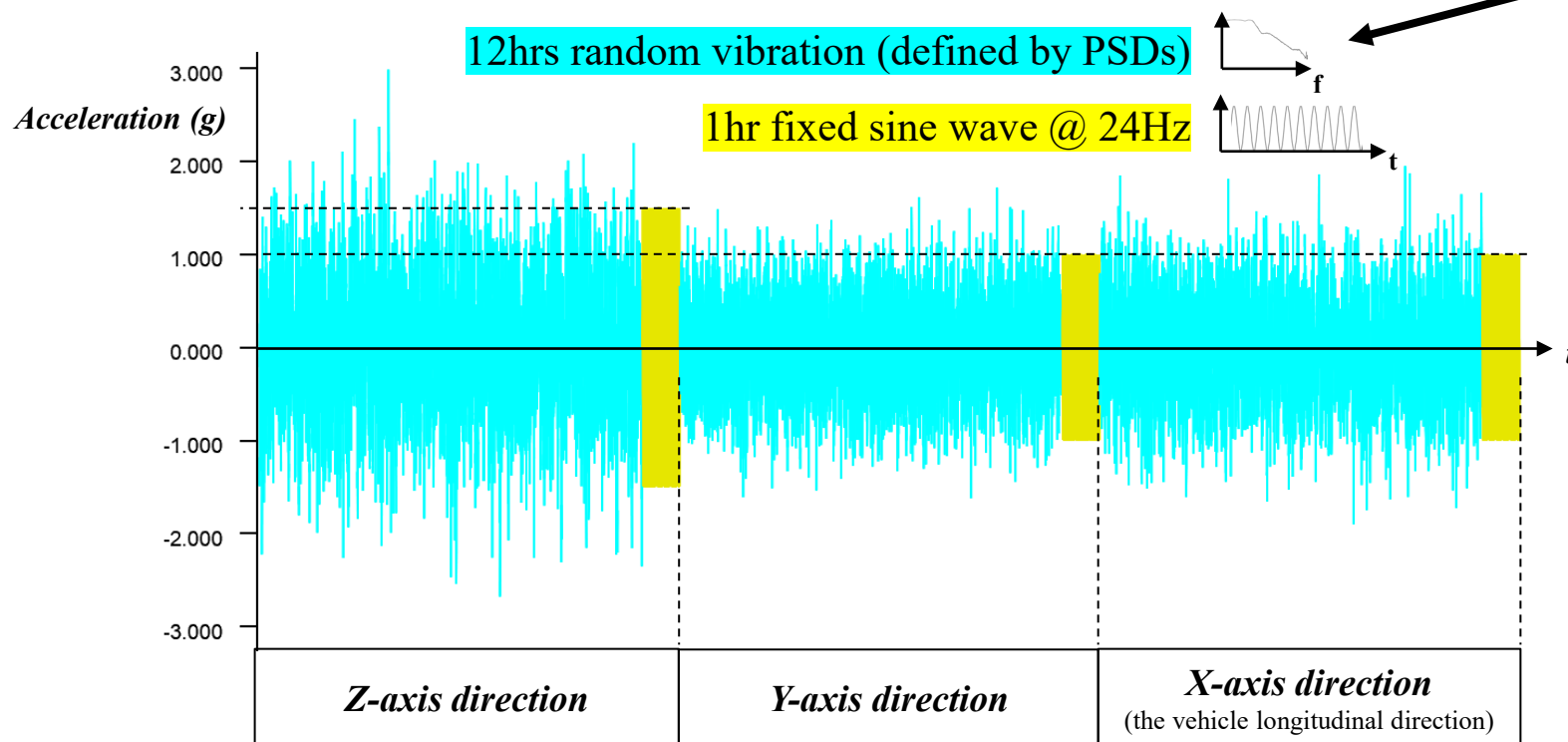
Keyword	Comment
*CONTROL_IMPLICIT_GENERAL	Activates implicit mode and defines timestep
*CONTROL_IMPLICIT_AUTO	Activates automatic timestep control
*CONTROL_IMPLICIT_SOLVER	Defines linear equation solver
*CONTROL_IMPLICIT_SOLUTION	Defines equilibrium search and convergence tolerances
*CONTROL_IMPLICIT_EIGENVALUE	Normal modal analysis Equivalent to NASTRAN SOL103
*FREQUENCY_DOMAIN_FRF	Direct freq-domain response analysis Equivalent to NASTRAN SOL108
*CONTROL_IMPLICIT_DYNAMICS	Direct time-domain response analysis Equivalent to NASTRAN SOL109
*FREQUENCY_DOMAIN_RANDOM_VIBRATION(_FATIGUE)	Modal freq-domain response analysis to random vibration Equivalent to NASTRAN SOL111
*FREQUENCY_DOMAIN_SSD(_FATIGUE)	Modal freq-domain response analysis to steady state dynamics Equivalent to NASTRAN SOL111
*CONTROL_IMPLICIT_MODAL_DYNAMIC	Modal time-domain response analysis Equivalent to NASTRAN SOL112
<i>...and many more</i>	

Predicting fatigue performance of structures

	Random vibration fatigue assessment using...	
	Time domain	Frequency domain
Physical tests	With random cyclic loading, until test specimen fails 	n/a
FE analysis	Random transient input loading  Slower analysis than frequency domain, producing more data (therefore, need to focus on regions of greatest importance) More flexibility with the fatigue assessment methodology (post-processing on time history results) Element stress time histories to count cycles at each stress range	Random input loading from a defined PSD [†]  Fast analysis method, which outputs element stress PSDs [†] (therefore, can assess all elements and do many studies) Constrained to standard freq-domain fatigue assessment methods Using PSD [†] statistics to obtain cycles at each stress range
	Fatigue damage calculated via comparison to failure cycles (S-N curve, Miner's rule)	
	*CONTROL_IMPLICIT_MODAL_DYNAMIC	*FREQUENCY_DOMAIN_RANDOM_VIBRATION_FATIGUE *FREQUENCY_DOMAIN_SSD_FATIGUE

Fatigue assessment: vibration load cases

- Objective:** to pass the “*GB 38031-2020 China Standard*” electric vehicle vibration load cases*, comprising the following sequence of tests (from Table 3 of the regulations):

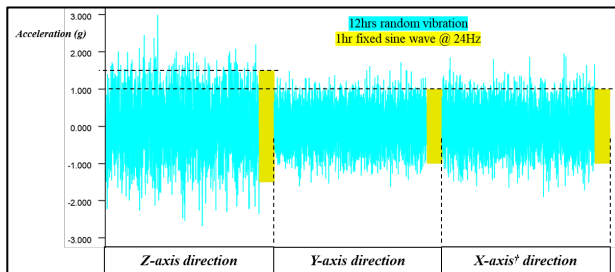


* for vehicle types M1 (passenger cars) and N1 (light goods vehicles, up to 3500kg)

Fatigue assessment: vibration load cases

- **Method:** implementing with LS-DYNA implicit solvers, using keywords:

GB 38031-2020 China Standard		Fatigue assessment for...	
Loading method...	Random vibration	Adhesive SOLIDs	Aluminium SHELLs
		*CONTROL_IMPLICIT _MODAL_DYNAMIC <i>X, Y, Z loading (analysed in the time domain)</i>	*FREQUENCY_DOMAIN _RANDOM_VIBRATION_FATIGUE <i>X, Y, Z loading (analysed in the frequency domain)</i>
	Fixed sine wave	*FREQUENCY_DOMAIN _SSD_FATIGUE <i>X, Y, Z loading (analysed in the frequency domain)</i>	

