

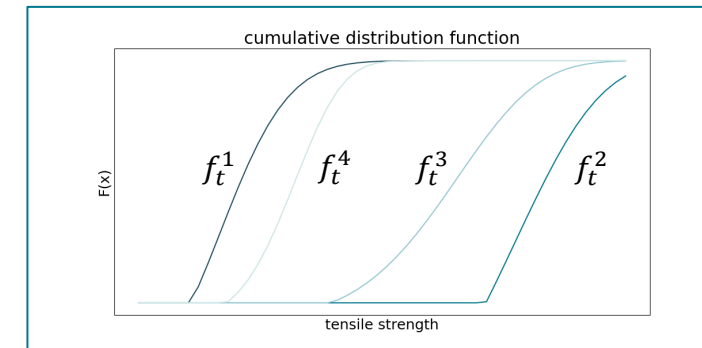
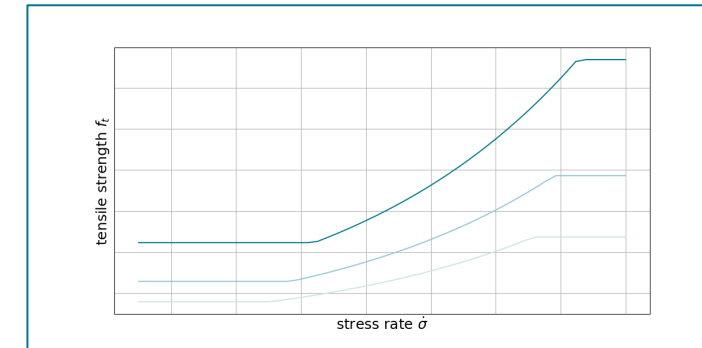
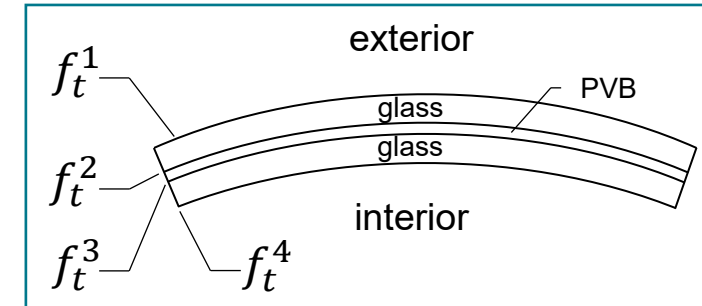
Detroit, November 16th, 2023

Status and Strategies of Glass Modelling with MAT_GLASS (MAT_280)

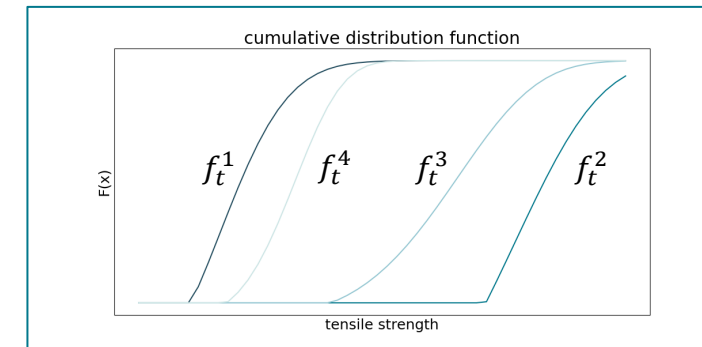
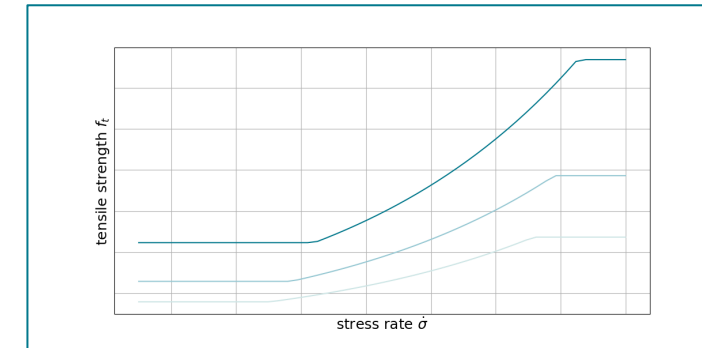
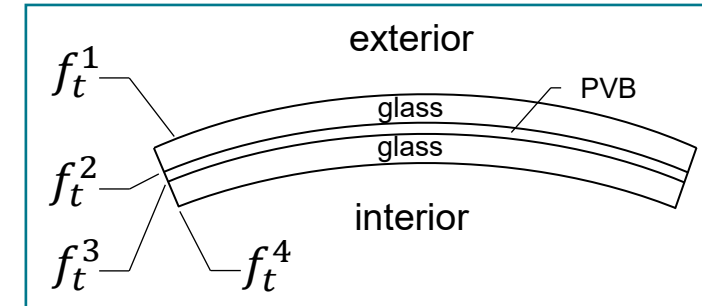
Christoph Wilking, Tobias Graf & André Haufe, DYNAmore GmbH, an Ansys company
Markus Feucht, Mercedes-Benz AG

Motivation

- Keynote given by Stefan Kolling at LS-Dyna Forum 2022 in Bamberg “Notes on Simulating Head Impact on Windshields”
 - Glass material model (user material) which allows for
 - different strengths over thickness
 - strength reduction near cracked elements
 - rate dependent tensile strengths
 - stochastic variation of strengths
 - ...
- This presentation
 - How to use *MAT_GLASS/*MAT_280 to get similar features as the user material described by Stefan Kolling



- Motivation
- Introduction to MAT_GLASS
- A Model for Laminated Glass
- MAT_GLASS Features
 - Strength Reduction
 - Strain Rate Dependency
 - Stochastic Variation
 - Position-Based Tensile Strength
- Application
- Summary

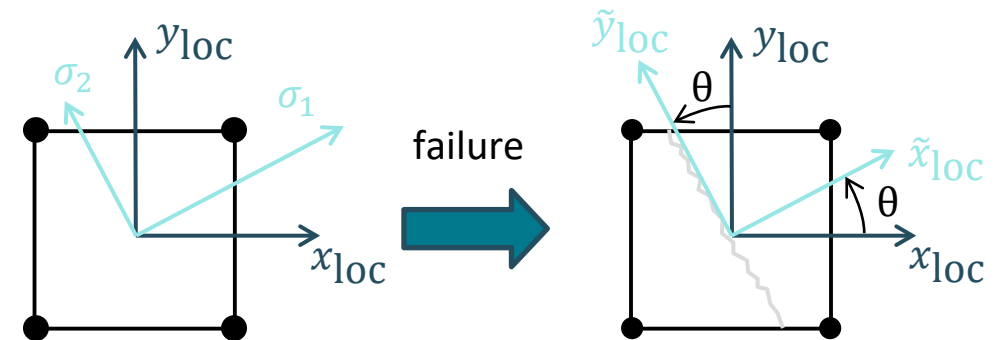
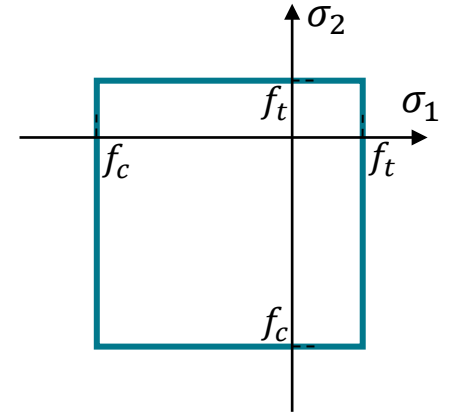


Introduction to MAT_GLASS

Introduction to MAT_GLASS

Theoretical Background

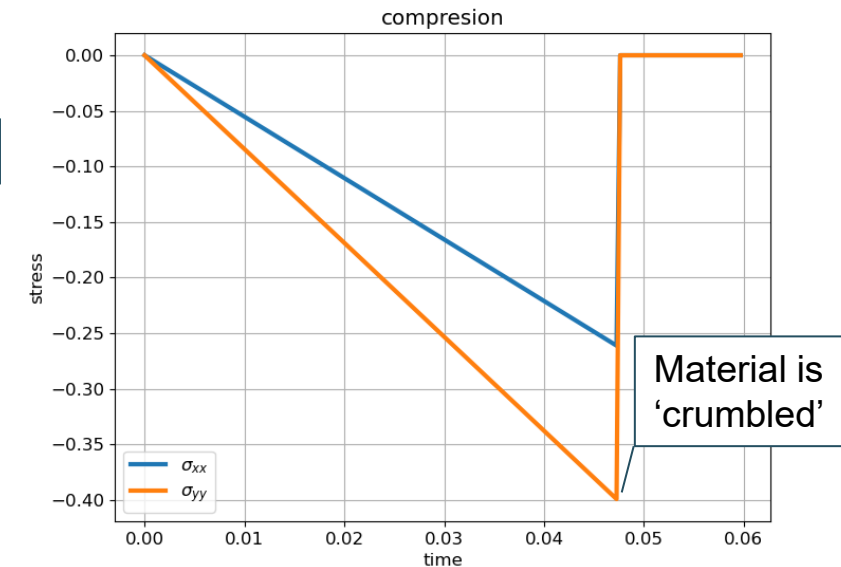
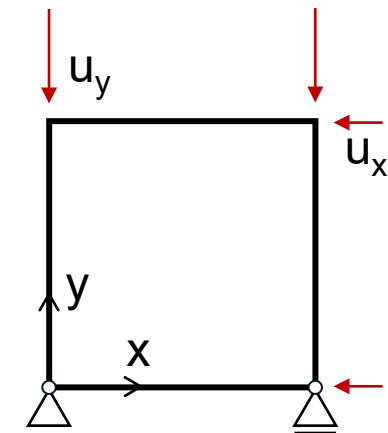
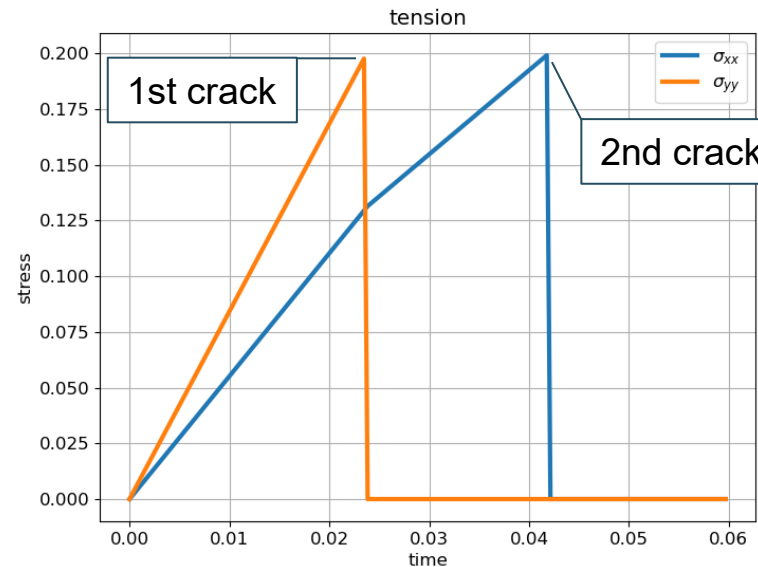
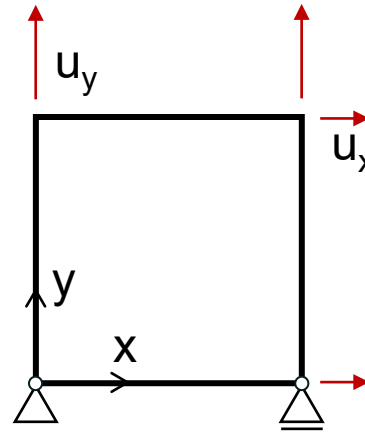
- Linear elastic until failure
- Stress based failure criteria: **Rankine**, Mohr-Coulomb, Drucker-Prager
- Compressive failure
 - Material is 'crumbled'
- Tensile failure
 - Single Cracks
 - Crack direction perpendicular to the 1st principal stress
 - Local crack coordinate systems
 - 2nd crack can occur orthogonal to the 1st crack
 - Cracks can open and close independently



Introduction to MAT_GLASS

Single element test

- Material properties
 - Tensile strength $f_t = 0.2$
 - Compressive strength $f_c = 0.4$



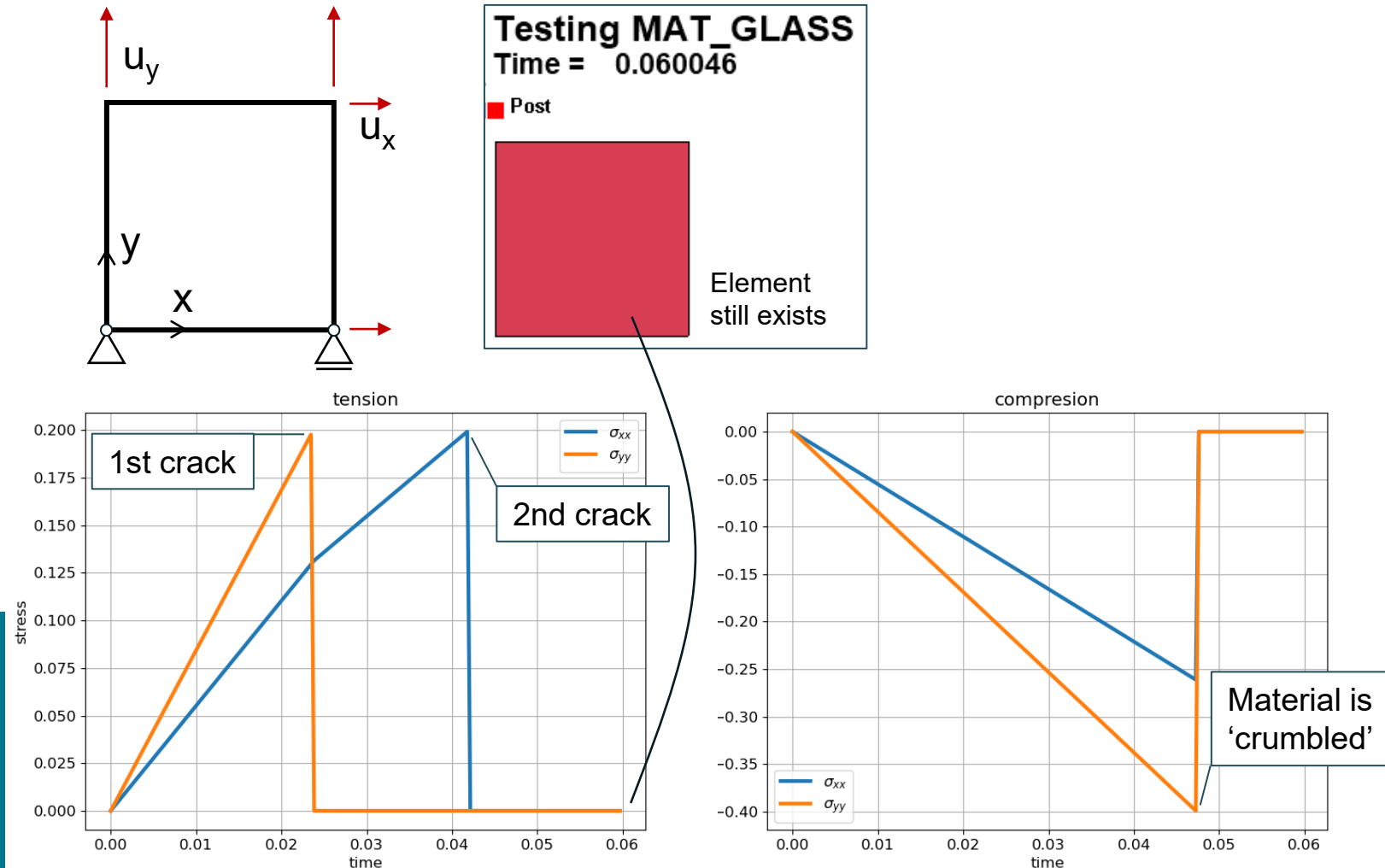
Introduction to MAT_GLASS

Element deletion

- Material properties
 - Tensile strength $f_t = 0.2$
 - Compressive strength $f_c = 0.4$
- MAT_GLASS elements will not be deleted when f_t or f_c is reached
- To avoid highly distorted elements use
 - EPSCR (MAT_GLASS)
 - MAT_ADD_EROSION

HINT

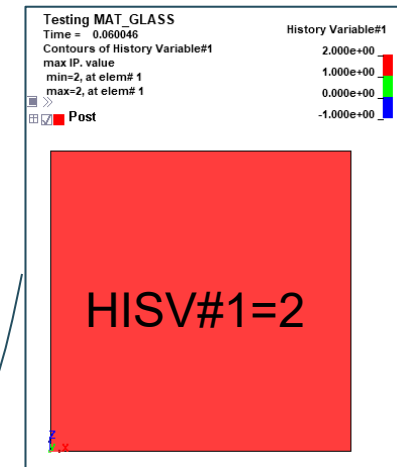
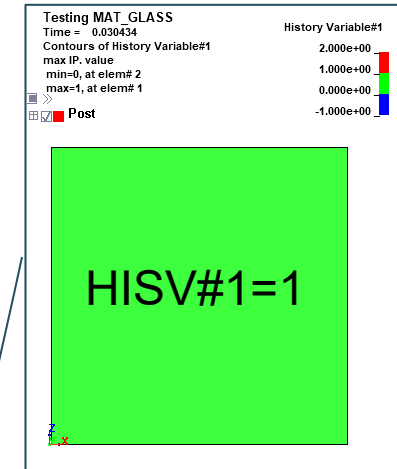
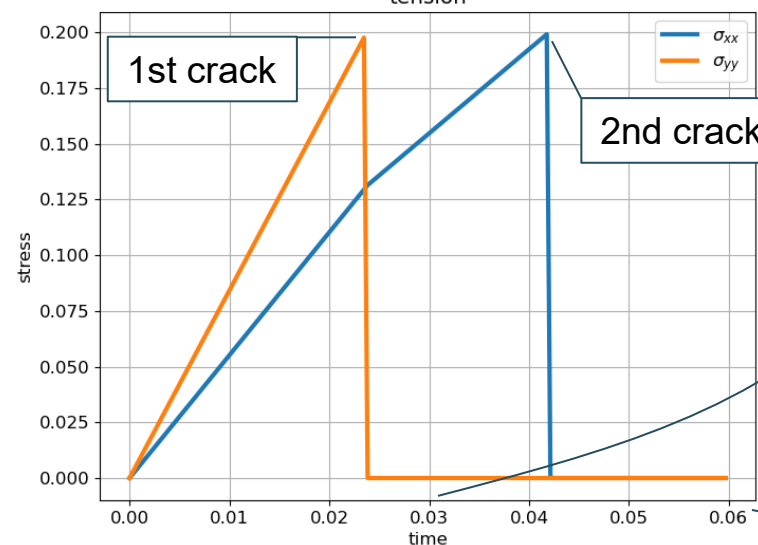
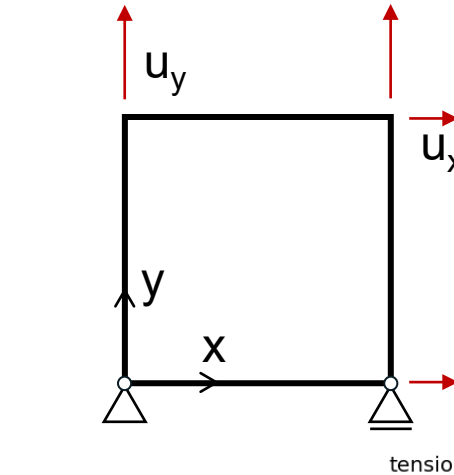
Make sure the element erosion criterion is not taking effect prior to tensile or compressive strength



Introduction to MAT_GLASS

Crack visualization – Option I

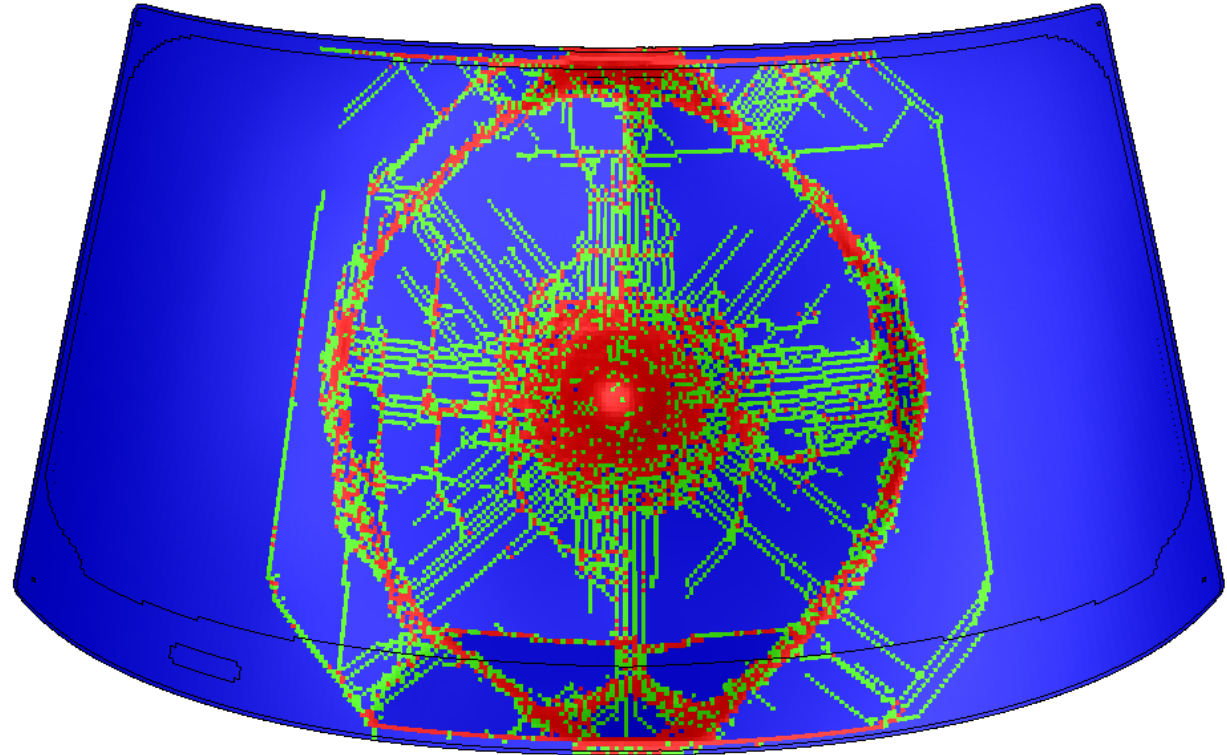
- Material properties
 - Tensile strength $f_t = 0.2$
 - Compressive strength $f_c = 0.4$
- Cracks can be visualized by history variable #1 of MAT_GLASS
 - -1: compressive failure
 - 0: no failure
 - 1: one crack
 - 2: two cracks