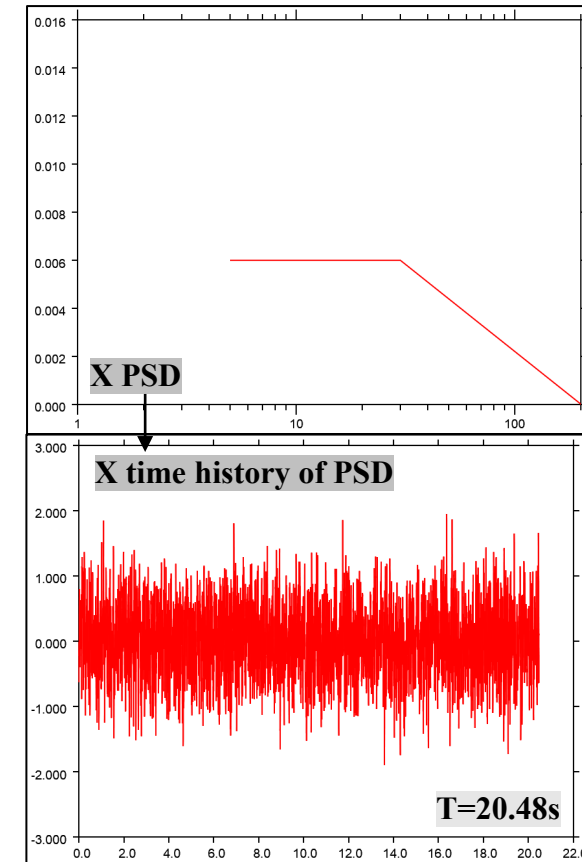
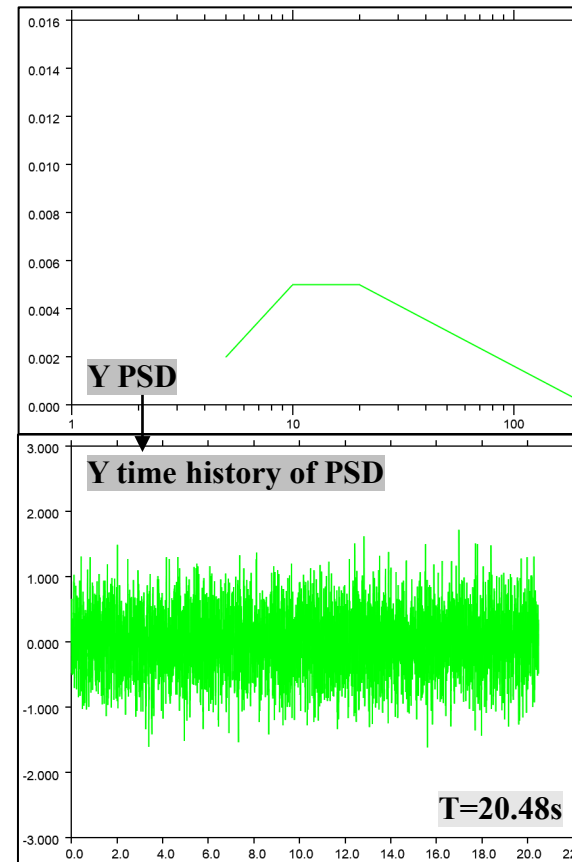
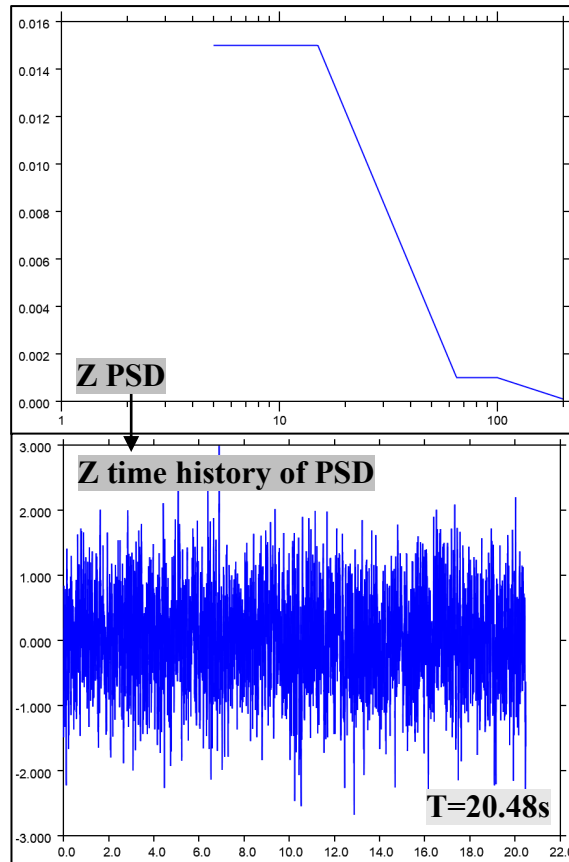


Analysed in the time domain to allow fatigue calculations using the *Sousa method* [1], requiring time histories of adhesive element stresses

Fatigue assessment: vibration load cases

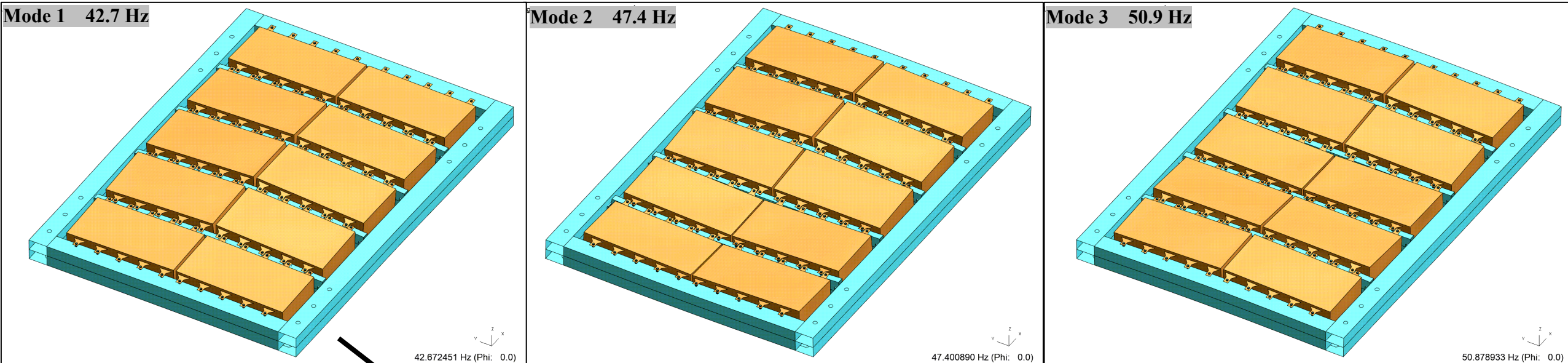
*PSD (g^2 / Hz)
vs frequency (Hz)*

*GB 38031-2020
China Standard*



- MATLAB script has generated random time signals from each PSD
- Time signal must be long enough to accurately capture the contents of the PSD
- A good check is then to create a PSD from the generated time signal, to compare to the original

Modal analysis results



From the modal analysis results...

Estimate the number of **cycles within the load case** ($n_{load\ case}$):

$$n_{load\ case} = (12*60*60)\ sec * 42.7\ Hz = \mathbf{1,844,640\ cycles}$$

Noting that the load case duration is 12 hours, and assuming vibration purely at the dominant modal frequency of the structure (42.7 Hz) [†]

[†] note that there are other methods to estimate the number of cycles within the load case

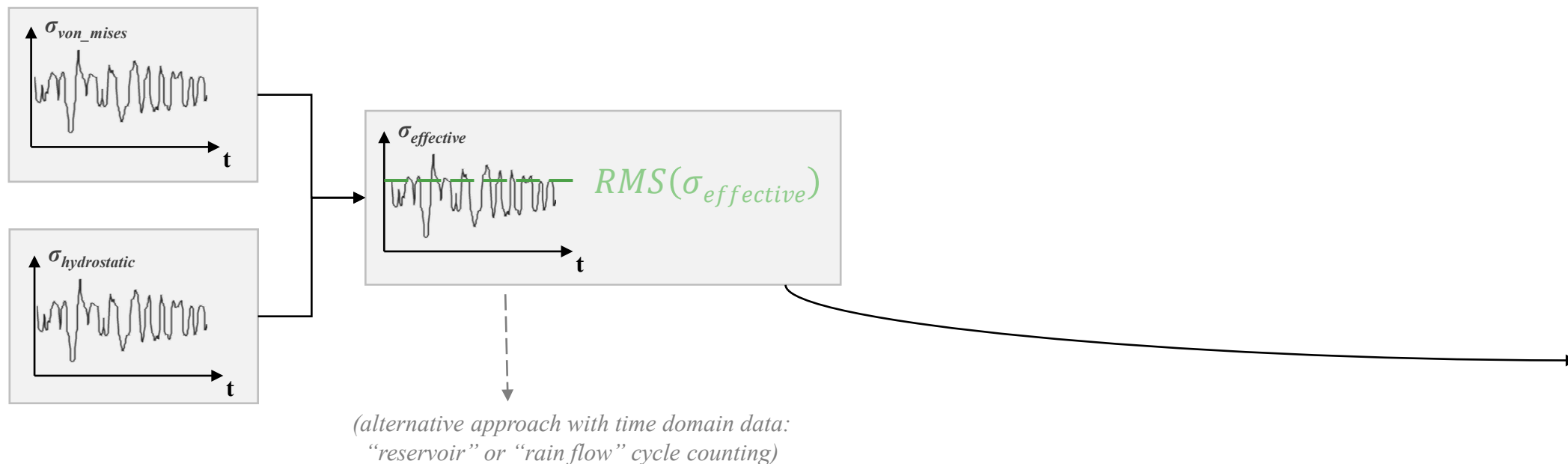
Fatigue assessment: adhesive

The number of **cycles to failure** ($n_{failure}$) for the **adhesive**:

- Requires appropriate values of stress range to be mapped onto the adhesive S-N curve
- **Sousa method**: using an “effective stress”, defined in a paper by *Sousa et al* [1]:

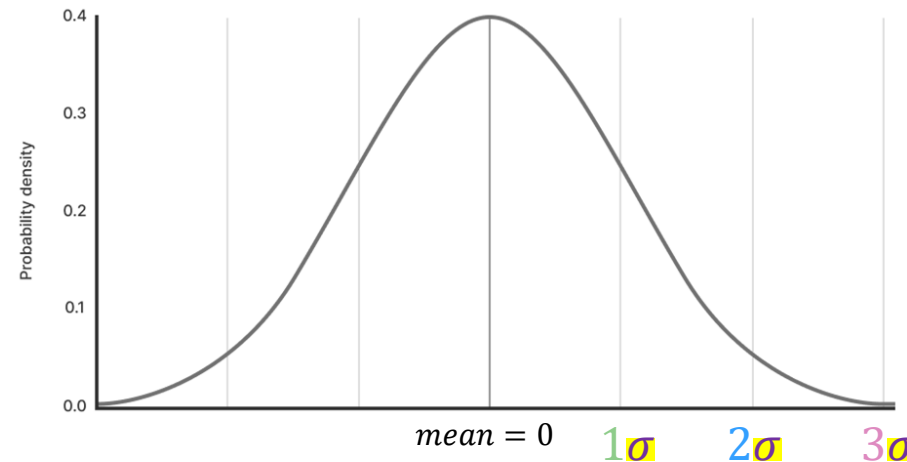
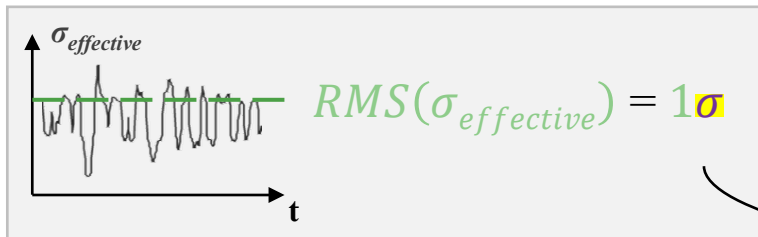
$$\sigma_{effective} = \sigma_{von\ mises} + \sigma_{hydrostatic}^2 / \sigma_{von\ mises}$$

- This “effective stress” was found to correlate best to overall adhesive fatigue damage



Fatigue assessment: adhesive

- One of many methods for fatigue damage assessment
- Using the *Steinberg 3-band method*, which assumes a Gaussian distribution of stress
- The stress range is at:
 - the one standard deviation value ($1\sigma = \text{RMS}^\dagger$) of mean for 68.3% of the time
 - 2σ for 27.1% of the time
 - 3σ for 4.3% of the time



† the Root Mean Square average of the stress time history

σ = the value at **one standard deviation** on a Gaussian (normal) distribution

Fatigue assessment: adhesive

Using the *Steinberg 3-band method*

$$N_1 = 10^{\frac{(\ln(1\sigma) - b)}{m}} \quad \text{where } 1\sigma = \text{RMS}(\sigma_{\text{effective}})$$

$$N_2 = 10^{\frac{(\ln(2\sigma) - b)}{m}} \quad 2\sigma = 2 * (1\sigma)$$

$$N_3 = 10^{\frac{(\ln(3\sigma) - b)}{m}} \quad 3\sigma = 3 * (1\sigma)$$

$$n_{\text{failure}} = 1.0 / \left(\frac{0.683}{N_1} + \frac{0.271}{N_2} + \frac{0.043}{N_3} \right)$$

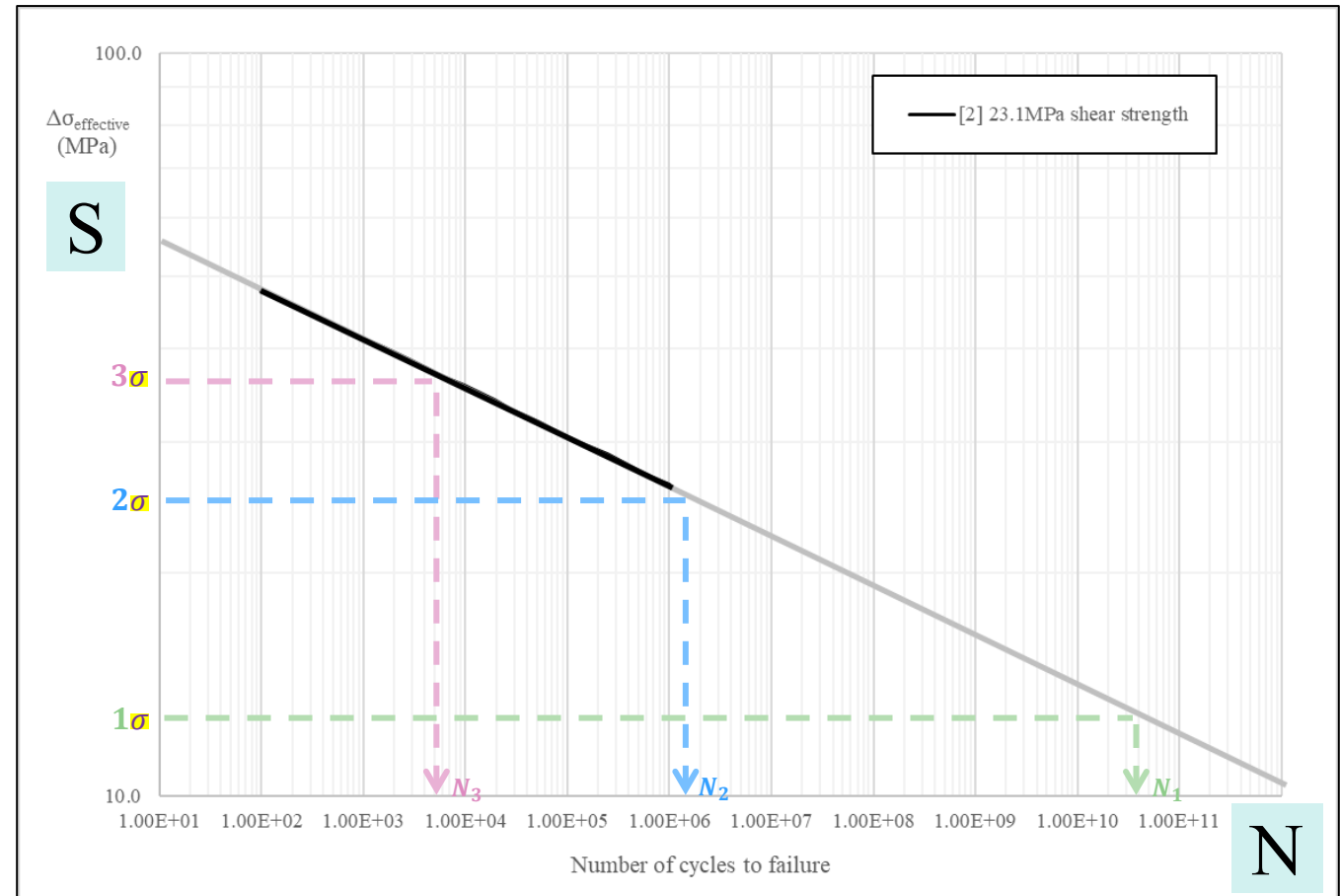
Fatigue damage

$$= \frac{n_{\text{load case}^*}}{n_{\text{failure}}}$$

$$= \frac{\text{\#cycles during the vibration test}}{\text{\#cycles at which adhesive will fail}}$$

Note: Damage > 1 is a prediction of fatigue failure

* e.g. 1,844,640 cycles



Castra Sousa, F, Akhavan-Safar, A, Goyal, R, da Silva, L.F.M. Fatigue life estimation of single lap adhesive joints using a critical distance criterion: An equivalent notch approach. *Mechanics of Materials* 2021;153

σ = the value at **one standard deviation** on a normal (Gaussian) distribution

Fatigue assessment: aluminium

Using the *Dirlik method*

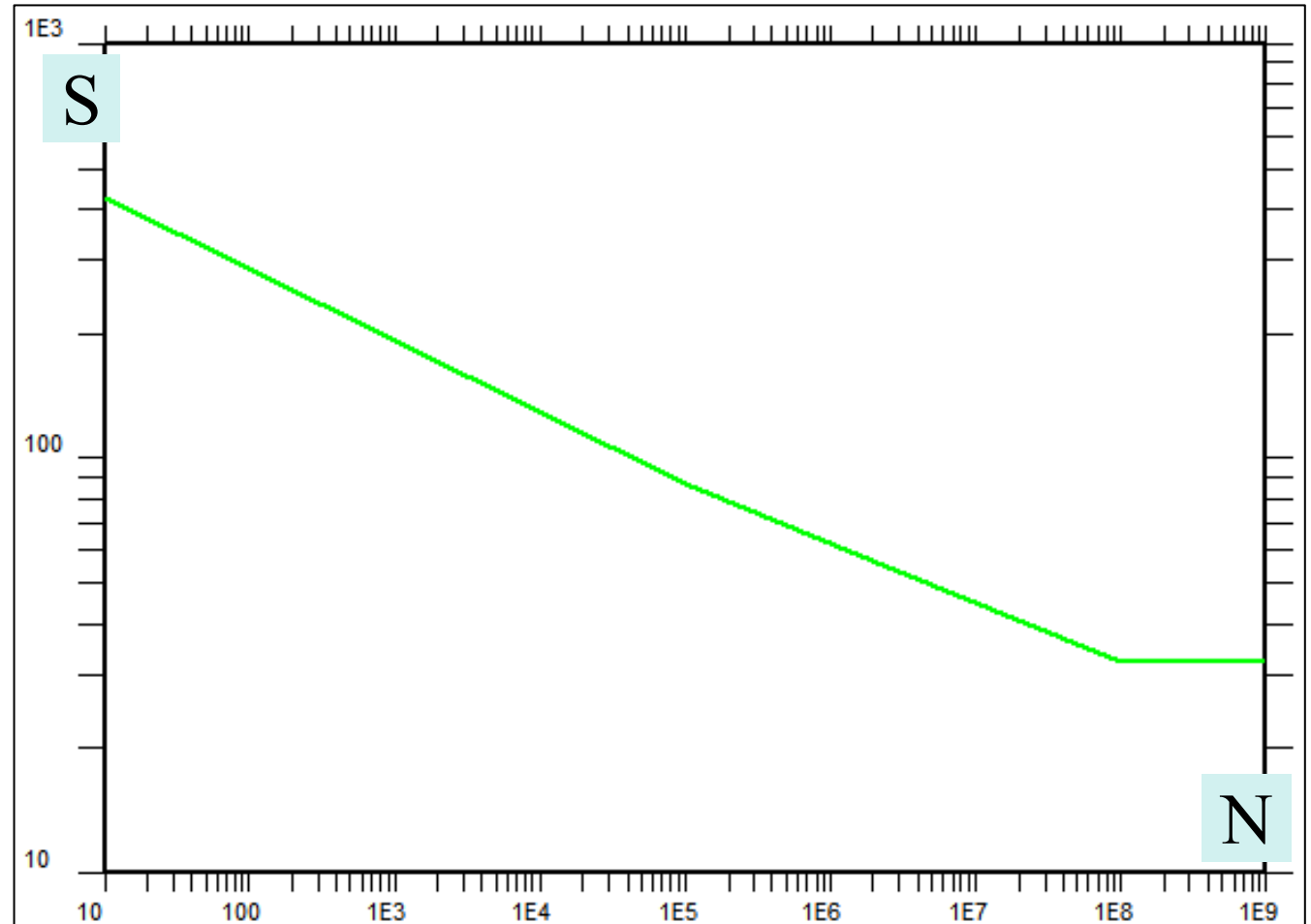
- Embedded within LS-DYNA
- Converts the PSD into a PDF (probability density function)[†] to create stress ranges
- Using input exposure time (12*60*60 sec)
- Performs $n_{failure}$ and $n_{load\ case}$ calculations