Introduction to MAT_GLASS

Crack visualization – Option I

- Head impact on windshield
- Cracks can be visualized by history variable #1 of MAT_GLASS
 - -1: compressive failure
 - 0: no failure
 - 1: one crack
 - 2: two cracks



Introduction to MAT_GLASS

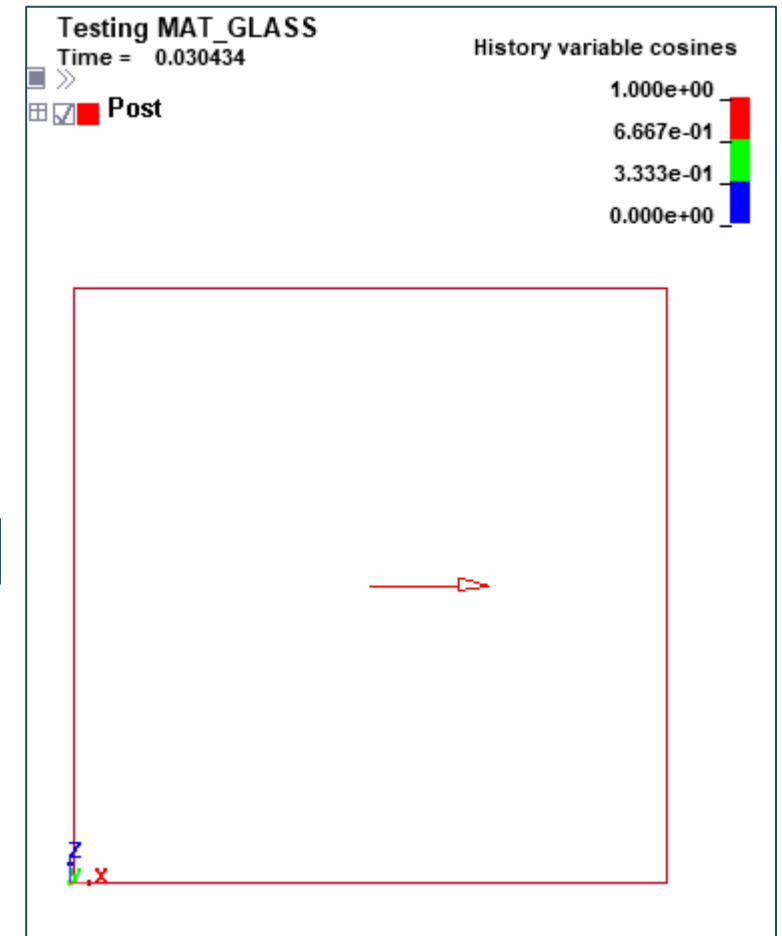
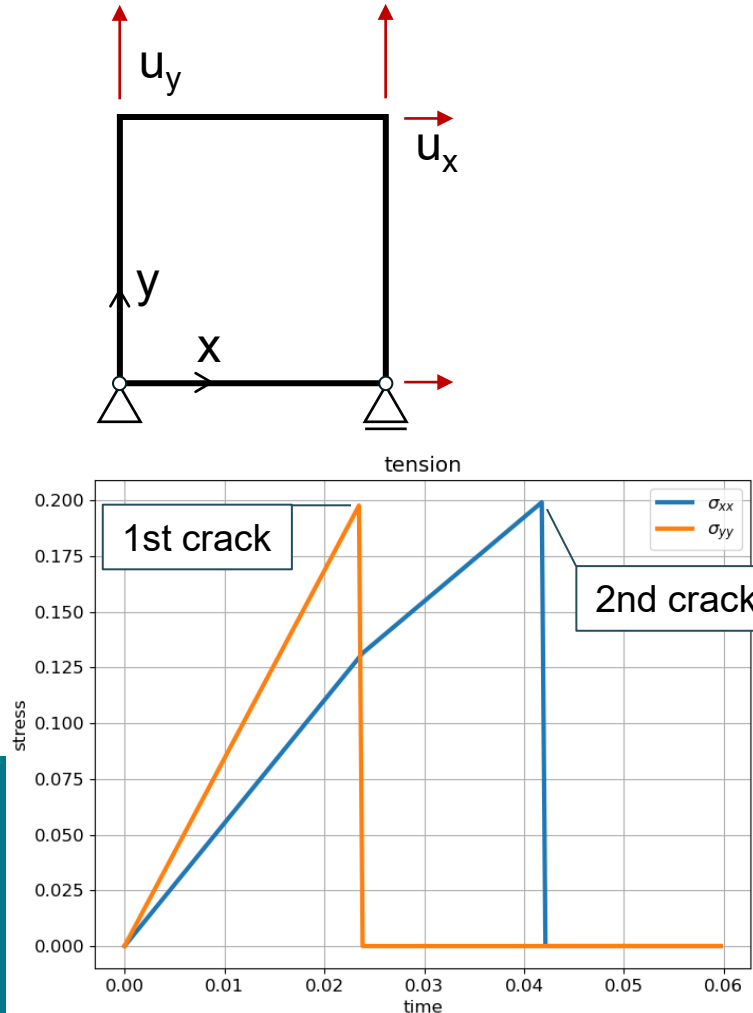
Crack visualization – Option II

- Material properties
 - Tensile strength $f_t = 0.2$
 - Compressive strength $f_c = 0.4$
- Cracks can be visualized as a vector plot using history variables #15, #16, and #17
 - Crack direction is shown
 - So far only shows 1st crack
 - So far only available in current DEV versions (→ R15)

IMPORTANT

NIPS ≥ 17 in

*DATABASE_EXTENT_BINARY



Introduction to MAT_GLASS

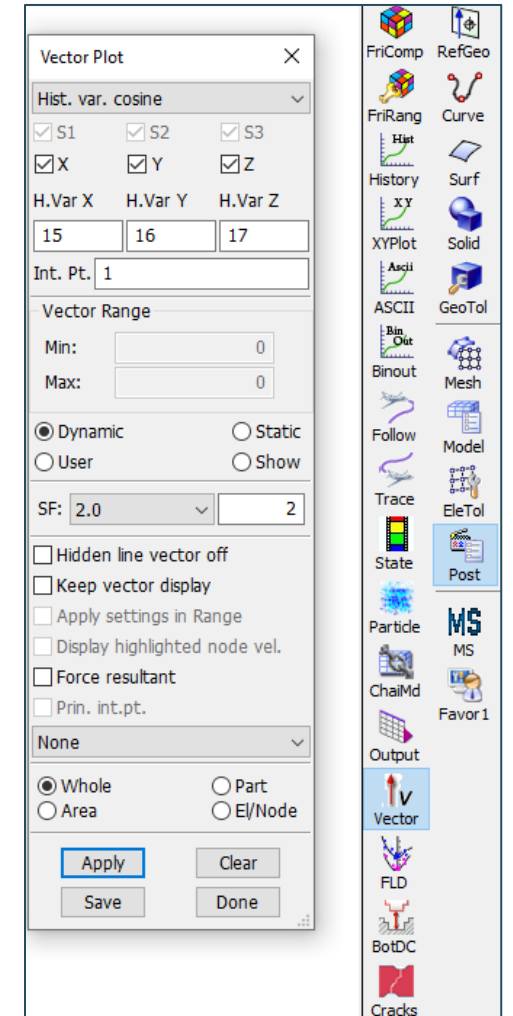
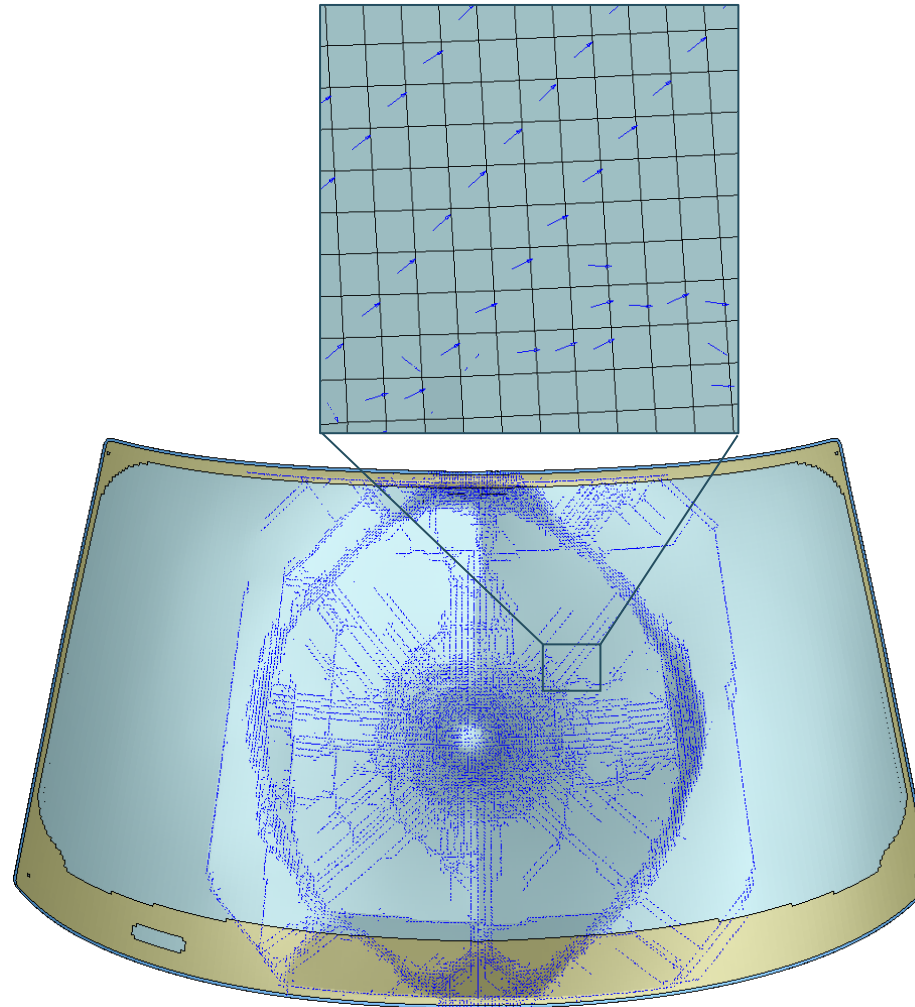
Crack visualization – Option II

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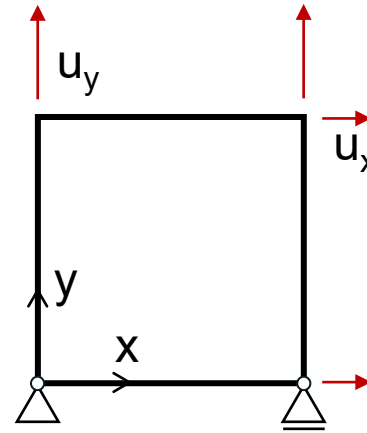
*DATABASE_EXTENT_BINARY