Fatigue damage

$$= \frac{n_{load\ case}}{n_{failure}}$$

$$= \frac{\#cycles\ during\ the\ vibration\ test}{\#cycles\ at\ which\ aluminium\ will\ fail}$$

Note: Damage > 1 is a prediction of fatigue failure

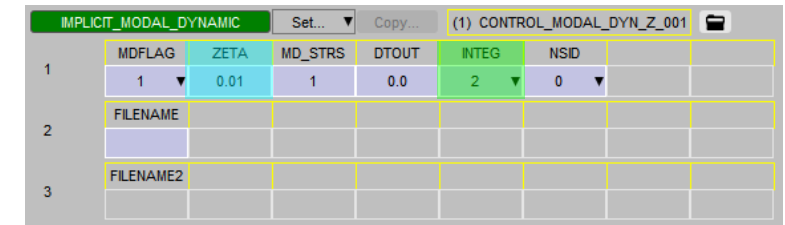


BS EN 1999-1-3:2007 Eurocode 9: Design of aluminium structures
Part 1-3: Structures susceptible to fatigue
"125-7" from Figure J.1 / Table J.2

[†] the Dirlik method PDF expression was originally derived from empirical simulations, using Monte Carlo sampling

*CONTROL_IMPLICIT_MODAL_DYNAMIC

- Implicit time-domain analysis using modal superposition
- First computes a modal analysis (***CONTROL_IMPLICIT_EIGENVALUE**)
- Applies the transient loading (using ***LOAD_BODY**, for X, Y, and Z separately)
- ZETA = modal damping ratio = 0.01 (1%_{critical})
- INTEG = computed with implicit time integration
- Uses modal superposition to obtain an overall response (a linear combination of the transient results), using all modes from ***CONTROL_IMP_EIGENVALUE** (NEIG)
- This modal transient approach is more efficient than a direct transient analysis
- Fatigue damage is calculated separately during post-processing, therefore an S-N curve is not given as input to LS-DYNA (refer back to the explanation of the *Steinberg 3-band method* and *Sousa method* for assessing the adhesive)



	MDFLAG	ZETA	MD_STRS	DTOUT	INTEG	NSID		
1	1	0.01	1	0.0	2	0		
2	FILENAME							
3	FILENAME2							

*FREQUENCY_DOMAIN_RANDOM_VIBRATION_FATIGUE

- Implicit frequency-domain analysis using modal superposition
- First computes a modal analysis (***CONTROL_IMP_EIG**)
- Range of modes used for modal superposition
- DAMPF = modal damping ratio = 0.01 (1%_{critical})
- STRTYP, STRSF = using Von Mises stress, stress range
- TEXPOS = exposure time to the PSD (i.e. length of vibration test) = $12 \times 60 \times 60 = 43200$ sec
- Using PSDs (g^2/Hz), with separate analyses for X, Y, Z
- _FATIGUE option computes cumulative damage
- Fatigue analysis method (2 = *Dirlik method*)
- S-N curve to be applied to all aluminium parts

MODIFY FREQUENCY_DOMAIN_RANDOM_VIBRATION 1

Update Reset All Check Sketch Only Cancel Copy In X-Refs Text Edit

Include: (1) FREQ_DOMAIN_RAND_VIB_FAT_Z_004

Modify FREQUENCY_DOMAIN_RANDOM_VIBRATION 1 (model 1)

<_OPTION>

☐ <BLANK> ☒ _FATIGUE

MDMIN	MDMAX	FMIN	FMAX	RESTR1	RESTRM
1	50	0.0	0.0	0	0

DAMPF	LCDAM	LCTYP	DMPMAS	DMPSTF	DMPTYP
0.01	0	0	0.0	0.0	0

VFLAG	METHOD	UNIT	UMLT	VAPSD	VARMS	NAPSD	NCPSD
1	0	4	0.0	1	1	1	0

LDTYPE	IPANELU	IPANELV	TEMPER	LDFLAG	ICOARSE	TCOARSE
0	0	0	0.0	0	0	0.0

MFTG	NFTG	STRTYP	TEXPOS	STRSF	INFTG
2	1	0	43200.0	1.0	0

SID	STYPE	DOF	LDPSD	LDVEL	LDLW	LDSPN	CID
0	0	3	64	0	0	0	0

LOAD_I	LOAD_J	LCTYP2	LDPSD1	LDPSD2

PID	LCID	PTYPE	LTYPE	A	B	STHRES	SNLIMIT
50	61	1	1	0.0	0.0	0.0	0

FILENAME

*FREQUENCY_DOMAIN_SSD_FATIGUE

- Implicit frequency-domain analysis using modal superposition
- First computes a modal analysis (***CONTROL_IMP_EIG**)
- Range of modes used for modal superposition
- DAMPF = modal damping ratio = 0.01 (1%_{critical})
- STRTYP = using Von Mises stress
- LCFTG = the duration of each frequency during the vibration test = $1 \times 60 \times 60 = 3600$ sec @ 24 Hz
- Acceleration @ 24 Hz, with separate analyses for X, Y, Z
- **FATIGUE** option computes cumulative damage
- S-N curve to be applied to all aluminium and adhesive parts (defined using ***MAT_ADD_FATIGUE**)
- SNTYP = using stress range

MODIFY FREQUENCY_DOMAIN_SSD 1

Update Reset All Check Sketch Only Cancel Copy In X-Refs Text Edit

Include: M1 <Master file>

Modify FREQUENCY_DOMAIN_SSD 1 (model 1)

<_OPTION>

_FATIGUE

MDMIN	MDMAX	FNMIN	FNMAX	RESTMD	RESTDP	LCFLAG	RELATV
1	50	0.0	0.0	0	0	0	0

DAMPF	LCDAM	LCTYP	DMPMAS	DMPSTF	DMPFLG
0.01	0	0	0.0	0.0	0

ISTRESS	MEMORY	NERP	STRTYP	NOUT	NOTYP	NOVA
0	0		0	0	0	0

RO	C	ERPLF	ERPREF	RADEFF

CASEID	TITLE	NLOAD

ND	NTYP	DOF	VAD	LC1	LC2	SF	VID
0	0	3	3	22	33	0.0	0

LCFTG 44

MODIFY MATERIAL M1/MAT4

Update Reset All Check Sketch Only Import from database... Cancel Copy In X-Refs Text Edit

Include: (1) FREQ_DOMAIN_SSD_FAT_Z_001.key

Modify material M1/MAT4

Label: 4 Etypes: H, S, B, TS, SPH, IGA

Type: MAT_003: PLASTIC_KINEMATIC

Suffix: <none>

Title: <No material name given>

ADD_EROSIO EDIT ADD_PORE_A EDIT
ADD_PERMEA EDIT ADD_ABAG EDIT
ADD_FATIGUE EDIT ADD_GEN_DA EDIT
ADD_DAM_DI EDIT ADD_DAM_GI EDIT
PZELECTRIC EDIT ADD_INELAST EDIT

Suffixes: EN

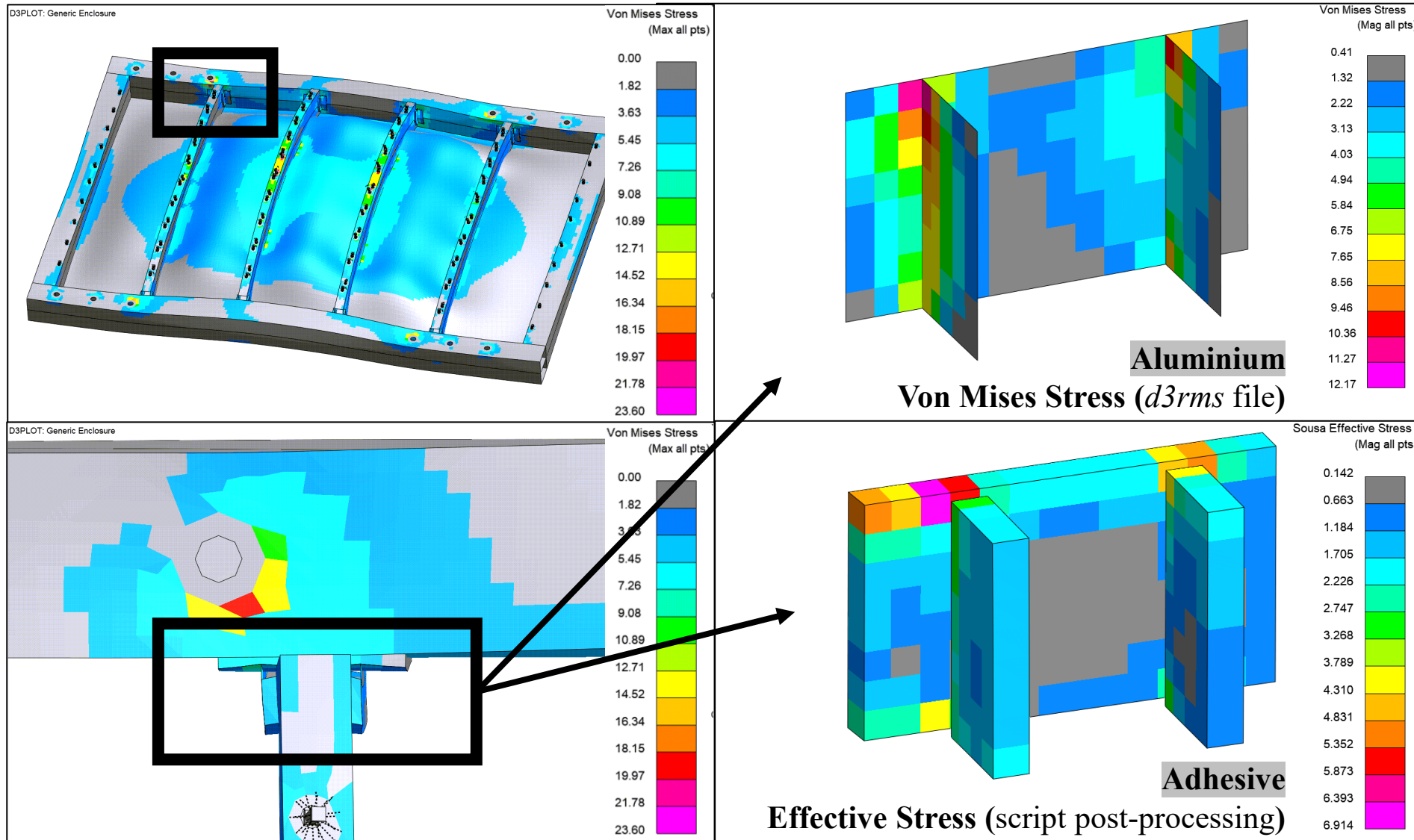
Row/Col	1	2	3	4	5	6	7	8
1	<Label>	LCID LC	LTYPE I	A F	B F	STHRES F	SNLIMIT I	SNTYPE I
	4	61	1	0.0	0.0	0.0	0	0