Introduction to MAT_GLASS

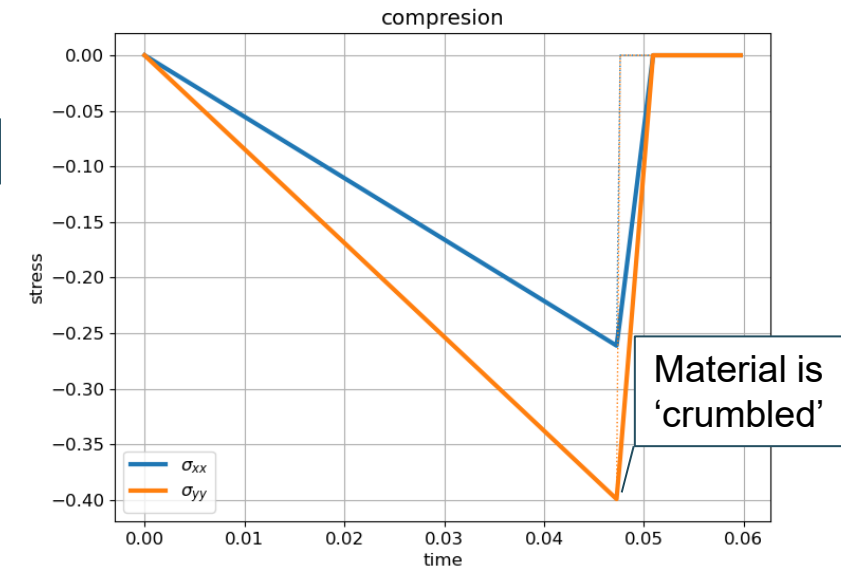
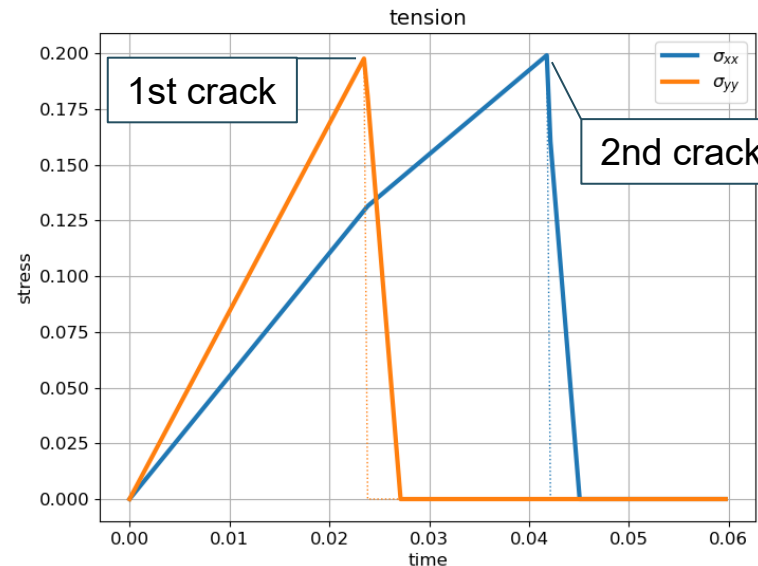
Softening/damage

- Material properties
 - Tensile strength $f_t = 0.2$
 - Compressive strength $f_c = 0.4$
- Without modifications after cracking the stress is relieved to zero within one cycle
- The post-cracking behavior can be controlled by the following variables
 - NCYCR, FRACEN, SFSTI, SFSTR, IMOD (AT, BT, AC, BC)

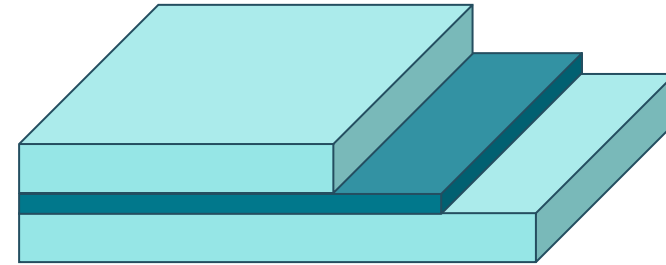
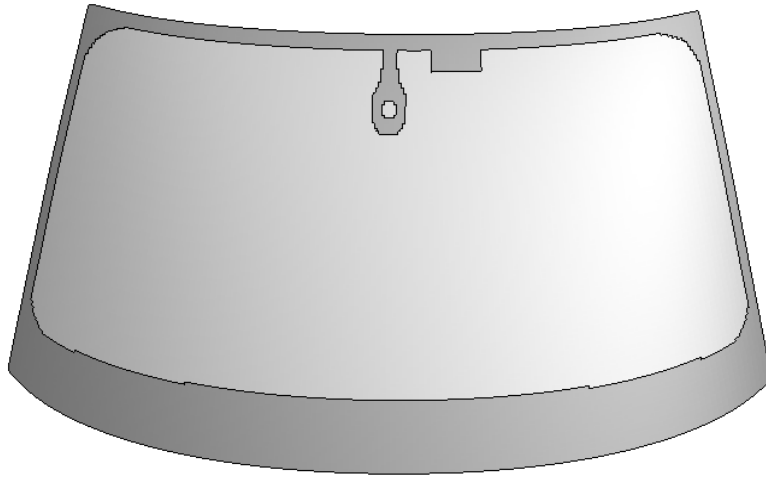


■ Example

- NCYCR = 10
- Stress is relieved within 10 cycles



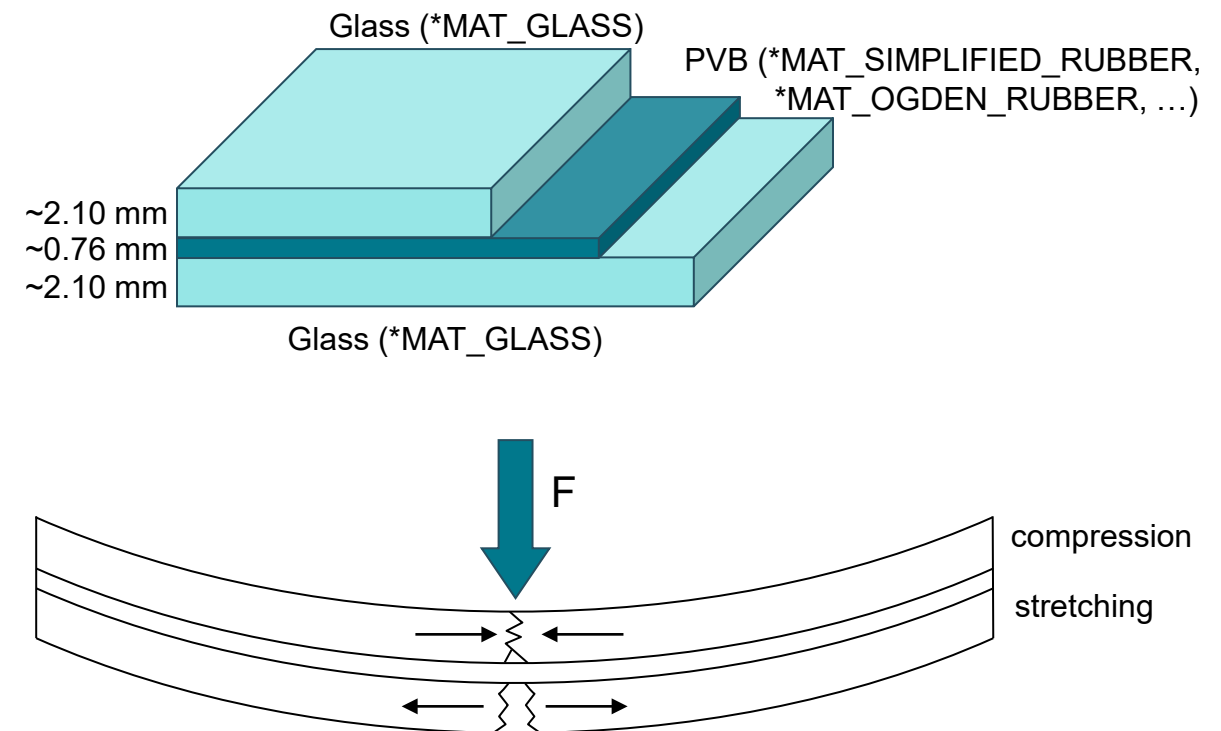
A Model for Laminated Glass



A Model for Laminated Glass

Overview

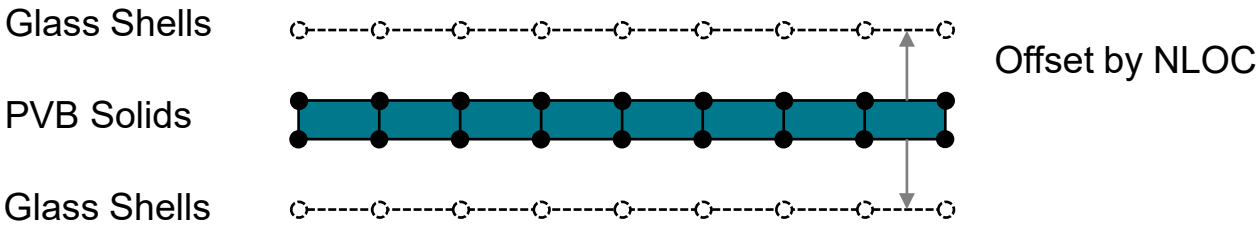
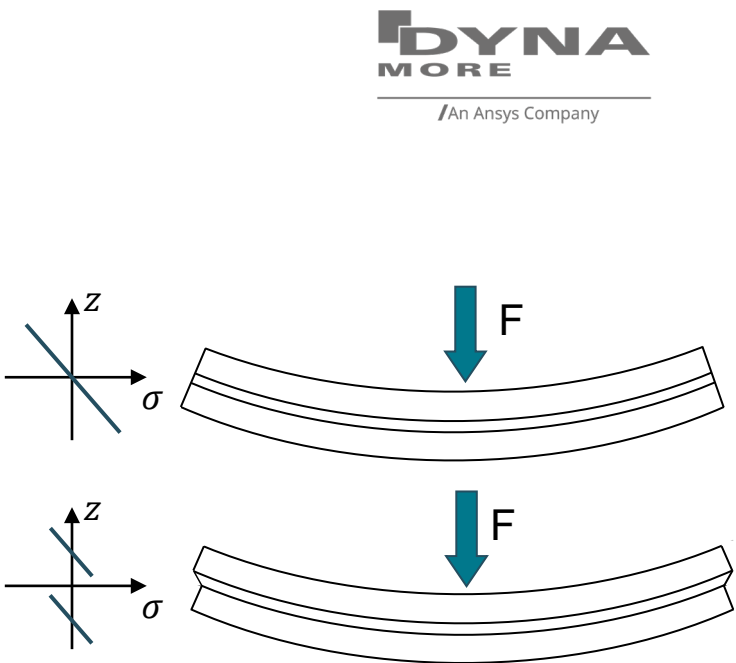
- Laminated glass consists of at least 3 layers
 - 2 glass panes
 - PVB interlayer
- Glass fragments are bonded
 - Difficult mechanical behavior