Fatigue assessment: considerations

- Sensitivity of fatigue damage results to inputs:
 - Modal damping – 1%, 2%, 3% – what is real/conservative?
 - Number of modes used in modal superposition – 25, 50, 100 – sufficient for a converged solution
 - Mesh resolution (number of elements), element quality – sufficient for a converged solution
 - Analysis verification with sensitivity studies is recommended
- If fatigue damage is above/below targets:
 - Local structural modifications to increase/reduce stiffness/mass
 - Resizing or redistributing the adhesive bond area
 - In combination with other load cases (also needs to meet other requirements; crash, NVH, etc...)

Now to look at some example results ...

Fatigue assessment: stress results

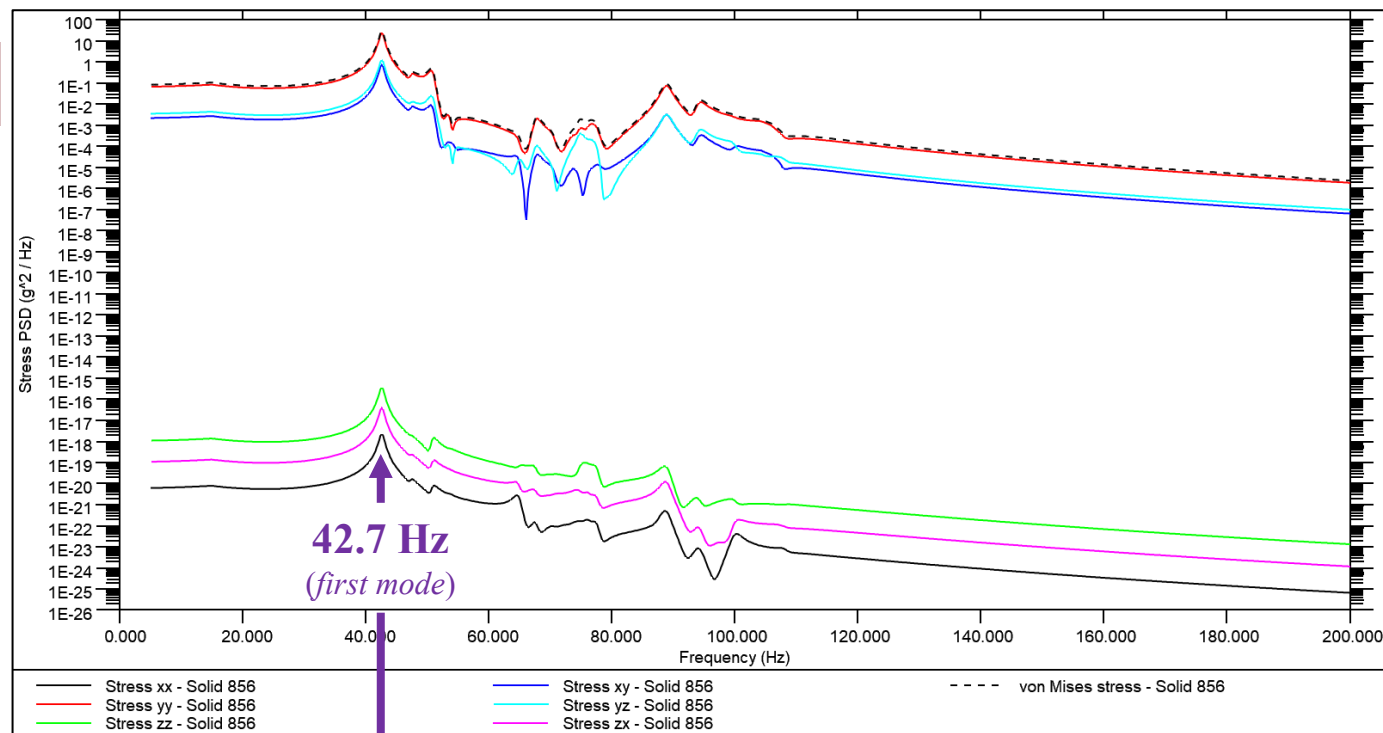


Element stresses

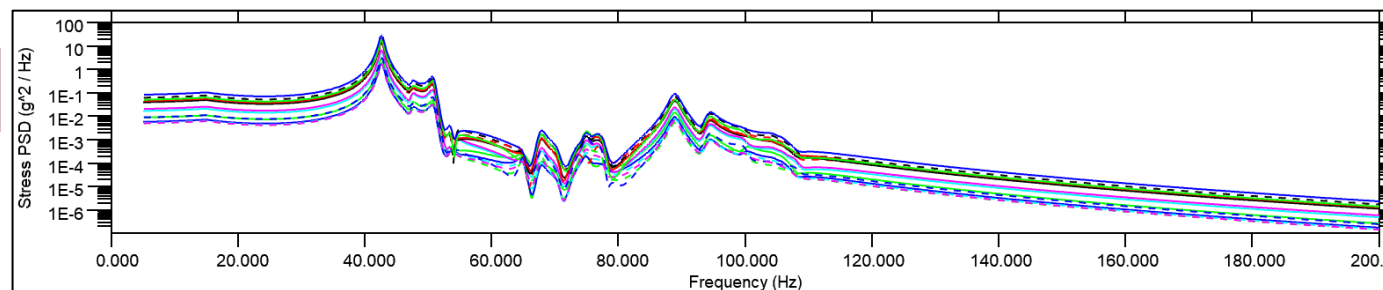
- From Z PSD random vibration
- Aluminium peak
 $3\sigma = 24 \times 3 = 72\text{MPa}$
 (compared to yield 360MPa)
- Adhesive peak
 $3\sigma = 7 \times 3 = 21\text{MPa}$
 (compared to bond shear failure 25MPa)

σ = the value at *one standard deviation* on a normal (Gaussian) distribution

Fatigue assessment: stress results



Adhesive SOLID stress PSDs

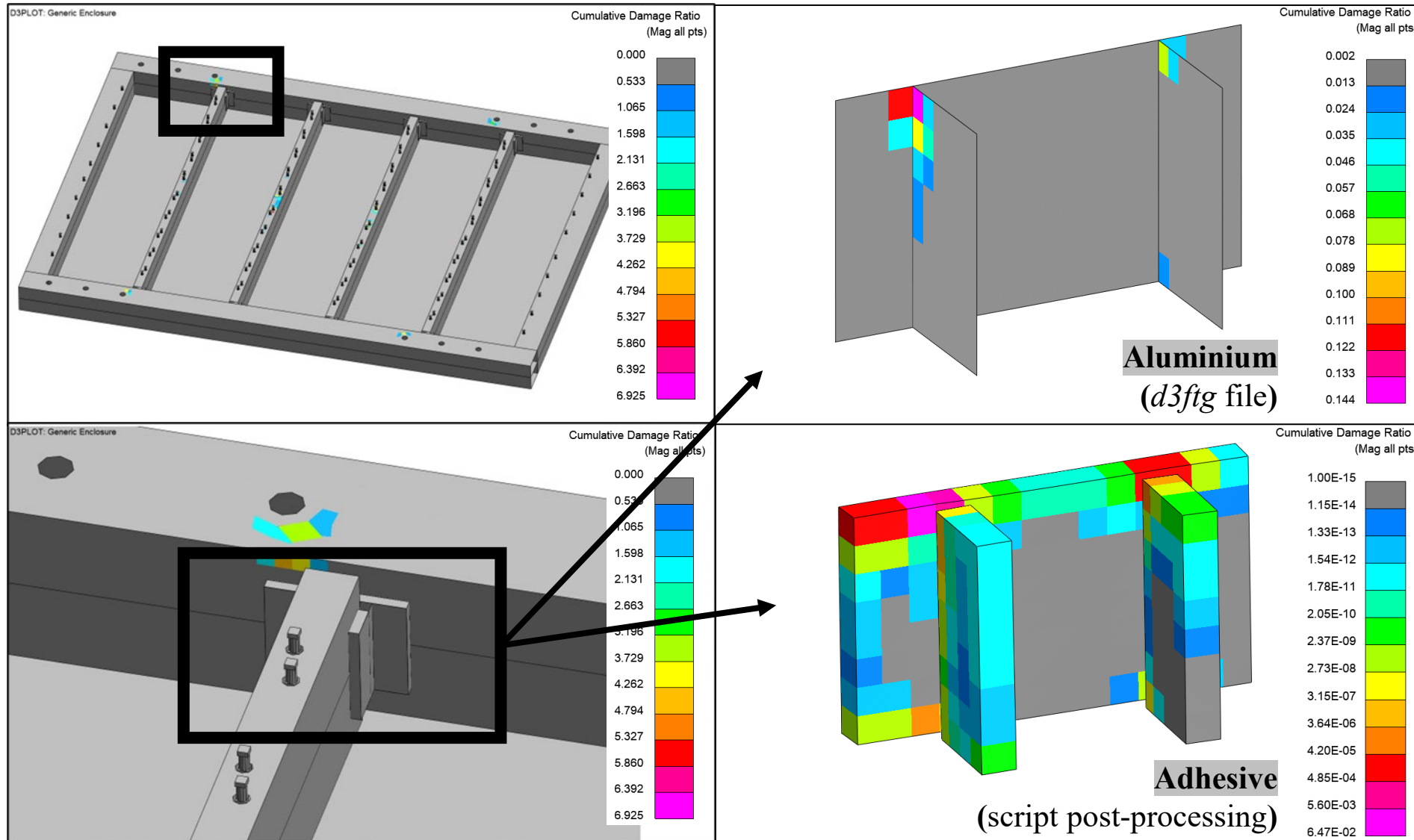


All components
SOLID 856

Von
Mises
stress

Adhesive

Fatigue assessment: damage results



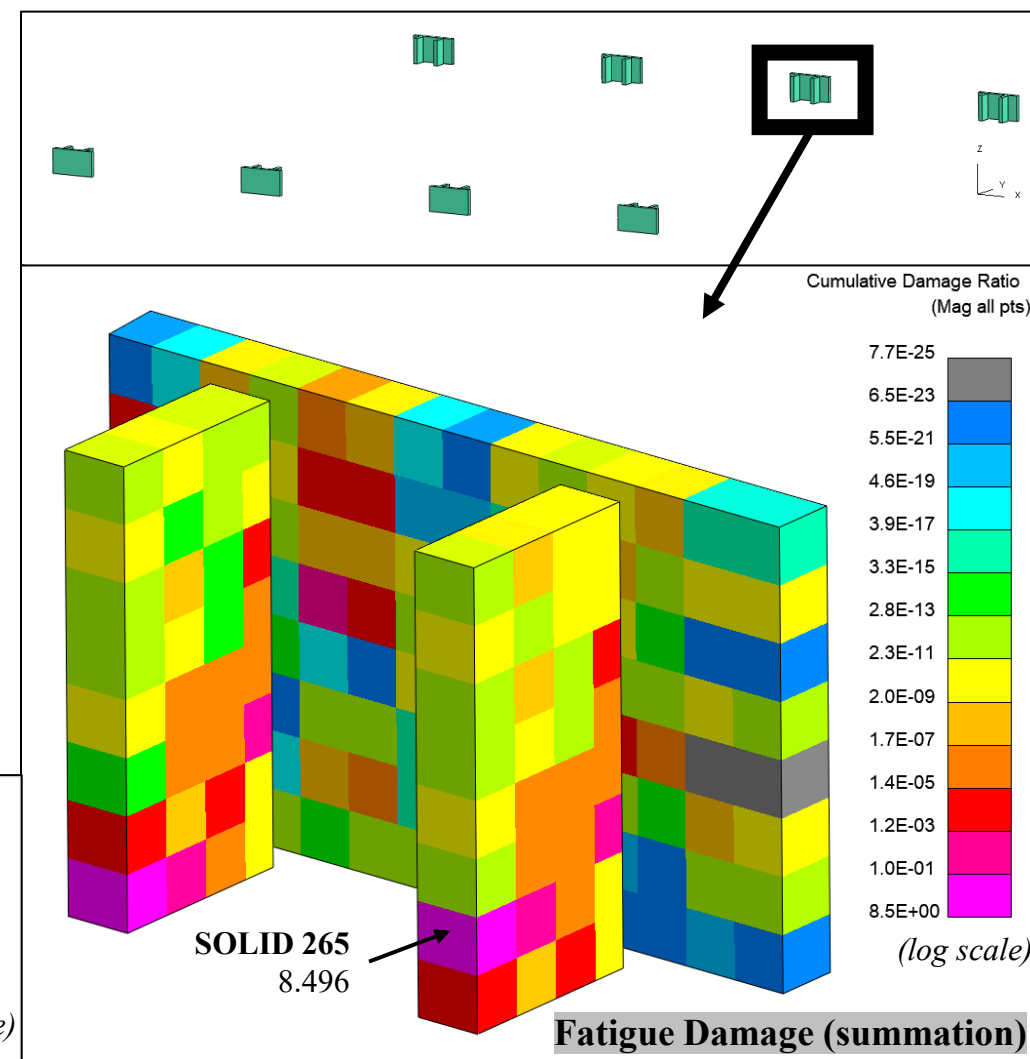
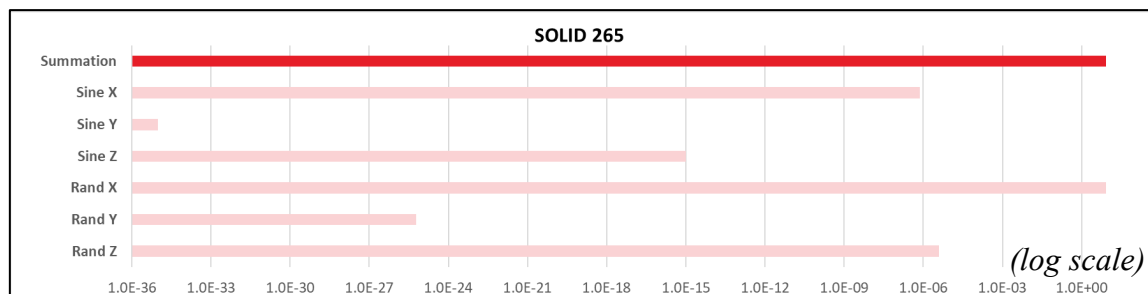
Fatigue damage

- From Z PSD random vibration
- *In this example:*
- Aluminium predicted to fail locally before the adhesive bond
- However, the joint should be safe during enclosure's operational life

Fatigue assessment: adhesive damage

- Linear summation (6 load cases)
- For example, **adhesive SOLID 265**

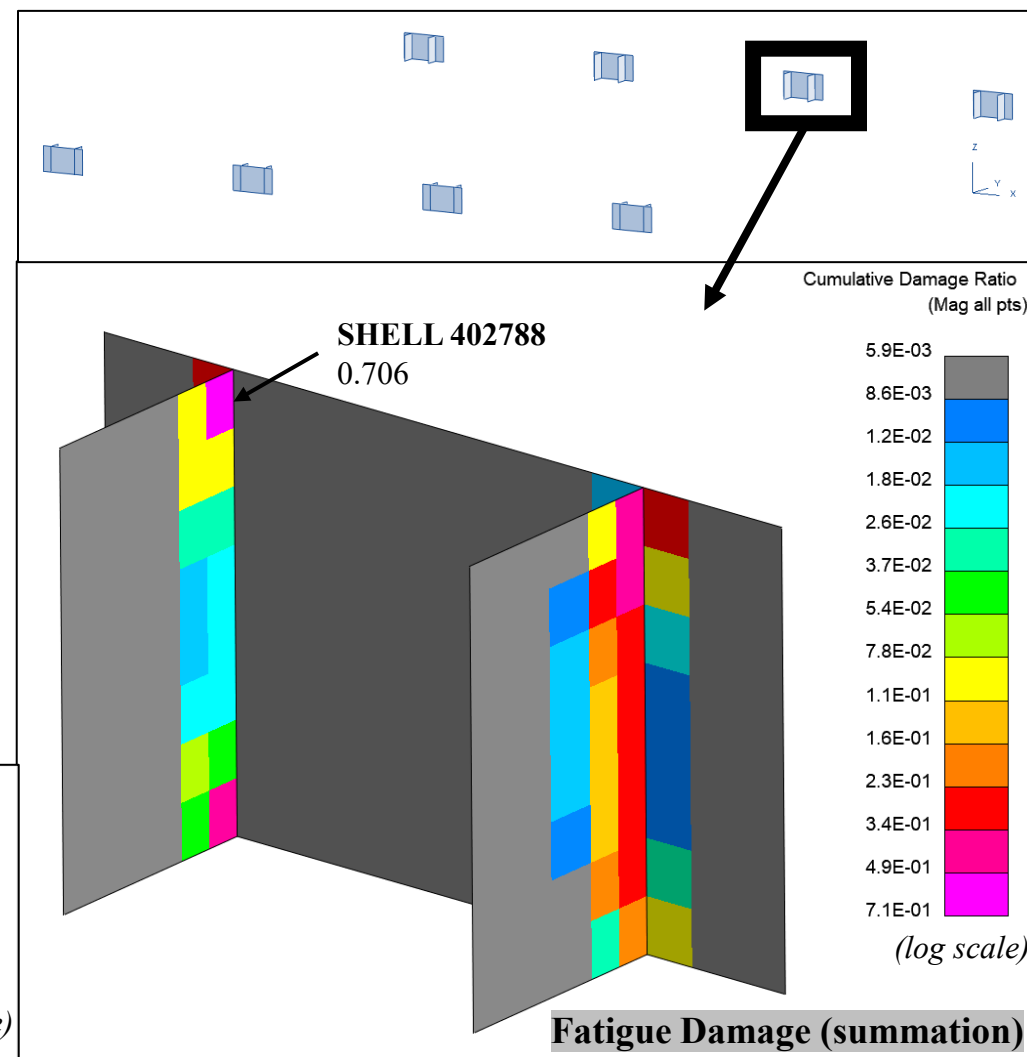
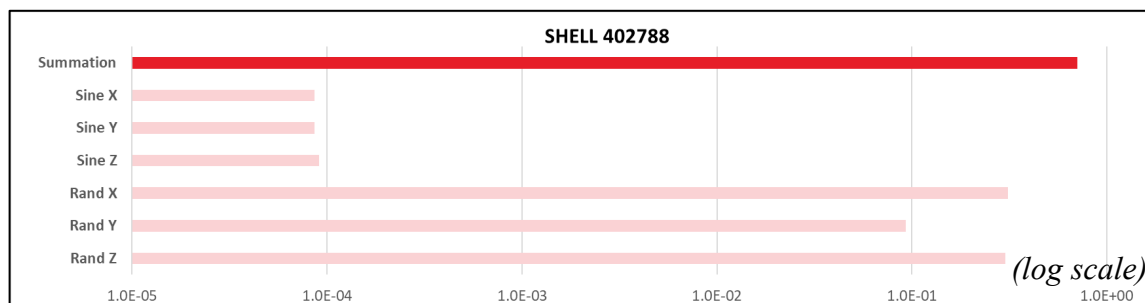
Adhesive SOLIDs					
Fixed sine wave			Random vibration		
Z	Y	X	Z PSD	Y PSD	X PSD
<i>(analysed in the frequency domain)</i> *FREQUENCY_DOMAIN _SSD_FATIGUE			<i>(analysed in the time domain)</i> *CONTROL_IMPLICIT _MODAL_DYNAMIC		
Fatigue Damage 1E-15	Fatigue Damage 1E-35	Fatigue Damage 7E-7	Fatigue Damage 4E-6	Fatigue Damage 6E-26	Fatigue Damage 8.496
Fatigue Damage (summation - SOLID 265) 8.496					