A Model for Laminated Glass

Discretization

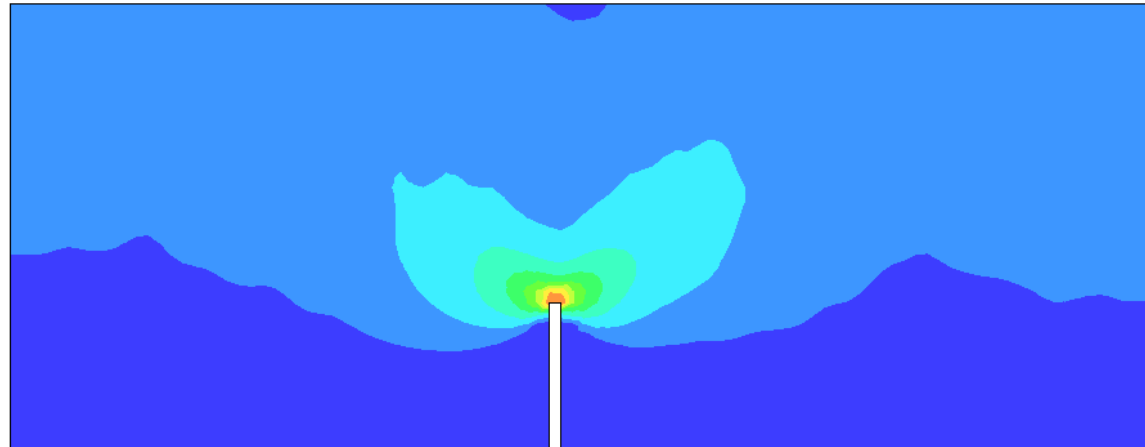
- Elements
 - PVB: transverse shear deformation important
→ **solid elements**
 - Glass: shell elements
- Contact between layers: Shared nodes
- Offset the glass layers by NLOC parameter (SECTION_SHELL)



*SECTION_SHELL								
\$	SECID	ELFORM	SHRF	NIP	PROPT	QR/IRID	ICOMP	SETYP
	100	2	0.833	5	1.0	0	0	0
\$	T1	T2	T3	T4	NLOC	MAREA		
	2.1	2.1	2.1	2.1	-1			

MAT_GLASS Features

Strength Reduction



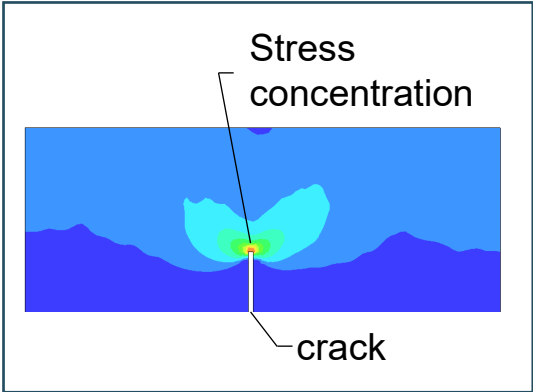
Strength Reduction

General Remarks

- Stress concentration in tip of crack
 - Cannot be resolved by coarse FE-mesh
 - To consider this effect in MAT_280 the tensile strength can be reduced after the first crack
- Variables affecting strength reduction

*MAT_GLASS_{STOCHASTIC}									
\$	MID	RO	E	PR			IMOD	ILAW	
	1	2.5E-6	70	0.23					
\$	FMOD	FT	FC	AT	BT	AC	BC	FTSCL	
		0.2						1	
\$	SFSTI	SFSTR	CRIN	ECRCL	NCYCR	NIPF			
\$	EPSCR	ENGCR	RADCRT	RATENL	RFILTF	FRACEN			

- Combination of variables determines the way the strength reduction works



Strength Reduction

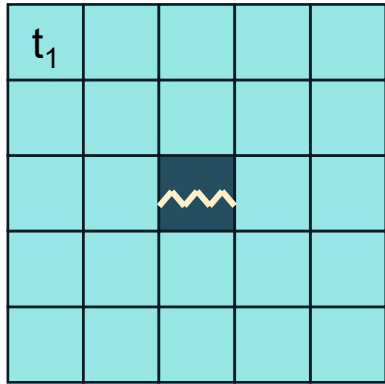
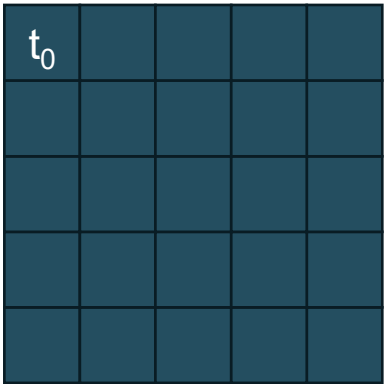
Type 1

- FT and FTSCL are defined

```
*MAT_GLASS
...
$      FMOD      FT      FC      AT      BT      AC      BC      FTSCL
      0.2      1.5
```

- Initially all elements have the tensile strength
- After the first crack **all elements of the part** get the tensile strength FT

$$FT_{mod} = FTSCL \times FT$$



Tensile strength



Strength Reduction

Type II

- FT, FTSCCL and RATENL are defined

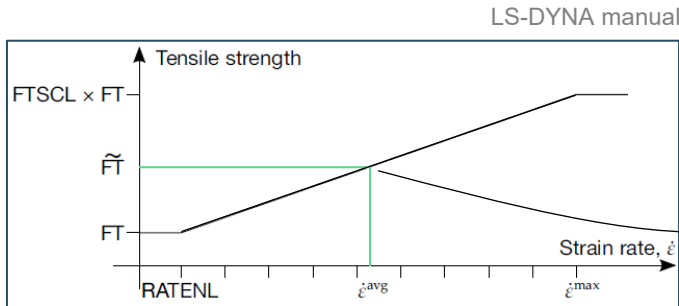
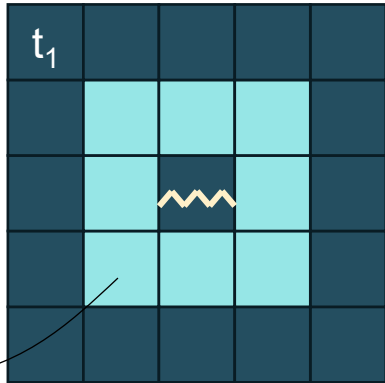
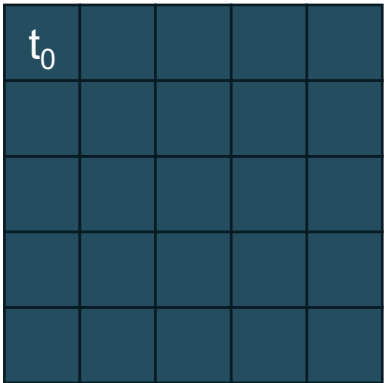
```
*MAT_GLASS
...
$      FMOD      FT      FC      AT      BT      AC      BC      FTSCCL
           0.2
...
$      EPSCR      ENGCRT      RADCRT      RATENL      RFLTF      FRACEN
           1.5      0.95
```

- Initially all elements have the tensile strength

$$F_{T_{mod}} = FTSCCL \times FT$$

- After a crack, all **elements adjacent to cracked elements** get a tensile strength \widetilde{FT} depending on their current strain rate

- The strain rate should be filtered by RFLTF



$$\dot{\epsilon}_{max} = 10^9 \times RATENL$$

Tensile strength



Strength Reduction

Type II

- FT, FTSCL and RATENL are defined

```
*MAT_GLASS
...
$      FMOD      FT      FC      AT      BT      AC      BC      FTSCL
           0.2
...
$      EPSCR      ENGCRT      RADCRT      RATENL      RFILTF      FRACEN
           1.5      0.95
```

HINT

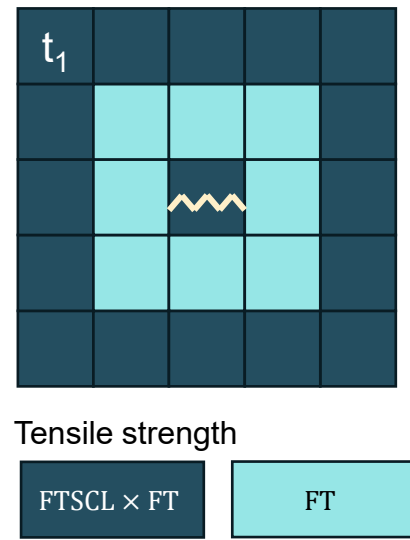
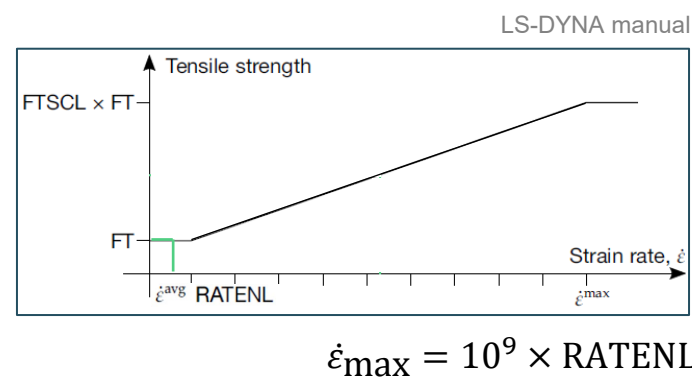
Setting RATENL to a high value e.g., 1E9 practically removes the rate dependency: $\widetilde{FT} = FT$

- Initially all elements have the tensile strength

$$FT_{mod} = FTSCL \times FT$$

- After a crack, all **elements adjacent to cracked elements** get a tensile strength \widetilde{FT} depending on their current strain rate

- The strain rate should be filtered by RFILTF

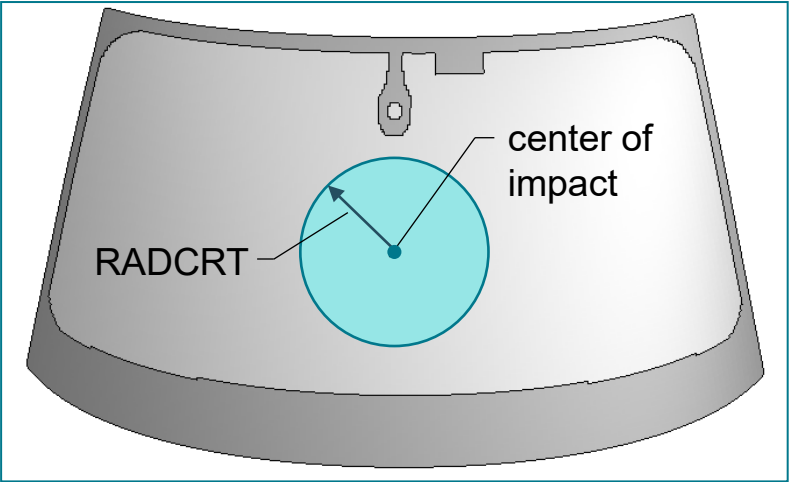


Strength Reduction

Delayed Crack Initiation

- ENGCR and RADCRT are defined

*MAT_GLASS									
\$	MID	RO	E	PR			IMOD	ILAW	
	1	2.5E-6	70	0.23					
\$	FMOD	FT	FC	AT	BT	AC	BC	FTSCL	
		0.2						1	
\$	SFSTI	SFSTR	CRIN	ECRCL	NCYCR	NIPF			
\$	EPSCR	ENGCR	RADCRT	RATENL	RFILTF	FRACEN			