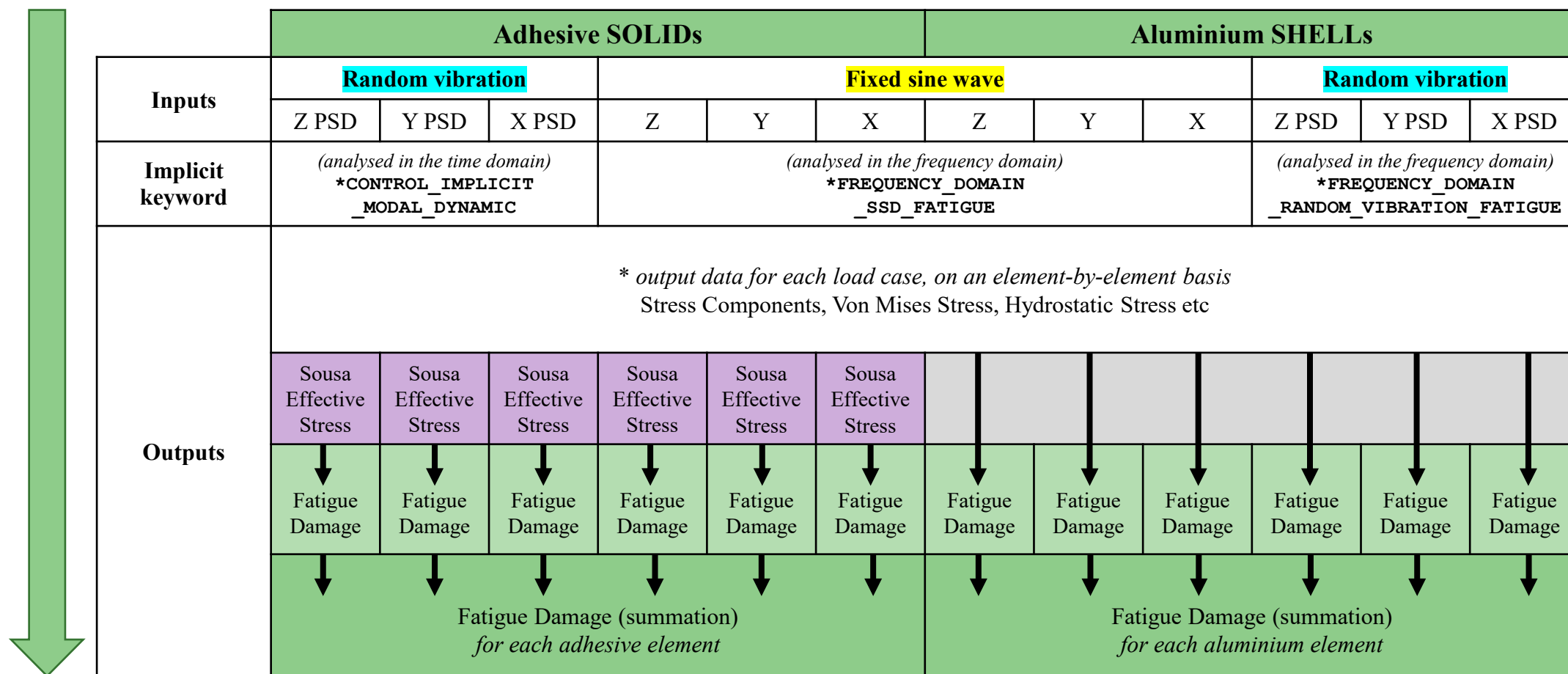
Fatigue assessment: aluminium damage

- Linear summation (6 load cases)
- For example, **aluminium** SHELL 402788

Aluminium SHELLs					
Fixed sine wave			Random vibration		
Z	Y	X	Z PSD	Y PSD	X PSD
<i>(analysed in the frequency domain)</i> *FREQUENCY_DOMAIN _SSD_FATIGUE			<i>(analysed in the frequency domain)</i> *FREQUENCY_DOMAIN _RANDOM_VIBRATION_FATIGUE		
Fatigue Damage 0.000091	Fatigue Damage 0.000086	Fatigue Damage 0.000086	Fatigue Damage 0.301019	Fatigue Damage 0.092770	Fatigue Damage 0.311591
Fatigue Damage (summation - SHELL 402788) 0.706					



Fatigue assessment: overall methodology



Benefits of LS-DYNA implicit fatigue methodology

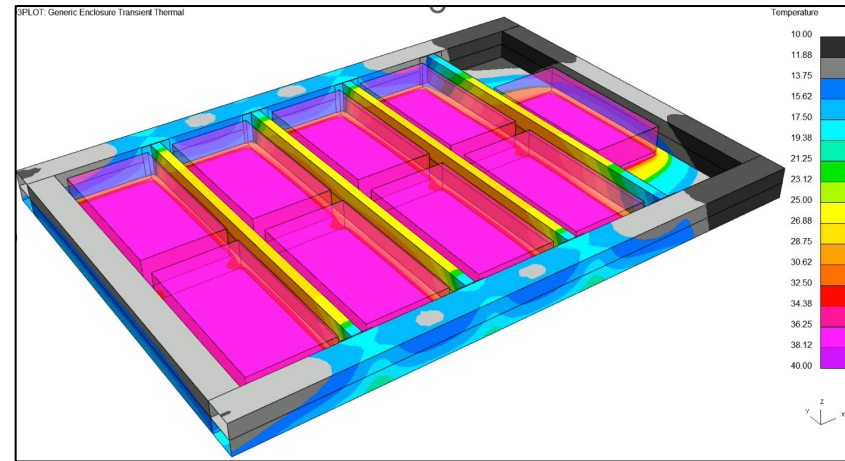
For adhesive fatigue assessment:

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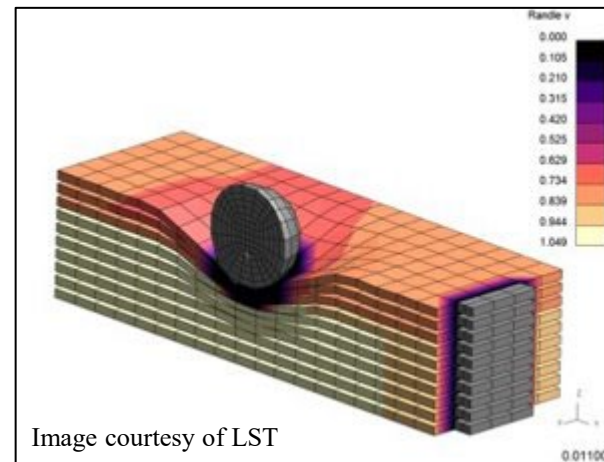
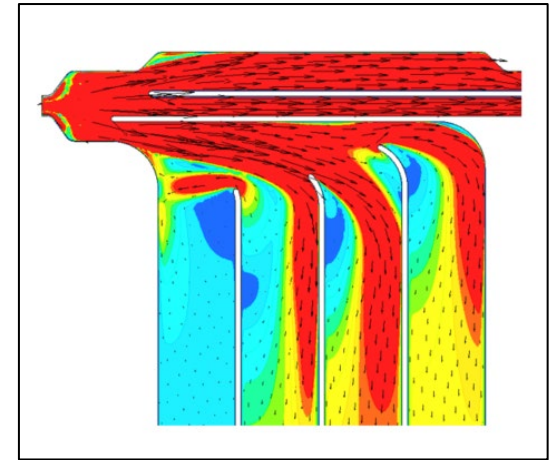
Automotive
consulting