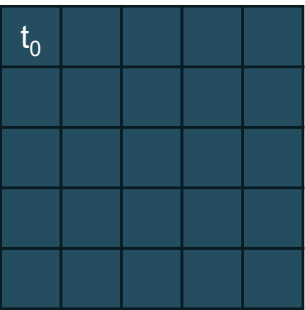
- Activates a failure model described by Pytell/Liebertz (2011)
- Initially deactivates failure/cracks
- 1st element with $\sigma_1 > FT \times FTSCL$ defines center of impact
- Internal energy of part within radius RADCRT is monitored
- When internal energy reaches ENGCR failure as activated
- Strength reduction according to type I or II depending on the variables defined

Strength Reduction

Overview

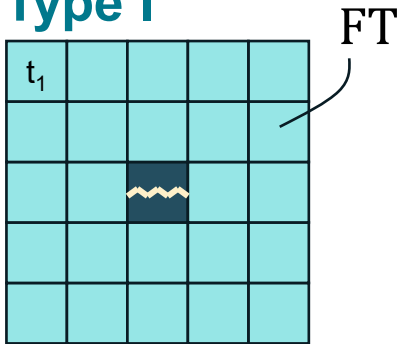
Initial state

$$FT_{mod} = FT_{SCL} \times FT$$



RATENL = 0

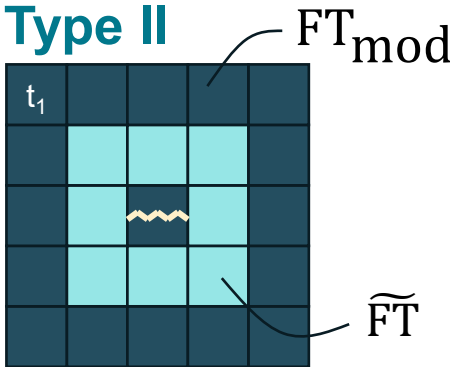
Type I



- After the first crack the tensile strength **in the entire part** is reduced to FT

RATENL \neq 0

Type II

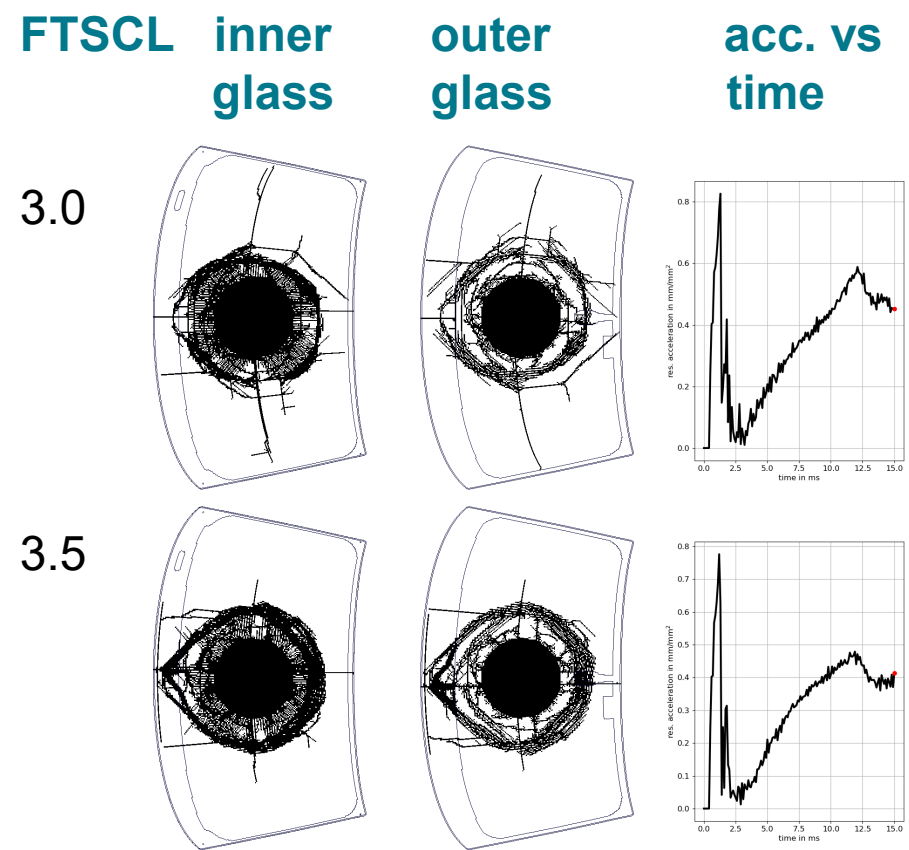
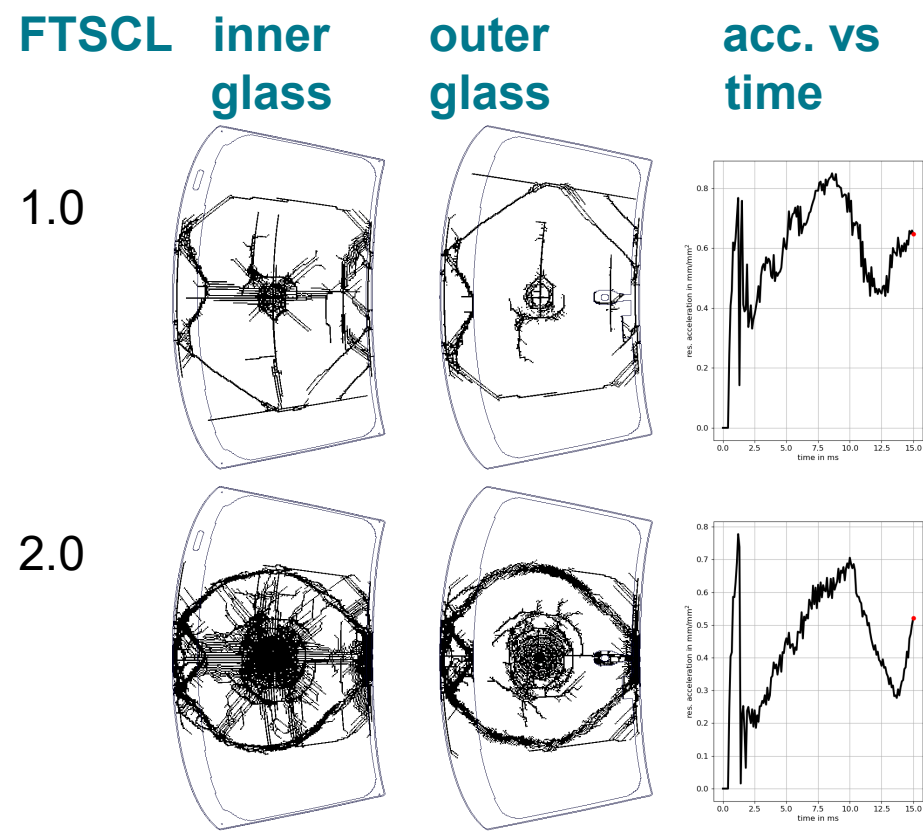


- After a crack, all **elements adjacent to cracked elements** get the tensile strength \widetilde{FT}

Strength Reduction

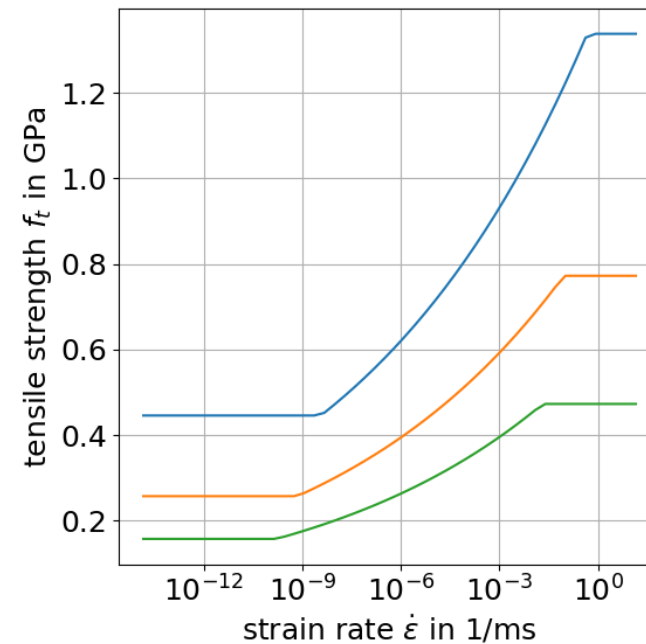
Parameter Study

- Head impact on windshield
- Type II – FT, FTSCL and RATENL are defined → strength reduction in adjacent elements



MAT_GLASS Features

Strain Rate Dependency



Strain Rate Dependency

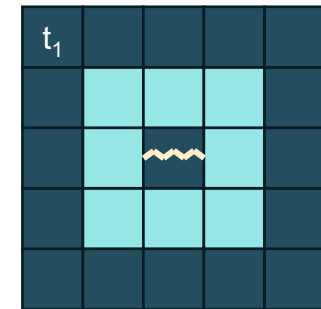
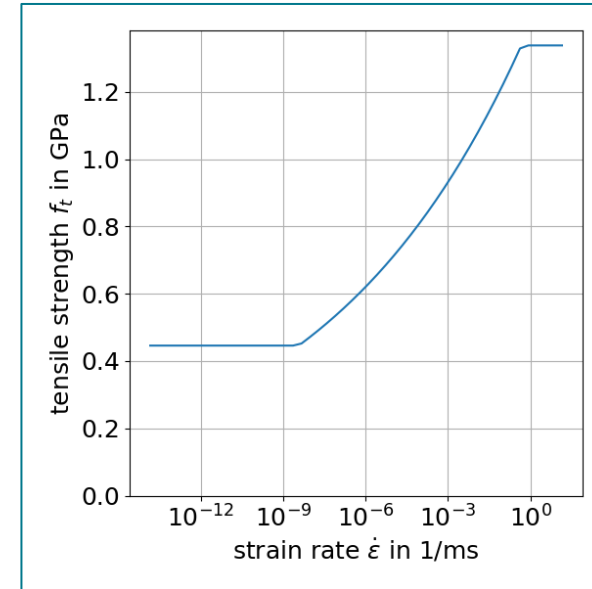
General Remarks

- Strain rate dependent tensile strength from literature, e.g.,

$$f_t = \left(\frac{2(n+1)K_{Ic}^n}{v_0(n-1)(Y\sqrt{\pi})^n a_i^{\frac{n-1}{2}}} \right)^{1/(1+n)} \dot{\sigma}^{1/(1+n)}$$

Alter, Kolling, Schneider 2017

- To be flexible LS-DYNA allows to define FT as a curve
 - Abscissa: strain rate $\dot{\varepsilon} = |d\varepsilon_1|/\Delta t$
with $d\varepsilon_1$: increment of 1st principal strain
 - If first value is negative, LS-DYNA expects logarithmic values $\ln(\dot{\varepsilon})$
 - Use $\ln(\dot{\varepsilon})$ when the lowest strain rate and highest strain rate differ by several orders of magnitude
 - Ordinate: tensile strength f_t
- Approximation to get strain rate from stress rate: $\dot{\varepsilon} \approx \dot{\sigma}/E$
- Strength reduction only in adjacent elements, Type II
- Strain rate should be filtered using RFILTF



+ rate
dependency

Strain Rate Dependency

Example

- Strain rate dependent tensile strength from literature, e.g.,

$$f_t = \left(\frac{2(n+1)K_{Ic}^n}{v_0(n-1)(Y\sqrt{\pi})^n a_i^{\frac{n-1}{2}}} \right)^{1/(1+n)} \dot{\sigma}^{1/(1+n)}$$

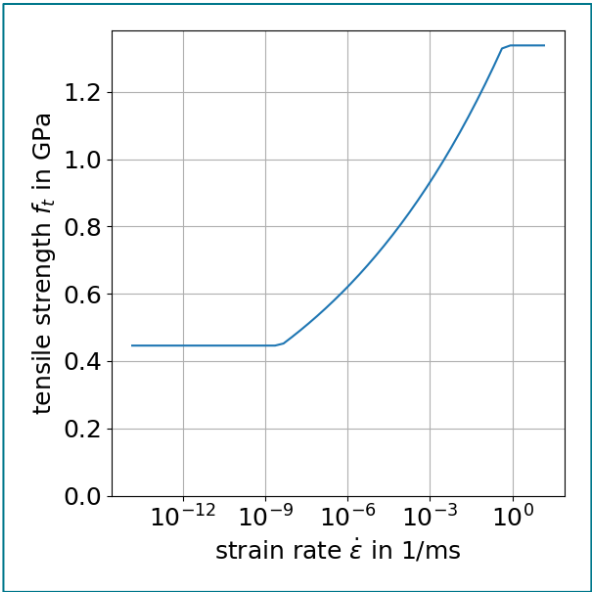
Alter, Kolling, Schneider 2017

- To be flexible LS-DYNA allows to define FT as a curve

```
*MAT_GLASS
$ MID RO E PR IMOD ILAW
$ 1 2.5E-6 70 0.23
$ FMOD FT FC AT BT AC BC FTSC1
$ SFSTI SFSTR CRIN ECRCL NCYCR NIPF
$ EPSCR ENGCR RADCR RATENL RFILTF FRACEN
$ 0.95

*DEFINE_CURVE
$ LCID SIDR SFA SFO OFFA OFFO DAT TYP LCINT
$ 100
$ ln(epsdot) ft
$ -31.187 0.158
$ 2.65926 0.473
```

$$\dot{\epsilon} = e^{2.65926} = 14.3/\text{ms}$$

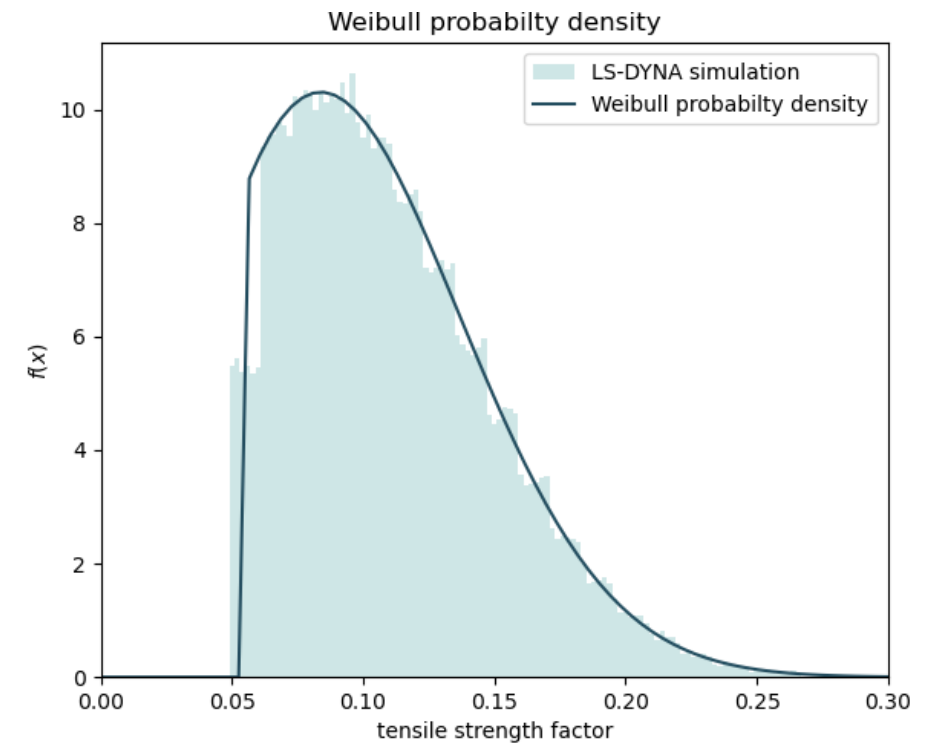
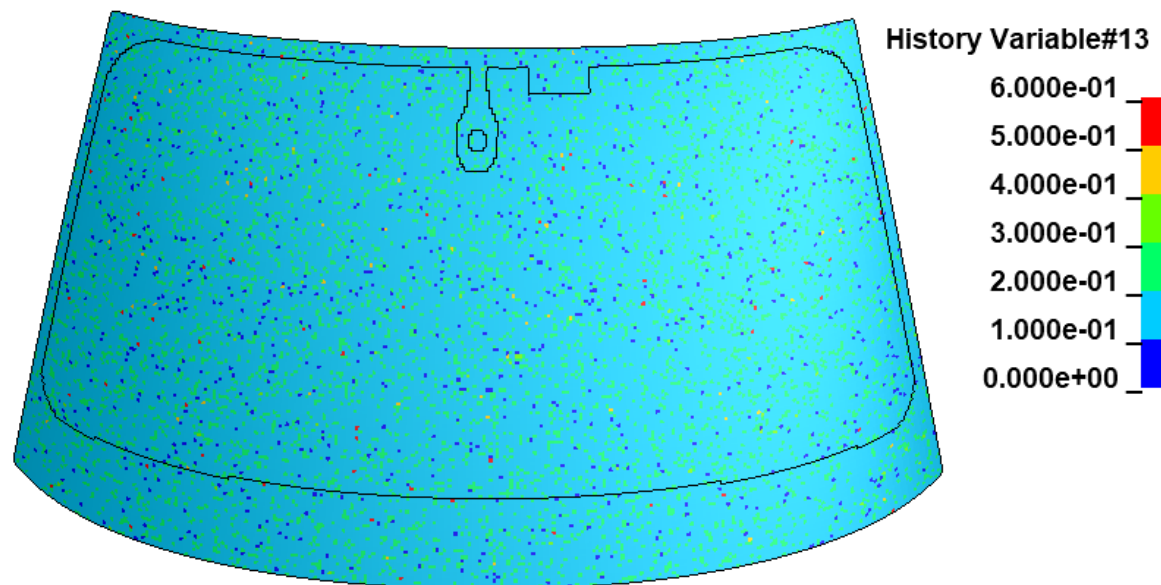


HINT

Use LS-DYNA versions \geq R12 and newer than August 2023

MAT_GLASS Features

Stochastic Variation



Stochastic Variation

How to define

- Stochastically distributed tensile strength due to microcracks
- *MAT_280_STOCHASTIC + *DEFINE_STOCHASTIC_VARIATION
→ stochastically distributed factor for tensile strength
- Kind of distribution is given by VAR_S
 - 1: Uniform random distribution
 - 2: Normal distribution
 - 3: User defined probability distribution
 - 4: User defined cumulative distribution
- History variable #13 shows factor

*PART							
Glass							
\$	PID	SECID	MID	EOSID	HGID	GRAV	ADPOPT
	100	100	100	0	0	0	0
*MAT_GLASS_STOCHASTIC							
\$	MID	RO	E	PR			IMOD
	100	2.5E-6	70	0.23			
\$	FMOD	FT	FC	AT	BT	AC	BC
		1					
\$	SFSTI	SFSTR	CRIN	ECRCL	NCYCR	NIPF	
\$	EPSCR	ENGCR	RADCRT	RATENL	RFILTF	FRACEN	
*DEFINE_STOCHASTIC_VARIATION							
\$	ID_SV	PID	PID_TYP	ICOR	VAR_S	VAR_F	IRNG
	100	100			4		1
\$	LCID						
	200						
\$	R1	R2	R3				
*DEFINE_CURVE_TITLE							
Weibull cumulative distribution							
\$	LCID	SIDR	SFA	SFO	OFFA	OFFO	DATTYP
	200						
\$		A		O			
		0.048980		0.000000			

Stochastic Variation

Example

- Stochastic variation given by left truncated Weibull distribution

- Left truncated Weibull probability density function

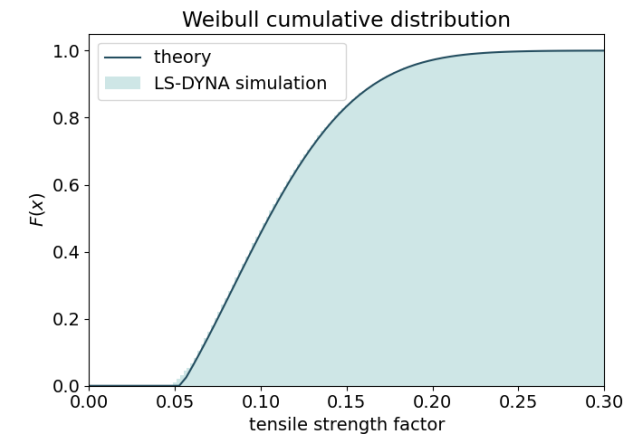
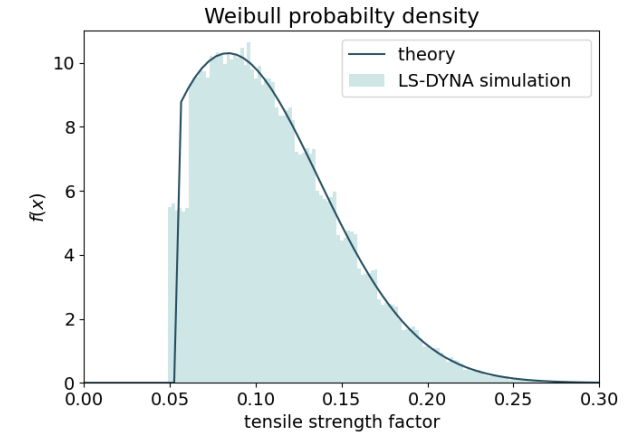
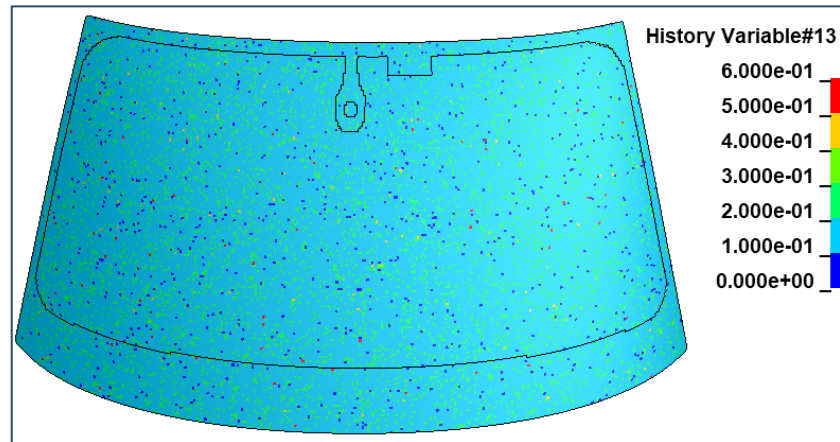
$$f(x) = \begin{cases} \left(\frac{k}{\lambda}\right) \left(\frac{x}{\lambda}\right)^{k-1} e^{\left((\tau/\lambda)^k - (x/\lambda)^k\right)} & , x \geq \tau \\ 0 & , x < \tau \end{cases}$$