EV battery
consulting

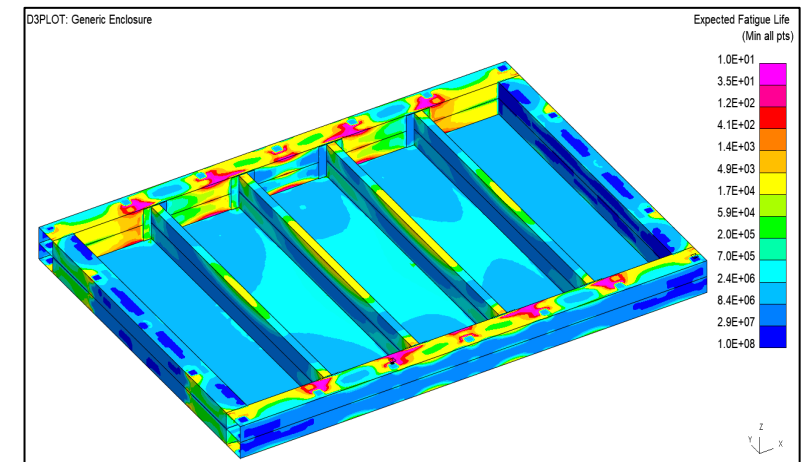
Transient thermal analysis



Coolant flow optimisation

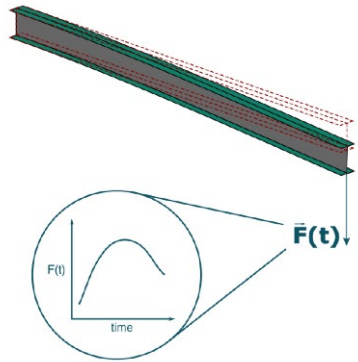
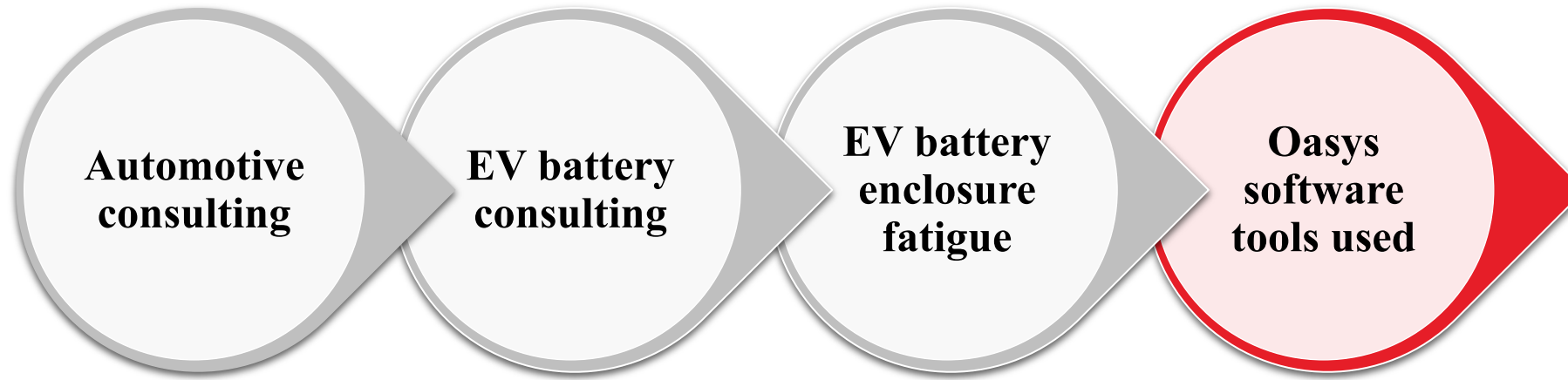


Cell penetration analysis



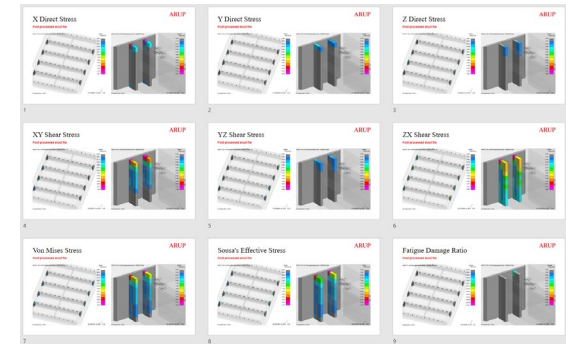
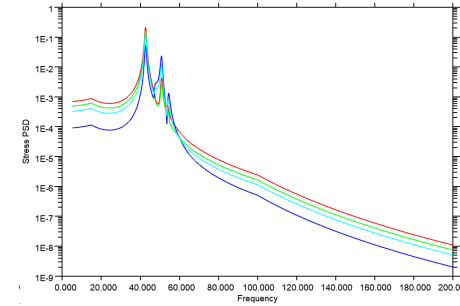
Fatigue analysis

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ID	Type	Subtype	Status	Part ID
CNX1	ADHESIVE	Patch	Realized	10
CNX2	ADHESIVE	Patch	Realized	10
CNX3	ADHESIVE	Patch	Realized	10
CNX4	ADHESIVE	Patch	Realized	10
CNX5	ADHESIVE	Patch	Realized	10
CNX6	ADHESIVE	Patch	Realized	10
CNX7	ADHESIVE	Patch	Realized	10
CNX8	ADHESIVE	Patch	Realized	10
CNX9	ADHESIVE	Patch	Realized	10
CNX10	ADHESIVE	Patch	Realized	10

☐ d3eigv
☐ d3eigv01
☐ d3eigv02
☐ d3eigv03
☐ d3eigv04
☐ d3eigv05
☐ d3eigv06
☐ d3ftg
☐ d3rms



PRIMER implicit setup tool

PRIMER connections tool

D3PLOT for d3rms, d3ftg, d3ssd

T/HIS for PSD results

REPORTER bespoke templates



Contact

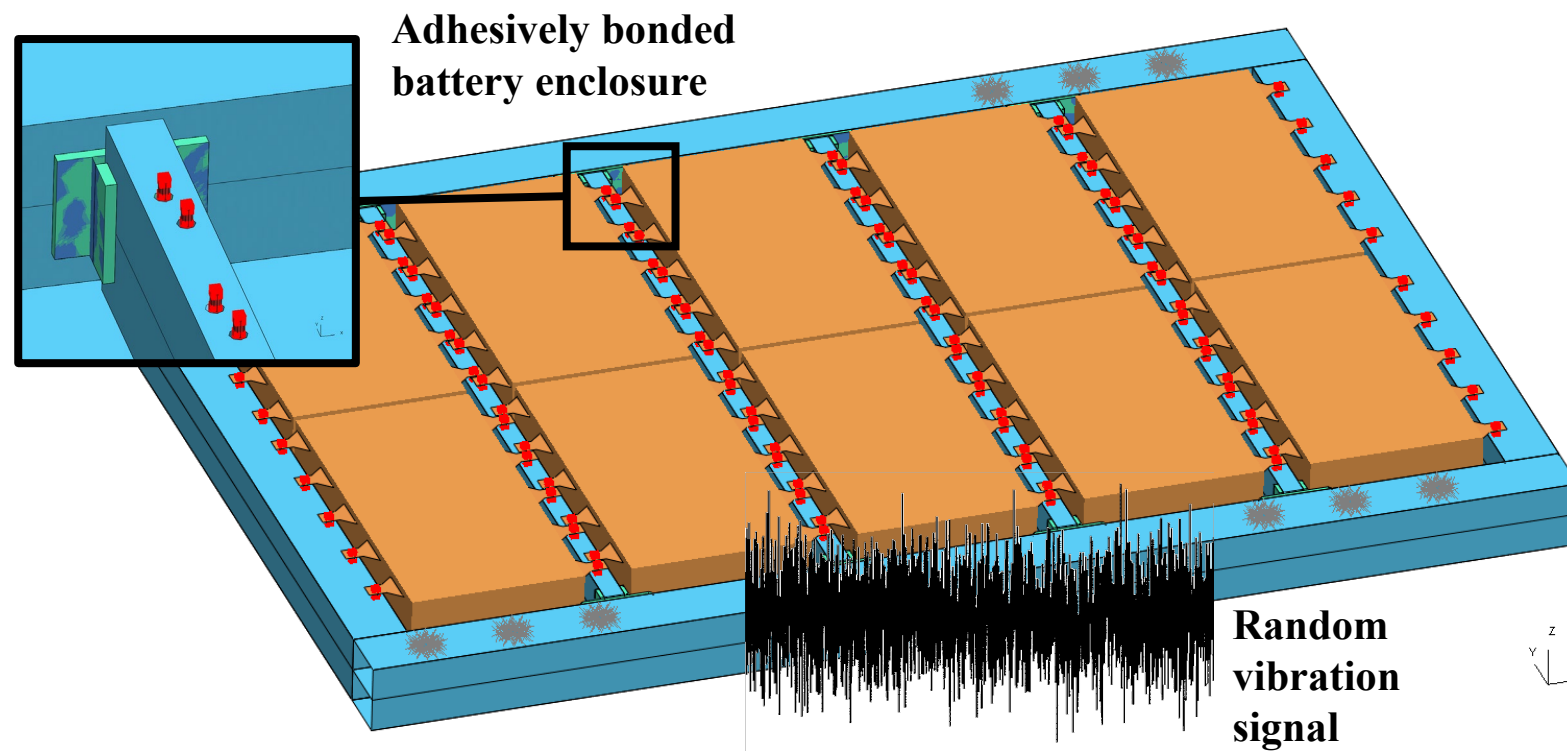
David McLennan

Engineer, Arup



Emily Owen

Senior Engineer, Arup



Thank you!