- Left truncated Weibull cumulative distribution function

$$F(x) = 1 - e^{\left((\tau/\lambda)^k - (x/\lambda)^k\right)}$$

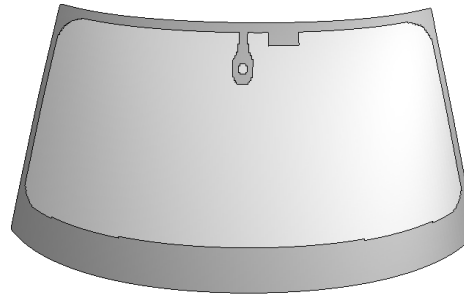
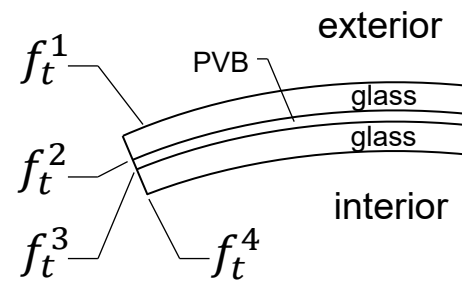
- Parameters Kolling, Schneider, FAT-Schriftenreihe 339

- Scale parameter $\lambda = 0.11$ GPa
- Shape parameter $k = 2.22$
- Truncation point $\tau = 0.054$ GPa



MAT_GLASS Features

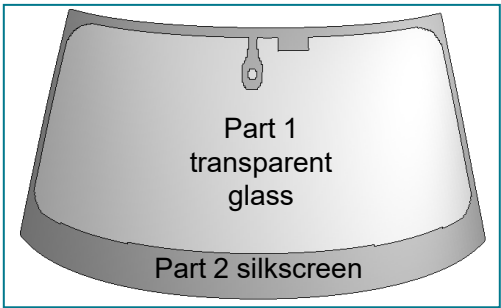
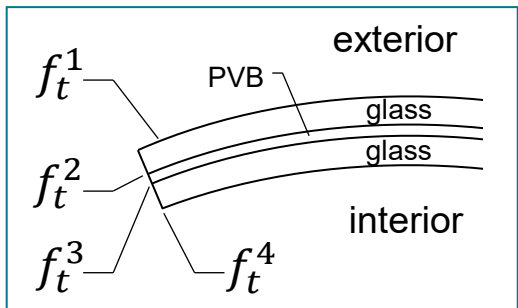
Position-Based Tensile Strength



Position-Based Tensile Strength

Ways to define

- Laminated glass
 - tensile strength varies over thickness
- Options to consider effect in LS-DYNA
 - INTEGRATION_SHELL
 - PART_COMPOSITE
- INTEGRATION_SHELL is more flexible
 - Integration rule can be defined
 - For each ply, an individual stochastic variation can be defined



```
*PART
Glass outer pane
$   PID      SECID      MID      EOSID      HGID      GRAV      ADPOPT
    100        100        100         0         0         0         0

*SECTION_SHELL
$   SECID      ELFORM      SHRF      NIP      PROPT QR / IRID      ICOMP
    100         2      0.833         3      1.0      -100         0

...

*INTEGRATION_SHELL
$ Gauss-Lobatto integration 3 IPs
$   IRID      NIP      ESOP      FAILOPT
    100         3
$   S      WF      PID
   -1.00000  0.3333333      101
    0.00000  1.3333333      101
    1.00000  0.3333333      102

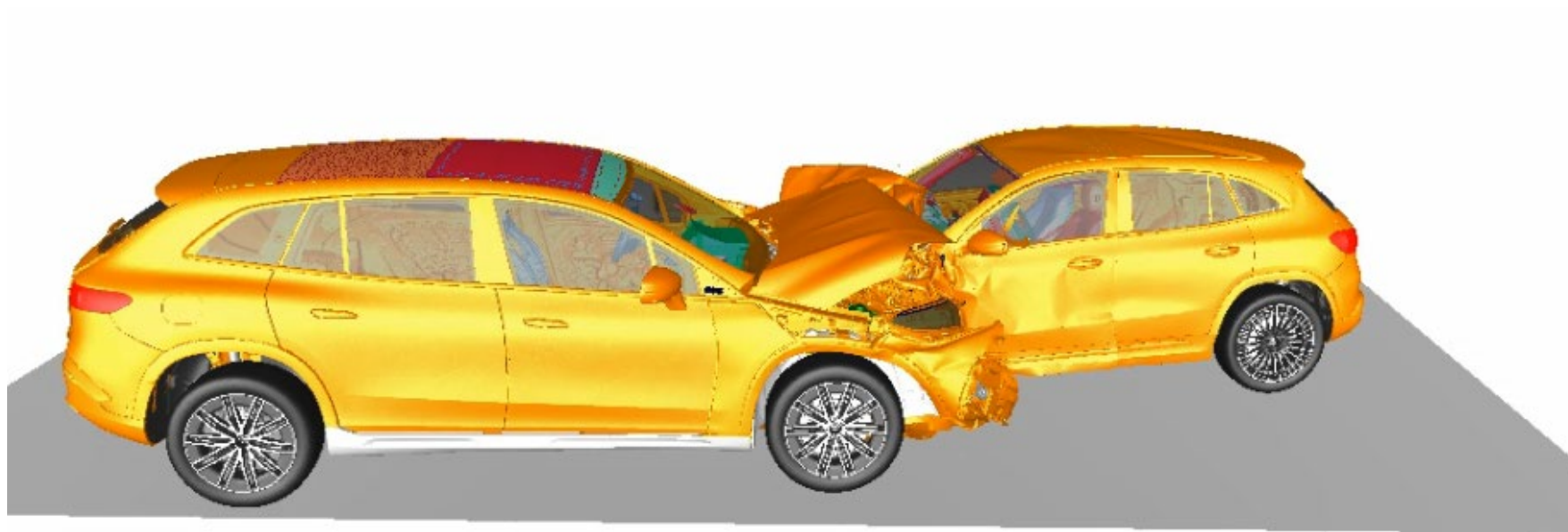
*PART
DUMMY PART - Glass outer pane - air side - position 1
$   PID      SECID      MID      EOSID      HGID      GRAV      ADPOPT
    102        100        102         0         0         0         0

*MAT_GLASS
$   MID      RO      E      PR      IMOD
    102      2.5E-6      70      0.23

...
```

Application

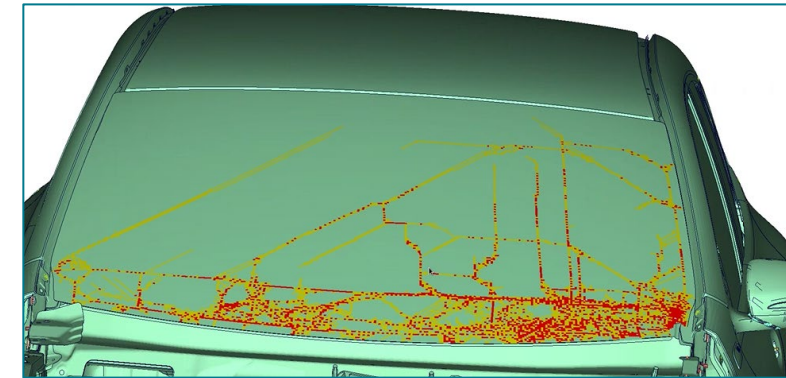
Car-to-Car Crash



Application

Car-to-Car Crash

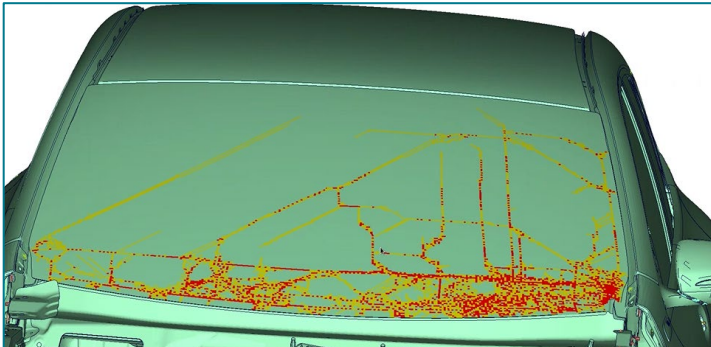
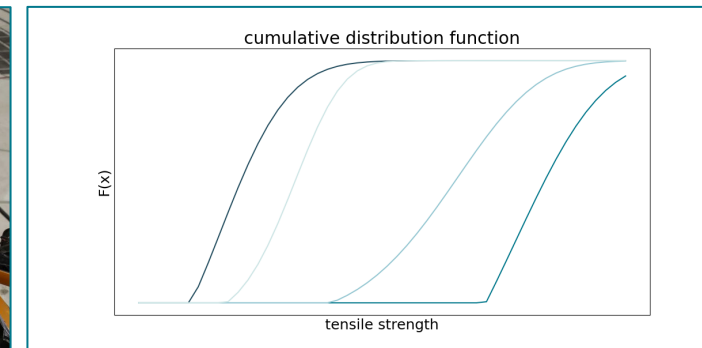
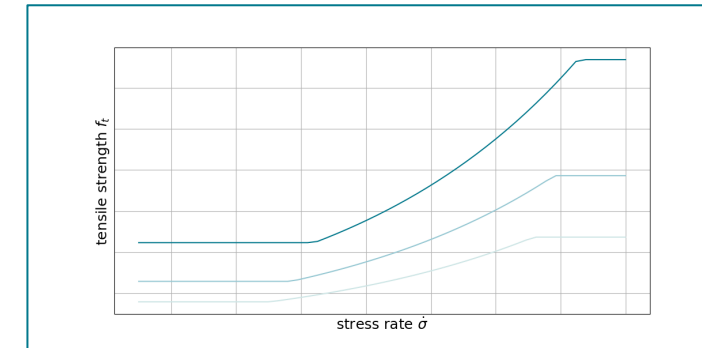
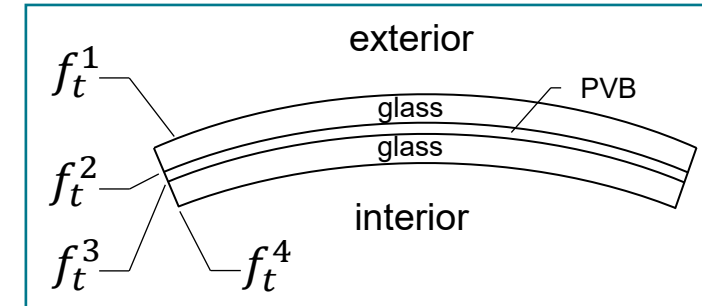
- Model presented this morning “Key success factors for digital vehicle development at Mercedes-Benz” by Markus Hermle, Markus Feucht
- Windshields modelled with MAT_GLASS
 - Shell-solid-shell discretization
 - Material card used is a work status coming from a different car model and crash scenario
 - Strength reduction
 - Strain rate dependency



Summary

Summary

- Now, we can define MAT_GLASS to use the following features
 - Strength reduction
 - Strain rate dependency
 - Stochastic variation
 - Position-based tensile strength
- MAT_GLASS can be used in full car models



Thank You

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